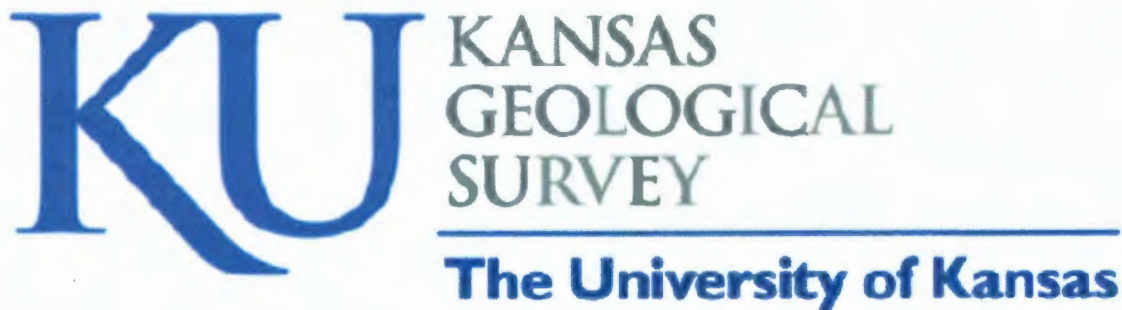


ANALYSIS OF MARMATON AND CHEROKEE GROUP CUTTINGS SAMPLES  
FOR GAS CONTENT

-- LAYNE ENERGY OPERATING, L.L.C. #8-4 TINCKNELL,  
E2 SE NE 4-T.31S.-R.17E., MONTGOMERY COUNTY, KANSAS

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## SUMMARY

Eight cuttings samples from the Pennsylvanian Marmaton Group and Cherokee Group were collected from the Layne Energy Operating, L.L.C. #8-4 Tincknell well, E2 SE NE 4-T.31S.-R.17E., Montgomery County, KS. The samples calculate as having the following gas contents:

- Little Osage Shale at 624' to 625' depth<sup>1</sup> (11 scf/ton)
- Excello Shale at 646' to 650' depth<sup>1</sup> (25 scf/ton)
- Mulky coal at 651' to 652' depth<sup>2,3</sup> (222 scf/ton)
- Iron Post coal at 680' to 682' depth<sup>4</sup> (---- scf/ton)
- Croweburg coal at 709' to 710' depth<sup>2,5</sup> (688 scf/ton)
- Flemming coal at 718' to 719' depth<sup>4</sup> (---- scf/ton)
- Mineral coal at 746' to 748' depth<sup>2</sup> (176 scf/ton)
- lower Weir coal at 877' to 878' depth<sup>2</sup> (28 scf/ton)

<sup>1</sup>no coal in sample

<sup>2</sup>assuming accompanying dark shales in sample desorb 3 scf/ton

<sup>3</sup>gas content is 98 scf/ton if accompanying dark shales in sample desorb 25 scf/ton  
(derived from Excello Shale sample at 646' to 650' depth)

<sup>4</sup>a leak was detected in the canister after desorption finished, no valid gas content  
measure is possible

<sup>5</sup>coal gas content difficult to assess due to gas-rich shales admixed with the coal

## BACKGROUND

The Layne Energy Operating, L.L.C. #8-4 Tincknell, E2 SE NE sec. 4-T.31S.-R.17E., in Montgomery Co., KS, was selected for cuttings desorption tests in association with an on-going coalbed gas research project at the Kansas Geological Survey. The samples were gathered April 7, 2004, by Jim Stegeman of Colt Energy, and turned over to K. David Newell of the Kansas Geological Survey on April 8, 2004. Samples were obtained during normal drilling of the well, with no cessation of drilling before zones of interest (i.e., coals and dark shales in the Marmaton Group and Cherokee Group) were penetrated.

The samples obtained by Jim Stegeman were canistered, with canistering times noted. These samples were collected in canisters that were supplied by the Kansas Geological Survey. Lag times for samples to reach the surface (important for assessing lost gas) were determined by using the lag times from a nearby air-drilled well (Dart Cherokee Basin #CH-1 Holder; sec. 1-T.30S.-R.14E., Wilson County, KS), which was also drilled in this vicinity. The lag times were determined by periodically noting the time it took for cuttings to reach the surface following resumption of drilling after new pipe was added to the drill string. In addition, 5 1/2 minutes was estimated for the surface time to the canistering time. This was the average time derived from the handling of 109 air-drilled cuttings samples by various industry and Survey personnel.

Eight cuttings samples from the Pennsylvanian Marmaton and Cherokee Groups were collected:

- Little Osage Shale at 624' to 625' depth (1912 grams dry wt.)
- Excello Shale at 646' to 650' depth (654 grams dry wt.)
- Mulky coal at 651' to 652' depth (131 grams dry wt.)
- Iron Post coal at 680' to 682' depth (sample not saved)
- Croweburg coal at 709' to 710' depth (1261 grams dry wt.)
- Flemming coal at 718' to 719' depth (sample not saved)
- Mineral coal at 746' to 748' depth (698 grams dry wt.)
- lower Weir coal at 877' to 878' depth (2000 grams dry wt.)

The cuttings were caught in kitchen strainers as they exited the air-stream pipe emptying to the mud pit. The samples were then washed in water while in the kitchen strainers to rid them of as much drilling mud as possible before the cuttings were placed in desorption canisters. Water with zephyrn chloride biocide was then added to the canisters, with a headspace of 1 to 2 inches being preserved at the top of the canister.

Several desorption volumetric measurements were made April 7 and 8 by Jim Stegeman. All samples were transported on the afternoon of April 8th afternoon to the laboratory at the Kansas Geological Survey in Lawrence, KS, and desorption measurements were continued at approximately 70 °F . Desorption measurements were periodically made until the canisters produced negligible gas with daily testing for at least two successive days.

## DESORPTION MEASUREMENTS

The equipment and method for measuring desorption gas is that prescribed by McLennan and others (1995). The volumetric displacement apparatus is a set of connected dispensing burettes, one of which measures the gas evolved from the desorption canister. The other burette compensates for the compression that occurs when the desorbed gas displaces the water in the measuring burette. This compensation is performed by adjusting the cylinders so that their water levels are identical, then figuring the amount of gas that evolved by reading the difference in water level using the volumetric scale on the side of the burette.

The desorption canisters were obtained from SSD, Inc., in Grand Junction, CO. These canisters are 12.5 inches high (32 cm), 3 1/2 inches (9 cm) in diameter, and enclose a volume of approximately 150 cubic inches (2450 cm<sup>3</sup>). The desorbed gas that collected in the desorption canisters was periodically released into the volumetric displacement apparatus and measured as a function of time, temperature, and atmospheric pressure.

Atmospheric pressure was measured in the field by Jim Stegeman using an analog barometer. The time and atmospheric pressure were measured in the lab using a portable weather station (model BA928) marketed by Oregon Scientific (Tualatin, OR). The atmospheric pressure was displayed in millibars on this instrument, however, this

measurement was not the actual barometric pressure, but rather an altitude-compensated barometric pressure automatically converted to a sea-level-equivalent pressure. To translate this measurement to actual atmospheric pressure, a regression correlation was determined over several weeks by comparing readings from the Oregon Scientific instrument to that from a pressure transducer in the Petrophysics Laboratory in the Kansas Geological Survey in Lawrence, KS (Figure 1). The regression equation shown graphically in Figure 1 was entered into a spreadsheet and was used to automatically convert the millibar measurement to barometric pressure in pounds per square inch (psi).

A spreadsheet program written by K.D. Newell (Kansas Geological Survey) was used to convert all gas volumes at standard temperature and pressure. Conversion of gas volumes to standard temperature and pressure was by application of the perfect-gas equation, obtainable from basic college chemistry texts:

$$n = PV/RT$$

where n is moles of gas, T is degrees Kelvin (i.e., absolute temperature), V is in liters, and R is the universal gas constant, which has a numerical value depending on the units in which it is measured (for example, in the metric system  $R = 0.0820$  liter atmosphere per degree mole). The number of moles of gas (i.e., the value n) is constant in a volumetric conversion, therefore the conversion equation, derived from the ideal gas equation, is:

$$(P_{\text{stp}}V_{\text{stp}})/(RT_{\text{stp}}) = (P_{\text{rig}}V_{\text{rig}})/(RT_{\text{rig}})$$

Customarily, standard temperature and pressure for gas volumetric measurements in the oil industry are 60 °F and 14.7 psi (see Dake, 1978, p. 13), therefore  $P_{\text{stp}}$ ,  $V_{\text{stp}}$ , and  $T_{\text{stp}}$ , respectively, are pressure, volume, and temperature at standard temperature and pressure, where standard temperature is degrees Rankine ( $^{\circ}R = 460 + ^{\circ}F$ ).  $P_{\text{rig}}$ ,  $V_{\text{rig}}$ , and  $T_{\text{rig}}$ , respectively, are ambient pressure, volume, and temperature measurements taken at the rig site or in the desorption laboratory.

The universal gas constant R drops out as this equation is simplified and the determination of  $V_{\text{stp}}$  becomes:

$$V_{\text{stp}} = (T_{\text{stp}}/T_{\text{rig}}) (P_{\text{rig}}/P_{\text{stp}}) V_{\text{rig}}$$

The conversion calculations in the spreadsheet were carried out in the English metric system, the customary measure system used in American coal and oil industry. V is therefore converted to cubic feet; P is psia; T is °R.

The desorbed gas was summed over the time period for which the coal samples evolved all of their gas.

Lost gas for samples (i.e., the gas lost from the sample from the time it was drilled, brought to the surface, to the time it was canistered) are normally determined using the

direct method (Kissel and others, 1975; also see McLennan and others, 1995, p. 6.1-6.14) in which the cumulative gas evolved is plotted against the square root of elapsed time. Time zero is assumed to be the moment that the rock is cut and its cuttings circulated off bottom. Lost gas, however, had to be inferred for the samples collected from this well because few desorption measurements could be made in the first hour after canistering. The procedure used to infer lost gas for these samples is outlined in the section below on Lost Gas.

## LITHOLOGIC ANALYSIS

Upon removal from the canisters, the cuttings were washed of drilling mud, and dried in an oven at 150 °F for 1 to 3 days. After drying, the cuttings were weighed and then dry sieved into 5 size fractions: >0.0930", >0.0661", >0.0460", >0.0331", and <0.0331". For large sample sizes, the cuttings were run through a sample splitter and a lesser portion (approximately 75 grams) were sieved and weighed, and the derived size-fraction ratios were applied to the entire sample.

The size fractions were then inspected and sorted by hand under a dissecting microscope. Three major lithologic categories were differentiated: coal, dark shales (generally Munsell rock colors N3 [dark gray], N2 [grayish black], and N1 [black] on dry surface), and lighter-colored lithologies and/or dark and light-colored carbonates. The lighter-colored lithologies are considered to be incapable of generating significant amounts of gas. After sorting, and for every size class, each of these three lithologic categories was weighed and the proportion of coal dark shale and light-colored lithologies were determined for the entire cuttings sample based on the weight percentages.

## DATA PRESENTATION

Data and analyses accompanying this report are presented in the following order: 1) lag time to surface for the well cuttings, 2) data tables for the desorption analyses, 3) lost-gas graphs, 4) "lithologic component sensitivity analyses" showing the interdependence of gas evolved from dark shale versus coal in each sample, 5) a summary component analysis for all samples showing relative reliability of the data from all the samples, and 6) a desorption graph for all the samples.

### *Graph of Lag-time to Surface for Well Cuttings (Figure 2)*

Lag time of cuttings to surface varied, but there is a general trend of longer lag times for greater depth. The lag times accepted for cuttings were taken to be a visual average of the trend (defined by the scatter of data points on this graph) at the depth at which the samples were taken.

### *Data Tables of the Desorption Analyses (Table 1)*

These are the basic data used for lost-gas analysis and determination of total gas desorbed from the cuttings samples. Basic temperature, volume, and barometric measurements are

listed at left. Farther to the right, these are converted to standard temperature, pressure, and volumes. The volumes are cumulatively summed, and converted to scf/ton based on the total weight of coal and dark shale in the sample. At the right of the table, the time of the measurements are listed and converted to hours (and square root of hours) since the sample was drilled.

#### *Lost-Gas Graphs (Figure 3)*

To infer an approximate lost-gas value for each sample, a correlation of the total gas desorbed from a sample after it had been canistered to its rate of lost gas was developed using desorption data accumulated for 42 cuttings samples obtained from air-drilled wells in the Cherokee basin in southeastern Kansas (Figure 3). The rate of lost gas used in this correlation was that amount of gas lost by 0.6 hours<sup>0.5</sup> (the square root of 0.36 hours). By knowing the total gas given up by the sample after canistering (i.e., the total gas desorbed) a hypothetical rate of lost-gas could be calculated using the a regression line:

$$\text{lost gas rate per square root of 0.36 hours} = 0.1241 X (\text{total gas desorbed in ccs}) + 48.14$$

Once the hypothetical lost-gas rate was calculated, the lost gas could be calculated by taking the square root of the bottom-hole to canister time (derived from subtracting the lag time plus 5 1/2 minutes handling time [surface time to canister time] from the surface time), and multiplying it times the hypothetical lost-gas rate. Analysis of the lithology of the cuttings used in this correlation revealed no consistent relationship (see Figure 3), therefore further refinement of the relationship of the rate of lost gas to the total gas desorbed after canistering is not possible.

#### *"Lithologic Component Sensitivity Analyses" (Figures 4-8)*

The rapidity of penetration of an air-drilled well makes collection of individual (i.e., unmixed) lithologies from relatively thin-bedded strata rather difficult. Mixed lithologies are more the norm rather than the exception. Some of this mixing is due to cavings from strata farther up hole. The mixing may also be due to collection of two or more successively drilled lithologies in the kitchen sieve at the exit line, or differential lifting of relatively less-dense coal compared to other lithologies, all of which are more dense than coal.

The total gas evolved from the sample is due to gas being desorbed from both the coal and dark shale. Both lithologies are capable of generating gas, albeit the coal will be richer in gas than the dark-colored shale. Even though dark-colored shale is less rich in sorbed gas than coal, if a sample has a large proportion of dark, organic-rich shale and only a minor amount of coal, the total volume of gas evolved from the dark-shale component may be considerable. The lighter-colored lithologies are considered to be incapable of generating significant amounts of gas.

The total amount of gas evolved from a cuttings sample can be expressed by the following equation:

$$\text{Total gas (cm}^3\text{)} = [\text{weight}_{\text{coal}} (\text{grams}) \times \text{gas content}_{\text{coal}} (\text{cm}^3/\text{gram})] +$$

$$[\text{weight}_{\text{dark shale}} (\text{grams}) \times \text{gas content}_{\text{dark shale}} (\text{cm}^3/\text{gram})]$$

A unique solution for  $\text{gas content}_{\text{coal}}$  in this equation is not possible because  $\text{gas content}_{\text{dark shale}}$  is not known exactly. An answer can only be expressed as a linear solution to the above equation. The richer in gas the dark shales are, the poorer in gas the admixed coal has to be, and vice versa. If there is little dark shale in a sample, a relatively well constrained answer for  $\text{gas content}_{\text{coal}}$  can be obtained. Conversely, if considerable dark shale is in a sample, the gas content of a coal will be hard to precisely determine.

The lithologic-component-sensitivity-analysis diagram therefore expresses the bivariant nature inherent in the determination of gas content in mixed cuttings. The gas content of dark shales in Kansas can vary greatly. Proprietary desorption analyses of dark shales in cores from southeastern Kansas have registered as much as 50 scf/ton, but can be as low as 2-4 scf/ton.

A value of 3 scf/ton for average dark shale is based on the assay of the gas content of cores of dark shales in nearby wells. However, high-gamma-ray shales (such as the Excello Shale), also colloquially known as "hot shales", typically have more organic matter and associated gas content than dark shales with no excessive gamma-ray level. Determination of gas content for a coal associated with a "hot" shale therefore carries more uncertainty than if the coal were associated with a shale without a high gamma-ray value.

In general, shale gas content does not have to be very much greater than 10 scf/ton before the associated coal starts to have a gas content less than that of the dark shale. In all the lithologic-component-sensitivity-analysis diagrams, a "break-even" point is therefore noted where the gas content of the coal is equal to that of the dark shale. This "break-even" point corresponds to the minimum gas content assignable to the coal and maximum gas content assignable to the dark shale. It can also be thought of the scf/ton gas content of the cuttings sample minus the weight of any of the lighter-colored lithologies, which are assumed to have no inherent gas content. Conversely, to assume that all the gas evolved from a cuttings sample is derived solely from the coal would result in an erroneously high gas content for the coal.

#### *Summary Component Analysis for all Samples (Figure 9)*

This diagram is a summary of the individual "lithologic component sensitivity analyses" for each sample, all set at a common scale. The steeper the angle of the line for a sample, the more uncertainty is attached to the results (i.e.,  $\text{gas content}_{\text{coal}}$ ) for that sample. If the coal content is miniscule (i.e., < approximately 5%), the results are a better reflection of the  $\text{gas content}_{\text{dark shale}}$ .

#### *Desorption Graph (Figure 10)*

This is a desorption graph (gas content per weight vs. square root of time) for all the samples. The rate at which gas is evolved from the samples is thus comparable at a common scale. The final value represents the standard cubic feet of gas per ton (scf/ton)

calculated for the sample, using the combined weight of the coal and dark shale in the sample.

## RESULTS and DISCUSSION

Two samples (Little Osage Shale at 624' to 625' depth; Excello Shale at 646' to 650' depth) contained no coal. The gas analyses associated with these samples are therefore a gas content for shale.

The Mulky coal (651'-652' depth) and Croweburg coal (709'-710' depth) samples registered high gas contents (respectively 222 scf/ton and 688 scf/ton; assuming accompanying black shales desorbed 3 scf/ton). These samples were dominated by very dark to black shales (N1, N2) that display high-gamma ray values on wireline logs. If 25 scf/ton is assumed to be the gas content of the dark shales accompanying the Mulky coal (i.e., the gas content determined for the Excello Shale sample just a few feet above the Mulky coal), a unique solution of 97 scf/ton for the gas content for the Mulky coal can be determined. The shales accompanying the Croweburg sample are likely richer in gas content, perhaps 50 to 60 scf/ton.

The best constrained data are that associated with the Mineral coal sample (746'-748'), which contained 24% coal. This sample is followed closely by the Mulky coal sample (651'-652' depth) and Croweburg coal sample (709'-710' depth), which respectively have 4% and 6% coal. The lower Weir coal sample (877'-878' depth), with 4% coal, also has acceptably constrained data, but the calculated gas content for the coal in this samples varies more with whatever value is assumed for the accompanying black shales due to the large amount of dark shale in the sample. The subsidiary amount of coal in this sample imparts some uncertainty to the desorption measurements, but an approximation of its gas content is nevertheless obtained. An estimate for gas content for the coal in this sample can be made, assuming the admixed dark shale in the sample desorb 3 scf/ton.

Leaks were detected in the canisters containing the Iron Post coal (680'-682' depth) and Flemming coal (718'-719' depth), thus any data collected for these sample are considered invalid. No material was retained from this canister for any further analyses.

## REFERENCES

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## FIGURES and TABLES

FIGURE 1. Correlation of field barometer to Petrophysics Lab pressure transducer.

FIGURE 2. Lag-time to surface for well cuttings.

TABLE 1. Desorption measurements for samples.

FIGURE 3. Correlation of the rate of lost gas to the total gas desorbed after canistering.

FIGURE 4. Sensitivity analysis for Little Osage Shale at 624' to 625' depth.

FIGURE 5. Sensitivity analysis for Excello Shale at 646' to 650' depth and Mulky coal sample at 651' to 652' depth.

FIGURE 6. Sensitivity analysis for Croweburg coal at 709' to 710' depth.

FIGURE 7. Sensitivity analysis for Mineral coal at 746' to 748' depth.

FIGURE 8. Sensitivity analysis for lower Weir coal at 877' to 878' depth.

FIGURE 10. Lithologic component sensitivity analyses for all samples.

FIGURE 11. Desorption graph for all samples.

## Correlation of Field Barometer to KGS Petrophysics Lab Barometer

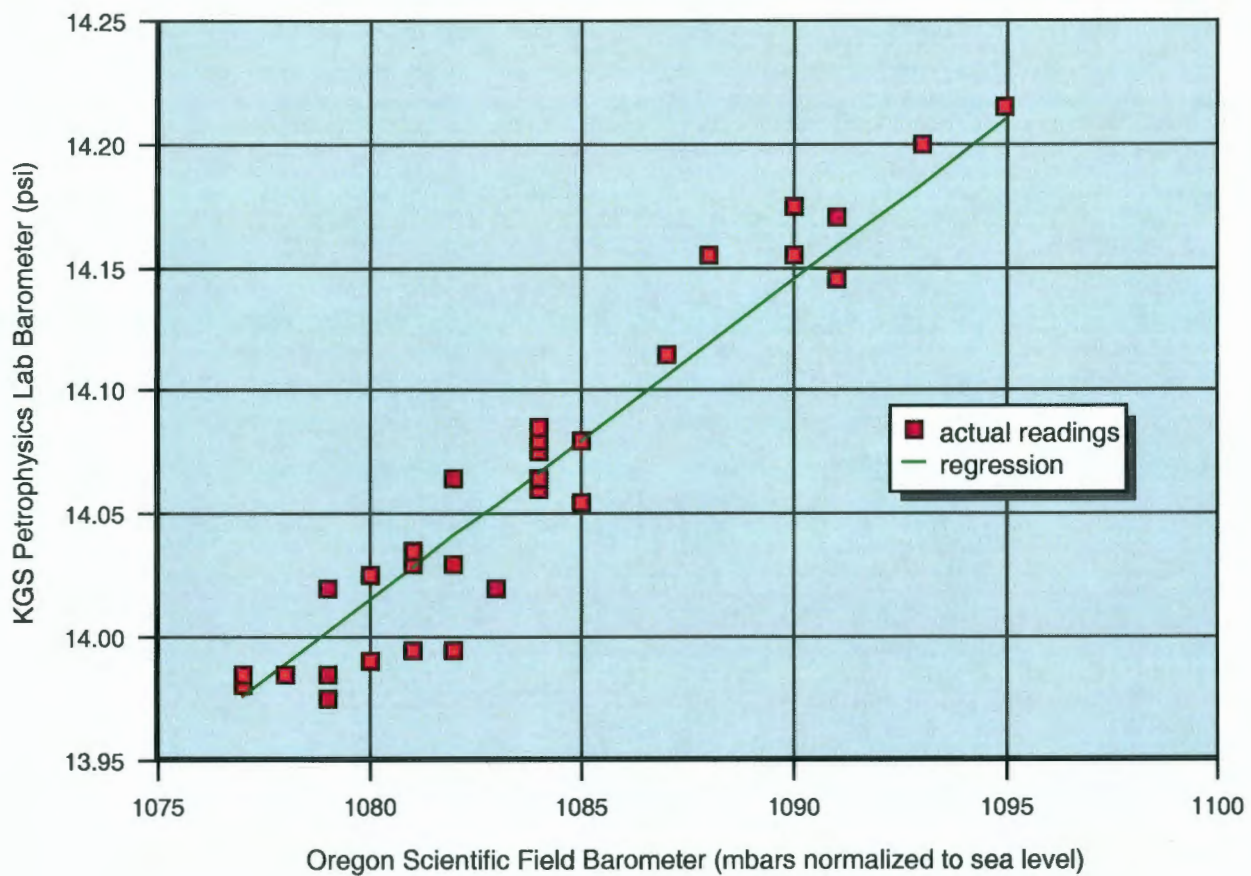
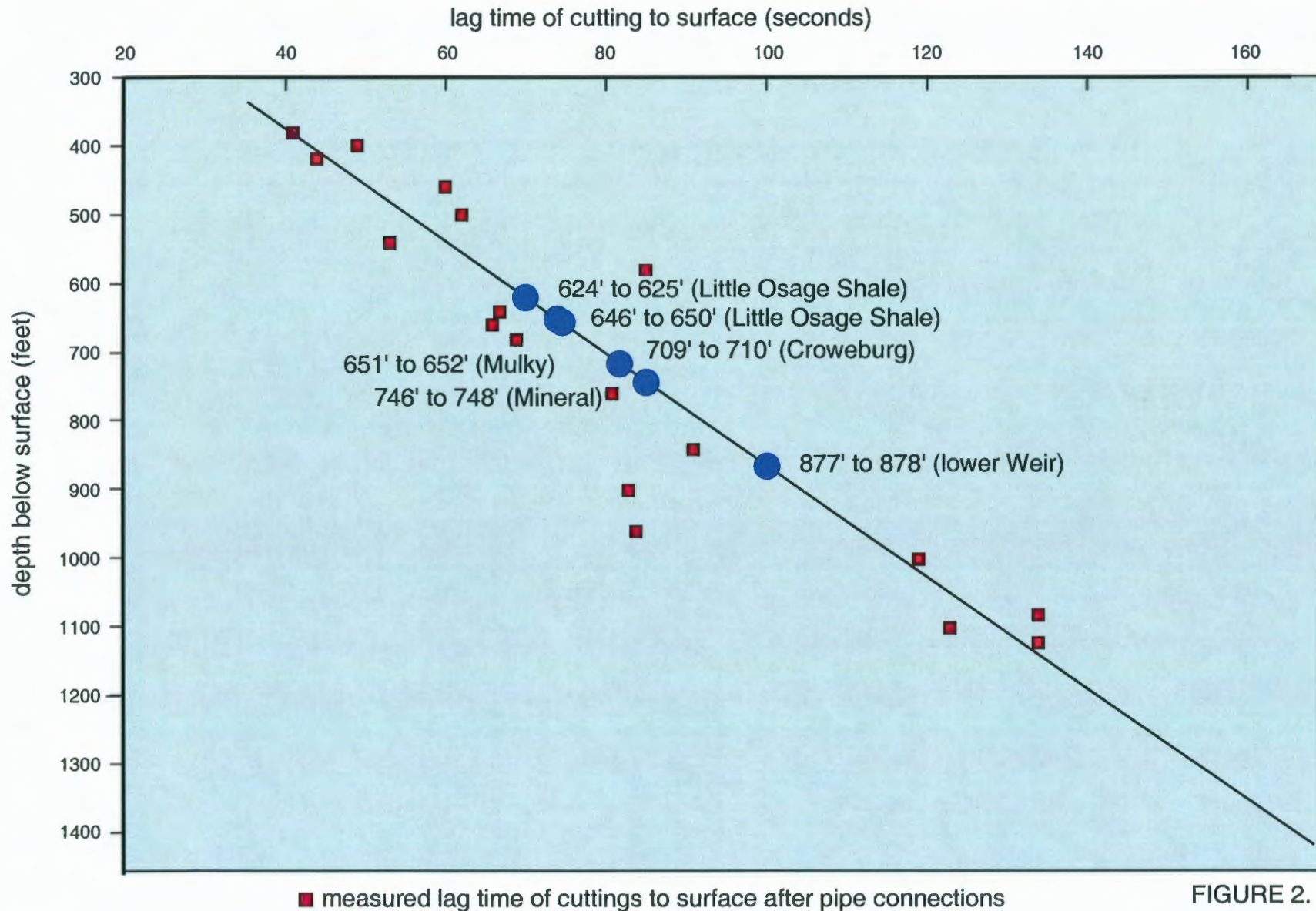


FIGURE 1.

Layne Energy Operating, L.L.C. #8-4 Tincknell, E2 SE NE 4-T.31S.-R.17E., Montgomery Co., KS  
(based on lag times from Dart Cherokee Basin #CH-1 Holder; sec. 1-T.30S.-R.14E., Wilson County, KS)

lag-time to surface for well cuttings









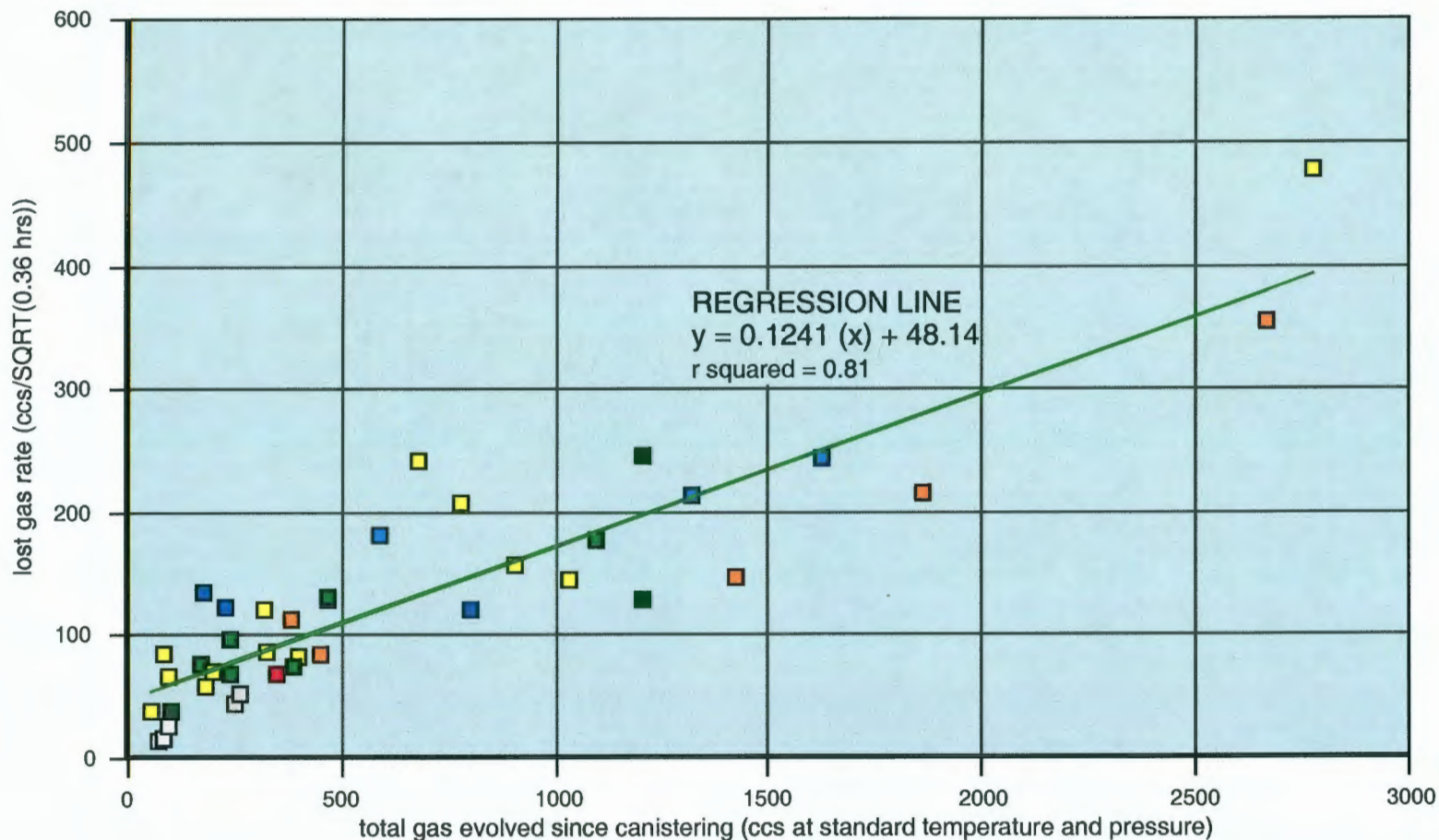


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4	71	1081	0.0001	531 14.031	0.000132037	3.74	0.003851903	109.07	2.04	2.51	4/17/04	19:38	246:26:12	246:24:30	246:19:00	15.69830139
3	71	1079	0.0001	531 14.005	9.88442E-05	2.80	0.003950747	111.87	2.10	2.56	4/18/04	16:07	266:57:12	268:55:30	268:50:00	16.3387086
0	88	1088	0	528 14.122	0	0.00	0.003950747	111.87	2.10	2.56	4/19/04	14:08	288:56:12	288:56:30	288:51:00	16.99911782
8	71	1071	0.0003	531 13.901	0.00028163	7.41	0.004212377	119.28	2.23	2.70	4/20/04	13:03	311:53:12	311:51:30	311:46:00	17.66031332
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2	68	1080	7E-05	528 14.018	6.4332E-05	1.88	0.004377747	123.98	2.32	2.79	4/22/04	16:19	363:09:12	363:07:30	363:02:00	19.05858241
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0	88	1090	0	528 14.148	0	0.00	0.004509418	127.89	2.39	2.88	4/28/04	23:21	488:11:12	488:09:30	488:04:00	21.5813583
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7	68	1072	0.0002	528 13.814	0.000230442	6.53	0.004840575	137.07	2.57	3.04	4/28/04	15:32	508:22:12	508:20:30	508:15:00	22.50288851
2	88	1079	7E-05	528 14.005	6.82708E-05	1.88	0.004908848	136.95	2.80	3.07	4/29/04	14:33	529:23:12	529:21:30	529:16:00	23.00840428
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5	88	1081	0.0002	528 14.031	0.000168615	4.72	0.005140546	145.58	2.73	3.19	5/5/04	9:39	668:29:12	668:27:30	668:22:00	25.8551091
4	69	1079	0.0001	529 14.005	0.000132291	3.75	0.005272837	149.31	2.80	3.26	5/8/04	10:57	693:47:12	693:45:30	693:40:00	26.33983042
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2	71	1081	7E-05	531 14.031	6.80183E-05	1.87	0.005702113	181.47	3.02	3.49	5/10/04	13:52	792:42:12	792:40:30	792:35:00	28.15498772
3	71	1077	0.0001	531 13.979	9.8881E-05	2.79	0.005800774	184.28	3.08	3.54	5/11/04	14:13	817:03:12	817:01:30	816:56:00	28.58414479
3	72	1078	0.0001	532 13.988	9.83841E-05	2.79	0.005899158	187.04	3.13	3.60	5/12/04	10:38	837:28:12	837:26:30	837:21:00	28.93907393
1	72	1081	4E-05	532 14.031	3.29471E-05	0.93	0.005932105	187.98	3.15	3.61	5/13/04	14:24	865:14:12	865:12:30	865:07:00	29.41490552
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4	68	1082	0.0001	528 14.044	0.00013291	3.76	0.005984207	188.89	3.16	3.63	5/17/04	9:37	958:27:12	958:25:30	958:20:00	30.92857972
2	70	1083	7E-05	530 14.057	6.82852E-05	1.88	0.006030473	170.78	3.20	3.87	5/18/04	14:33	985:23:12	985:21:30	985:16:00	31.39088918
5	72	1081	0.0002	532 14.031	0.000164736	4.86	0.006195208	175.43	3.29	3.75	5/20/04	13:52	1032:42:12	1032:40:30	1032:35:00	32.13570185
3	73	1079	0.0001	533 14.005	9.84733E-05	2.79	0.006293881	178.22	3.34	3.81	5/21/04	13:51	1058:41:12	1058:39:30	1058:34:00	32.50871725
5	72	1074	0.0002	532 13.940	0.000183889	4.83	0.00645735	182.85	3.42	3.89	5/23/04	14:59	1105:49:12	1105:47:30	1105:42:00	33.25387198
2	73	1075	7E-05	533 13.953	6.54055E-05	1.85	0.006522756	184.70	3.48	3.93	5/24/04	10:24	1125:14:12	1125:12:30	1125:07:00	33.5445475
0	72	1080	0	532 14.018	0	0.00	0.006522756	184.70	3.48	3.93	5/25/04	11:51	1150:41:12	1150:39:30	1150:34:00	33.92177275
1	70	1075	4E-05	530 13.953	3.26879E-05	0.93	0.006555644	185.83	3.48	3.94	5/28/04	12:38	1175:26:12	1175:24:30	1175:19:00	34.28484185
3	70	1070	0.0001	530 13.888	9.82047E-05	2.78	0.006653848	188.42	3.53	4.00	5/27/04	11:12	1198:02:12	1198:00:30	1197:55:00	34.61288828
0	72	1078	0	532 13.982	0	0.00	0.006653848	188.42	3.53	4.00	5/28/04	13:11	1224:01:12	1223:59:30	1223:54:00	34.9859972
4	71	1069	0.0001	531 13.875	0.000130671	3.70	0.008784419	192.11	3.80	4.07	5/29/04	14:20	1249:10:12	1249:08:30	1249:03:00	35.34359914
2	71	1067	7E-05	531 13.849	6.51833E-05	1.85	0.006849583	193.96	3.83	4.10	5/30/04	12:47	1271:37:12	1271:35:30	1271:30:00	35.85878127
-1	70	1077	-4E-05	530 13.879	-3.28491E-05	-0.93	0.006818834	193.02	3.81	4.08	6/1/04	10:49	1317:39:12	1317:37:30	1317:32:00	36.29949495
-2	70	1085	-7E-05	530 14.083	-6.83878E-05	-1.88	0.008750246	191.14	3.58	4.05	6/2/04	13:34	1344:24:12	1344:22:30	1344:17:00	36.88810808
-1	70	1080	-4E-05	530 14.148	-3.33488E-05	-0.94	0.008718899	190.20	3.56	4.03	6/3/04	11:11	1388:01:12	1385:59:30	1385:54:00	36.95970779
2	71	1087	7E-05	531 14.109	6.83847E-05	1.88	0.008783284	192.08	3.80	4.07	6/4/04	13:43	1392:33:12	1392:31:30	1392:26:00	37.31893092

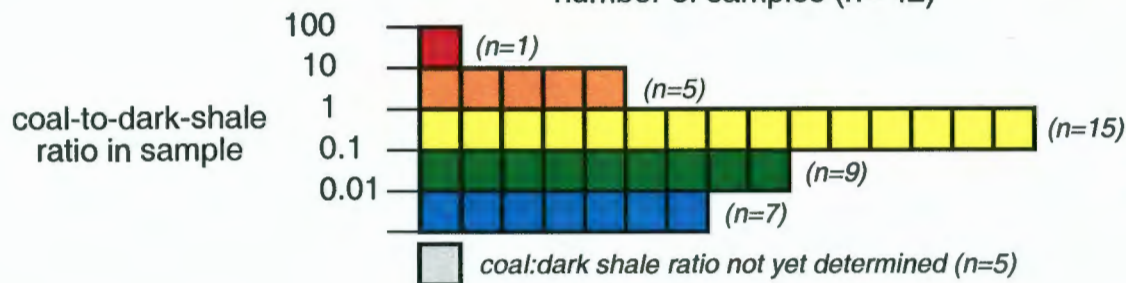
DECANISTERED 6/4/2004; sample dried 10 days in air



RELATIONSHIP of TOTAL GAS EVOLVED FROM a CUTTINGS SAMPLE to RATE of LOST-GAS  
 (from 42 cuttings samples from air-drilled wells, Cherokee basin, southeastern Kansas)



number of samples (n= 42)



LOST-GAS ALGORITHM

$$\text{ccs lost gas} = \sqrt{X} (Y)$$

where X = bottom-hole to canister time (in hours)  
 where Y = ccs lost gas at 0.36 hours  
 (i.e., value Y from regression equation)

FIGURE 3.

# Desorption Characteristics of Cuttings Samples

Layne Energy Operating, L.L.C. #8-4 Tincknell, E2 SE NE 4-T.31S.-R.17E., Montgomery Co., KS

LITHOLOGIC COMPONENT SENSITIVITY ANALYSIS for calculation of Little Osage Shale from 624' to 625'

$$\text{GAS CONTENT}_{\text{coal}} = \frac{\text{total gas desorbed} - ((\text{gas content}_{\text{dark shale}}) * (\text{weight}_{\text{dark shale}}))}{\text{weight}_{\text{coal}}}$$

total gas desorbed  
(including estimated lost gas) = 518.0 ccs

TOTAL DRY WEIGHT OF SAMPLE = 1912.10 grams

weight<sub>light-colored lithologies</sub> = 211.51 grams (11.1%)

weight<sub>dark shale</sub> = 1700.59 grams (88.9%)

weight<sub>coal</sub> = 0.00 grams (0.0%)

sieve size	grams	% coal / % dark shale / % light-colored liths
>0.0930"	1280.49	0.00% / 88.92% / 11.08%
>0.0661"	262.27	0.00% / 87.76% / 12.24%
>0.0460"	184.51	0.00% / 90.13% / 9.87%
>0.0331"	90.71	0.00% / 89.12% / 10.88%
<0.0331"	94.11	0.00% / 90.00% / 10.00%
<b>1912.10 TOTAL</b>		

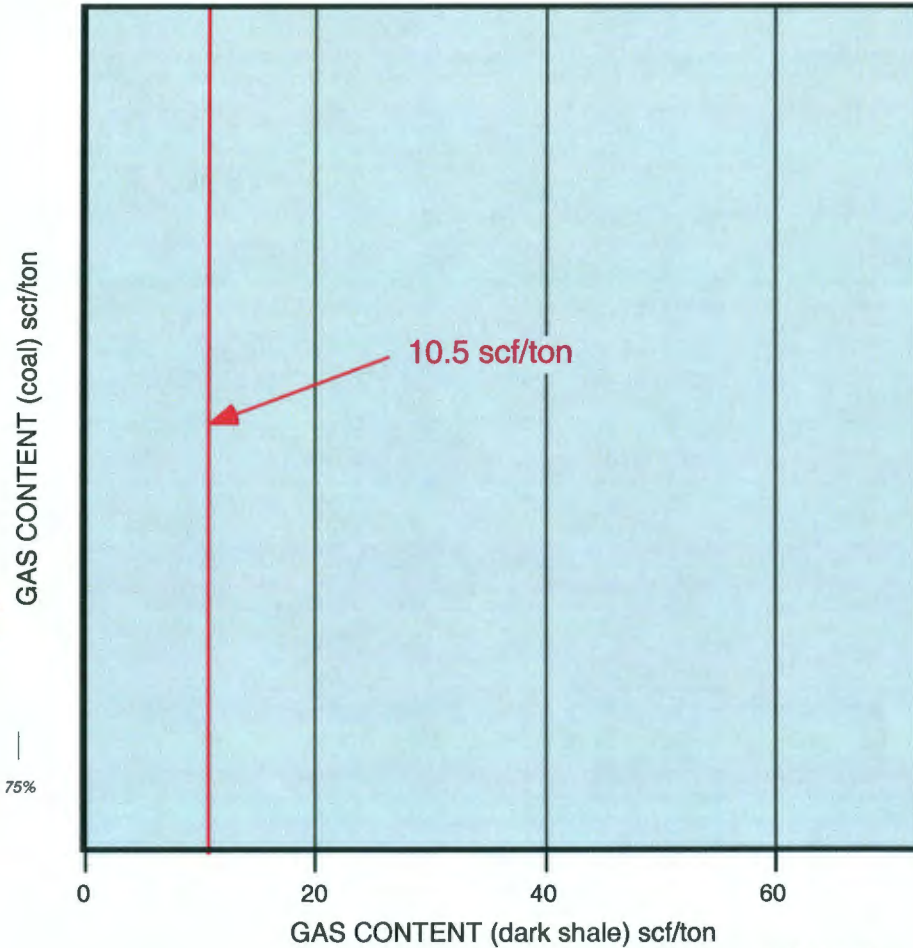


FIGURE 4.

# Desorption Characteristics of Cuttings Samples

Layne Energy Operating, L.L.C. #8-4 Tincknell, E2 SE NE 4-T.31S.-R.17E., Montgomery Co., KS

LITHOLOGIC COMPONENT SENSITIVITY ANALYSIS for calculation of Excello Shale from 646' to 650' and Mulky coal from 651' to 652'

$$\text{GAS CONTENT}_{\text{coal}} = \frac{\text{total gas desorbed} - ((\text{gas content}_{\text{dark shale}}) * (\text{weight}_{\text{dark shale}}))}{\text{weight}_{\text{coal}}}$$

total gas desorbed (**Excello Shale**)  
(including estimated lost gas) = 653.8 ccs

TOTAL DRY WEIGHT OF SAMPLE = 853.89 grams

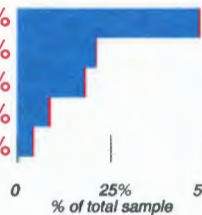
weight<sub>light-colored lithologies</sub> = 18.53 grams (2.2%)

weight<sub>dark shale</sub> = 835.36 grams (97.8%)

weight<sub>coal</sub> = 0.00 grams (0.0%)

sieve size	grams	% coal / % dark shale / % light-colored liths
>0.0930"	413.51	0.00% / 99.09% / 0.91%
>0.0661"	177.44	0.00% / 99.29% / 0.71%
>0.0460"	153.55	0.00% / 96.93% / 3.07%
>0.0331"	73.40	0.00% / 92.93% / 7.07%
<0.0331"	35.99	0.00% / 90.00% / 10.00%

**853.89 TOTAL**



total gas desorbed (**Mulky coal**)  
(including estimated lost gas) = 130.7 ccs

TOTAL DRY WEIGHT OF SAMPLE = 383.50 grams

weight<sub>light-colored lithologies</sub> = 267.52 grams (69.8%)

weight<sub>dark shale</sub> = 98.42 grams (25.7%)

weight<sub>coal</sub> = 17.56 grams (4.06%)

sieve size	grams	% coal / % dark shale / % light-colored liths
>0.0930"	243.27	2.55% / 27.47% / 69.97%
>0.0661"	75.98	8.81% / 19.67% / 71.52%
>0.0460"	47.84	6.97% / 25.44% / 67.60%
>0.0331"	12.04	7.96% / 28.85% / 63.46%
<0.0331"	4.37	9.09% / 22.73% / 68.61%

**383.50 TOTAL**

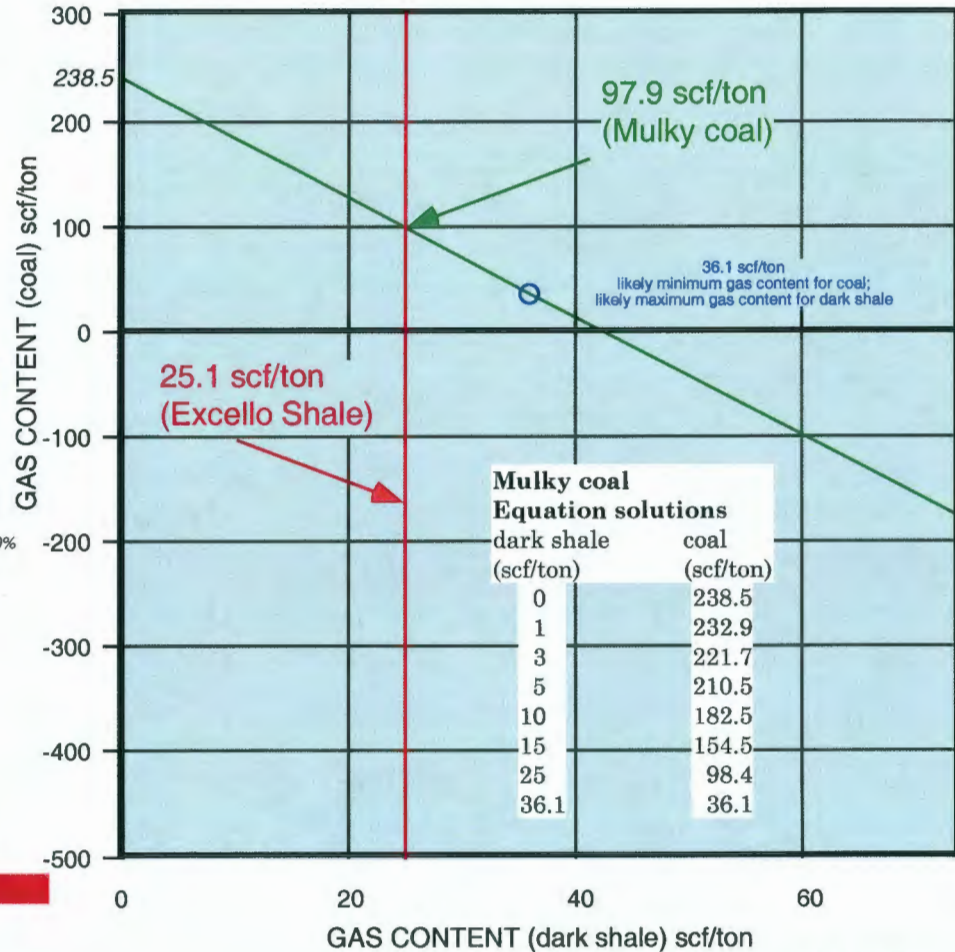
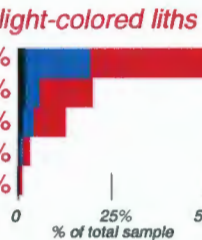


FIGURE 5.

# Desorption Characteristics of Cuttings Samples

Layne Energy Operating, L.L.C. #8-4 Tincknell, E2 SE NE 4-T.31S.-R.17E., Montgomery Co., KS

LITHOLOGIC COMPONENT SENSITIVITY ANALYSIS for calculation of gas content of Croweburg coal from 709' to 710'

$$\text{GAS CONTENT}_{\text{coal}} = \frac{\text{total gas desorbed} - ((\text{gas content}_{\text{dark shale}}) * (\text{weight}_{\text{dark shale}}))}{\text{weight}_{\text{coal}}}$$

total gas desorbed  
(including estimated lost gas) = 1260.8 ccs

TOTAL DRY WEIGHT OF SAMPLE = 930.47 grams

weight<sub>light-colored lithologies</sub> = 470.18 grams (50.5%)  
weight<sub>dark shale</sub> = 403.35 grams (43.4%)  
weight<sub>coal</sub> = 56.94 grams (6.1%)

sieve size	grams	% coal / % dark shale / % light-colored liths
>0.0930"	568.78	4.57% / 33.71% / 61.72%
>0.0661"	190.48	10.60% / 51.37% / 38.03%
>0.0460"	122.54	7.07% / 66.24% / 26.69%
>0.0331"	35.50	4.81% / 65.78% / 29.41%
<0.0331"	13.17	3.00% / 70.00% / 27.00%
<b>930.47 TOTAL</b>		

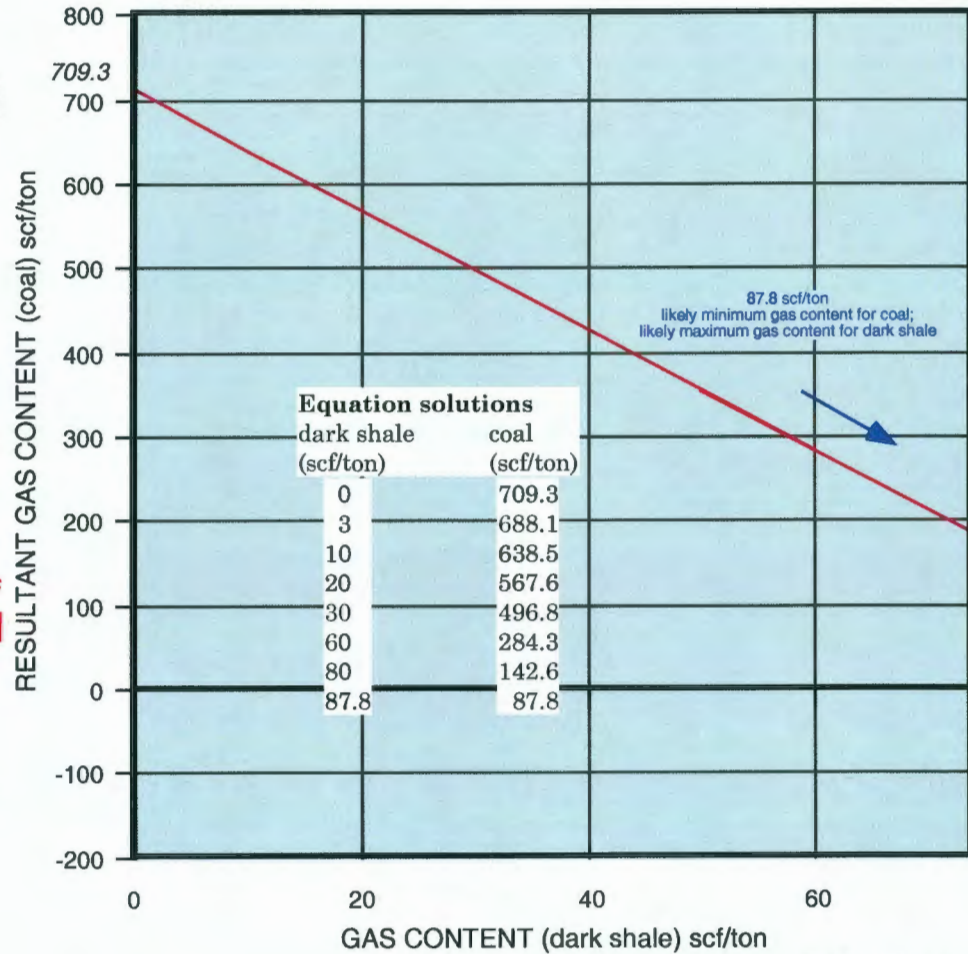
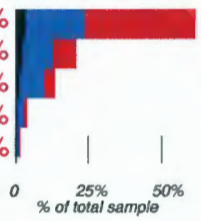


FIGURE 6.

# Desorption Characteristics of Cuttings Samples

Layne Energy Operating, L.L.C. #8-4 Tincknell, E2 SE NE 4-T.31S.-R.17E., Montgomery Co., KS

LITHOLOGIC COMPONENT SENSITIVITY ANALYSIS for calculation of gas content of Mineral coal from 746' to 748'

$$\text{GAS CONTENT}_{\text{coal}} = \frac{\text{total gas desorbed} - ((\text{gas content}_{\text{dark shale}}) * (\text{weight}_{\text{dark shale}}))}{\text{weight}_{\text{coal}}}$$

total gas desorbed  
(including estimated lost gas) = 948.3 ccs

TOTAL DRY WEIGHT OF SAMPLE = 697.83 grams

weight<sub>light-colored lithologies</sub> = 250.49 grams (35.9%)

weight<sub>dark shale</sub> = 279.37 grams (40.0%)

weight<sub>coal</sub> = 167.97 grams (24.1%)

sieve size	grams	% coal / % dark shale / % light-colored liths
>0.0930"	325.20	30.91% / 38.04% / 31.05%
>0.0661"	167.17	25.85% / 40.04% / 34.11%
>0.0460"	140.18	15.34% / 42.48% / 42.18%
>0.0331"	43.93	5.36% / 43.45% / 51.19%
<0.0331"	21.35	1.82% / 47.27% / 50.91%
<b>697.83 TOTAL</b>		

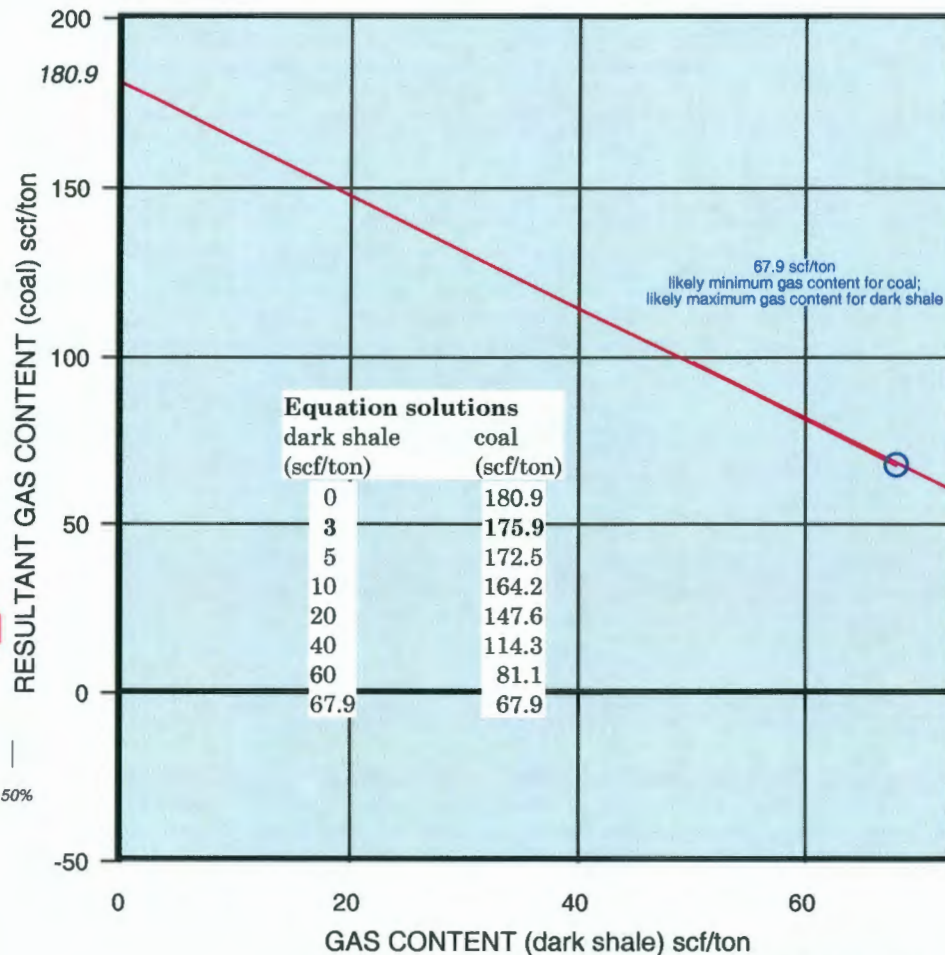
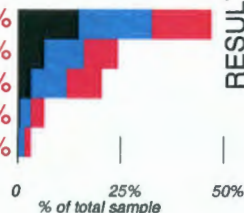


FIGURE 7.

# Desorption Characteristics of Cuttings Samples

Layne Energy Operating, L.L.C. #8-4 Tincknell, E2 SE NE 4-T.31S.-R.17E., Montgomery Co., KS

LITHOLOGIC COMPONENT SENSITIVITY ANALYSIS for calculation of gas content of lower Weir coal from 877' to 878'

$$\text{GAS CONTENT}_{\text{coal}} = \frac{\text{total gas desorbed} - ((\text{gas content}_{\text{dark shale}}) * (\text{weight}_{\text{dark shale}}))}{\text{weight}_{\text{coal}}}$$

total gas desorbed  
(including estimated lost gas) = 218.6 ccs

TOTAL DRY WEIGHT OF SAMPLE = 1999.72 grams

weight<sub>light-colored lithologies</sub> = 289.05 grams (14.5%)

weight<sub>dark shale</sub> = 1634.20 grams (81.7%)

weight<sub>coal</sub> = 76.48 grams (3.8%)

sieve size	grams	% coal / % dark shale / % light-colored liths
>0.0930"	1658.66	3.64% / 84.70% / 11.66%
>0.0661"	210.82	3.84% / 70.84% / 25.32%
>0.0460"	101.77	6.29% / 61.98% / 31.74%
>0.0331"	20.29	6.15% / 56.92% / 36.92%
<0.0331"	8.18	5.00% / 65.00% / 30.00%

1999.72 TOTAL

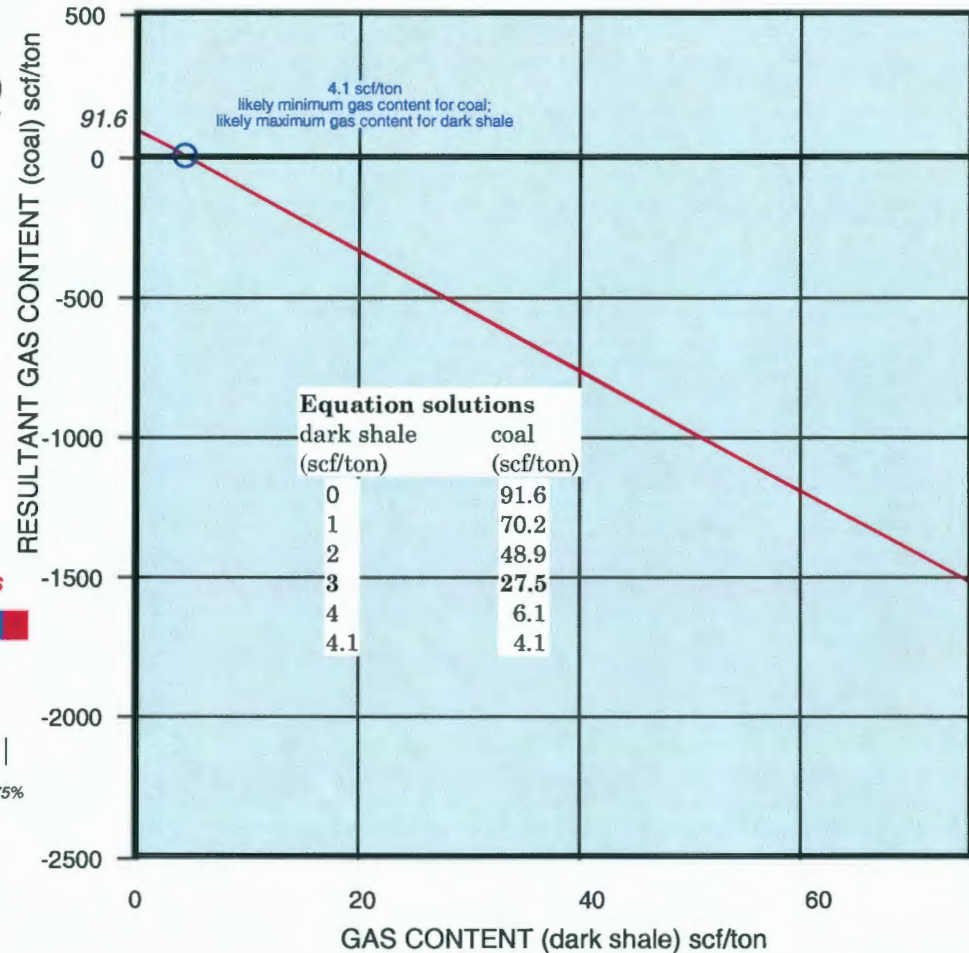
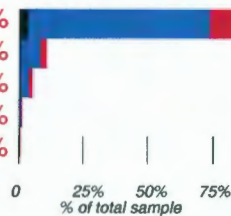


FIGURE 8.

# Desorption Characteristics of Cuttings Samples

Layne Energy Operating, L.L.C. #8-4 Tincknell, E2 SE NE 4-T.31S.-R.17E., Montgomery Co., KS

surface

LITHOLOGIC COMPONENT SENSITIVITY ANALYSIS for all samples

100'	UNIT	coal in sample	scf/ton w/ shale @ 3 scf/ton	maximum scf/ton	minimum scf/ton
200'	Little Osage Shale	0%	----	----	10.5
300'	Excello Shale	0%	----	----	25.1
	Mulky	4%	221.7	238.5	36.1
	Iron Post	----	no valid data		
400'	Croweburg	6%	688.1	709.3	87.8
	Flemming	----	no valid data		
	Mineral	24%	175.9	180.9	67.9
500'	lower Weir	4%	27.5	91.6	4.1
600'	<ul style="list-style-type: none"> <li>○ 624'-625' Little Osage Shale</li> <li>○ 646'-650' Excello Shale</li> <li>○ 651'-652' Mulky</li> <li>○ 680'-682' Iron Post</li> <li>○ 709'-710' Croweburg</li> <li>○ 718'-719' Flemming</li> <li>○ 746'-748' Mineral</li> </ul>				
800'	<ul style="list-style-type: none"> <li>○ 877'-878' lower Weir</li> </ul>				

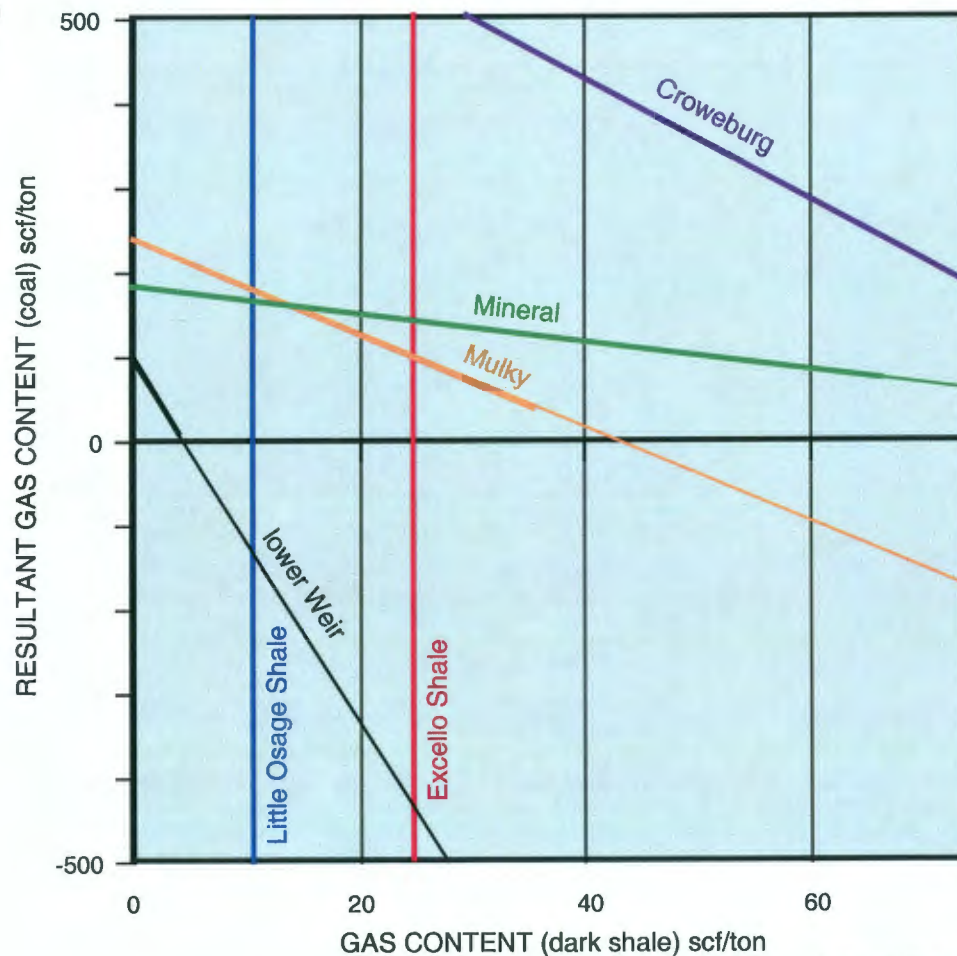


FIGURE 9.

# Desorption Characteristics of Cuttings Samples

based on total weight of gas-generating lithologies (i.e., coal and dark shale) in sample  
 Layne Energy Operating, L.L.C. #8-4 Tincknell, E2 SE NE 4-T.31S.-R.17E., Montgomery Co., KS

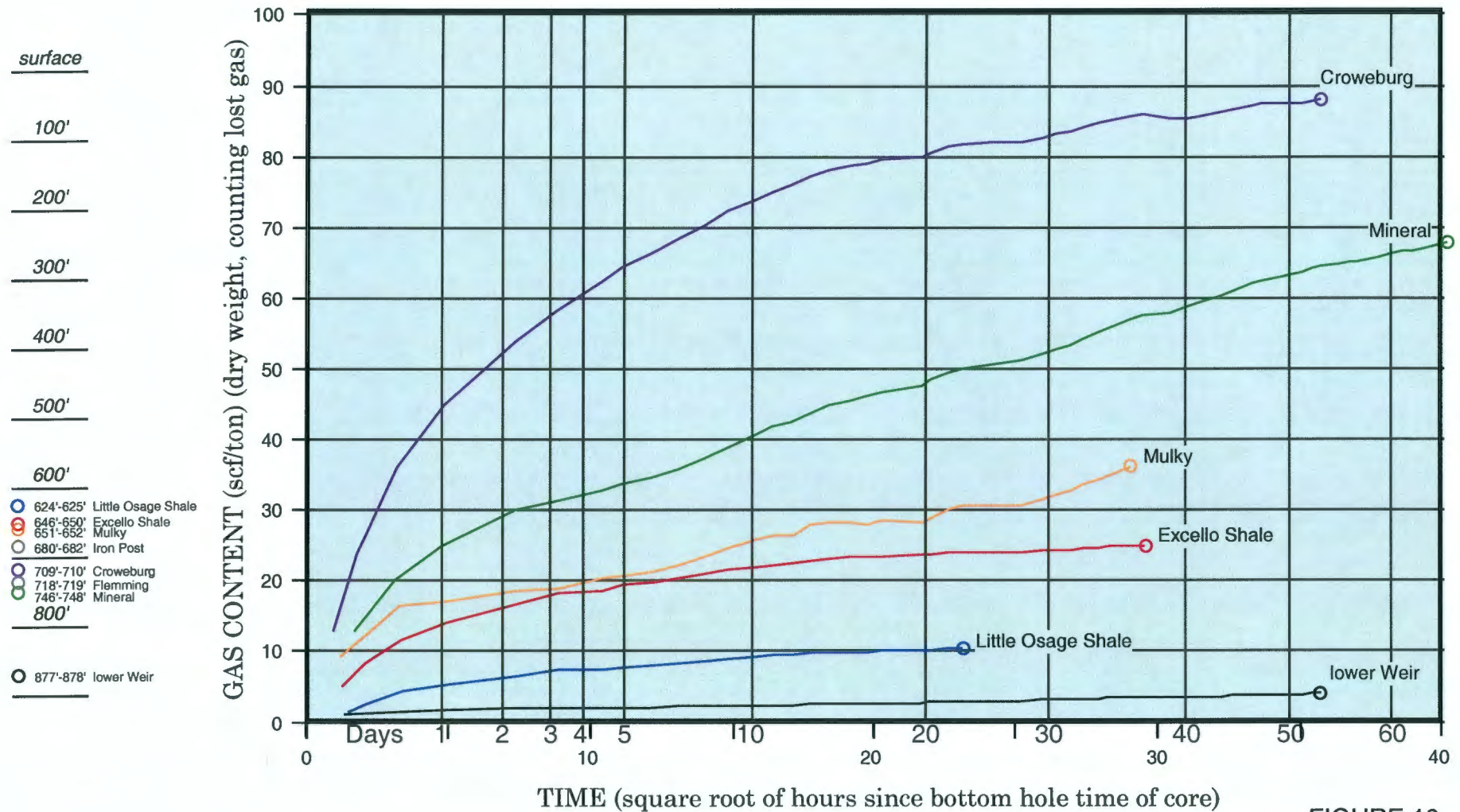


FIGURE 10.