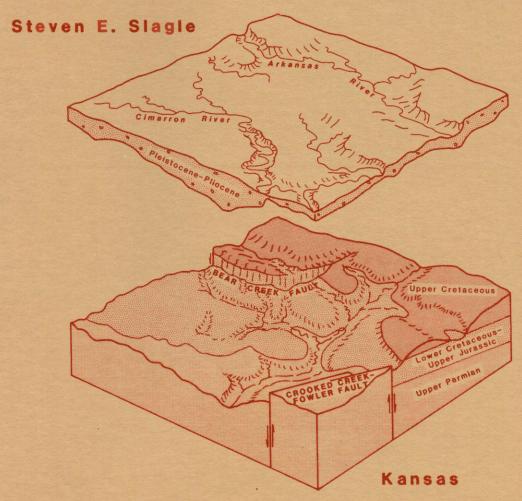
GEOHYDROLOGY OF SOUTHWESTERN KANSAS

Edwin D. Gutentag

David H. Lobmeyer



Geological Survey
Irrigation Series 7

Prepared by the
U.S. GEOLOGICAL SURVEY
in cooperation with the
KANSAS GEOLOGICAL SURVEY

KANSAS GEOLOGICAL SURVEY IRRIGATION SERIES 7

GEOHYDROLOGY OF SOUTHWESTERN KANSAS

Ву

Edwin D. Gutentag, David H. Lobmeyer, and Steven E. Slagle
U.S. Geological Survey, Lawrence, Kansas

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ABSTRACT

The study area includes about 8,900 square miles in 11 counties of south-western Kansas. This is one of the principal areas of ground-water development for irrigation in the State. The area is flat to gently rolling and is drained by the Arkansas and Cimarron Rivers. Mean annual precipitation at Sublette is 19.45 inches.

Consolidated rocks underlie the area in a broad northeast-trending syncline. This structure is bounded by major faults on the northwest and southeast. The surface of the bedrock, which may be on Permian, Jurassic, or Cretaceous rocks, defines the lower limit of the principal aquifer in the unconsolidated deposits.

Minor amounts of water for irrigation use are available from gypsum in Upper Permian rocks, sandstones in Upper Jurassic and Lower Cretaceous rocks, and chalk in Upper Cretaceous rocks. The principal sources of water used for irrigation are the sand and gravel layers in Pliocene and Pleistocene deposits and in Quaternary alluvium in the stream valleys. These sand and gravel layers, collectively termed the unconsolidated aquifer, underlie about 75 percent of southwestern Kansas.

In the main part of the unconsolidated aquifer, saturated thicknesses range from less than 50 feet to about 630 feet, and yields to irrigation wells commonly range from 500 to 1,500 gallons per minute. The total quantity of water available for pumping was estimated in 1975 to be 105 million acre-feet. The chemical quality of water in the aquifer ranges from a calcium bicarbonate type to a sodium chloride type.

The number of irrigation wells in southwestern Kansas has increased from 420 in 1945 to about 7,000 in 1975, and irrigated land has increased from 124,000 acres in 1950 to 1,400,000 acres in 1975. Since 1940, pumpage of about 14 million acre-feet of water from storage has resulted in water-level declines ranging from 0 to 135 feet. Saturated thicknesses have decreased as much as 60 percent in a few areas and have decreased a median of 8 percent within the main part of the aguifer.

INTRODUCTION

Purpose and Scope of Investigation

Southwestern Kansas is one of the principal areas of ground-water development for irrigation in the State, and many reports are available concerning ground-water conditions in the area. The purposes of this investigation were to consolidate and update data, to determine the extent and effects of irrigation development on the ground-water resource, to determine the chemical quality of the ground water in relation to irrigation use, to describe the general operation of the hydrologic system, and to identify problem areas where intensive quantitative studies will be needed by State and local agencies for planning and management of the resource. This study began in 1972 as part of a cooperative program of ground-water investigations between the Kansas Geological Survey and the U.S. Geological Survey. Support in this study was provided by the Division of Water Resources of the Kansas State Board of Agriculture and the Division of Environment of the Kansas Department of Health and Environment.

Location and Extent of the Area

The study area (fig. 1) includes Finney, Grant, Gray, Hamilton, Haskell, Kearny, Meade, Morton, Seward, Stanton, and Stevens Counties in southwestern Kansas. The total area is about 8,900 square miles (Institute for Social and Environmental Studies, 1971).

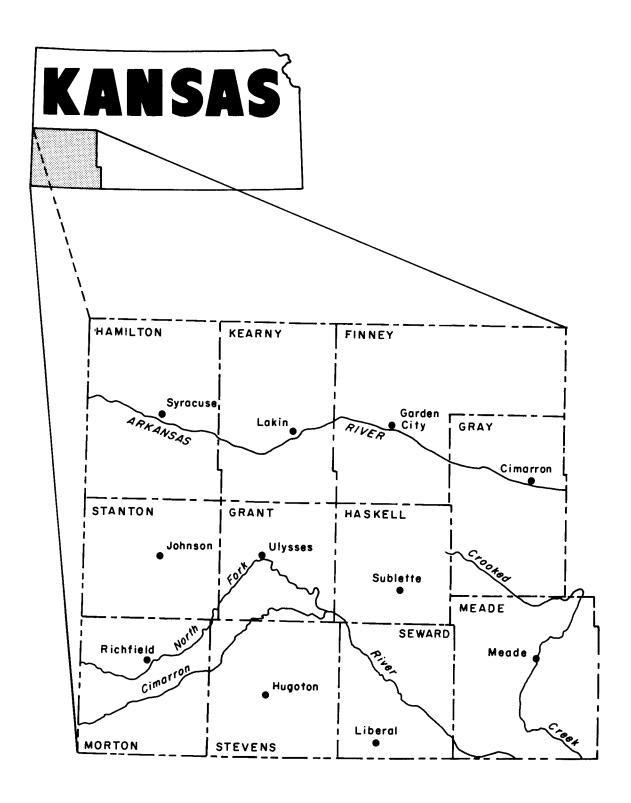


Figure 1.--Location of report area.

Previous Investigations

There are many studies dealing with geology and water resources in the study area. Early studies from 1897 to 1940 are listed by Smith (1940).

The historical data for this report were obtained from studies of the ground-water resources that began in 1937 in cooperation with the Kansas Geological Survey. These studies were reported as follows: Finney and Gray Counties by Latta (1944); Grant, Haskell, and Stevens Counties by McLaughlin (1946); Hamilton and Kearny Counties by McLaughlin (1943); Meade County by Frye (1942); Morton County by McLaughlin (1942); Seward County by Bryne and McLaughlin (1948); and Stanton County by Latta (1941).

Additional cooperative studies were made in southwestern Kansas after irrigation development. These studies were made as follows: Finney County by Meyer and others (1970) and by Gutentag and others (1972); Grant and Stanton Counties by Fader and others (1964); Gray County by McGovern and Long (1974); Hamilton County by Lobmeyer and Sauer (1974); Haskell County by Gutentag and Stullken (1974); and Kearny County by Gutentag and others (1972).

Well-Numbering System

The well numbers in this report give the location of wells and test holes according to the Bureau of Land Management's system of land subdivision. This method of well and test-hole location is shown in figure 2. The first number indicates the township; the second number indicates the range west of the sixth principal meridian; and the third indicates the section in which the well or test hole is situated. Letters following the section number locate the well within the section. The first letter denotes the quarter section or 160-acre tract; the second letter, the quarter-quarter section or 40-acre tract; the third letter, the quarter-quarter section or 10-acre tract.

These tracts are designated A, B, C, and D in a counterclockwise direction beginning in the northeast quadrant. Where two or more wells are located in a 10-acre tract, wells are numbered serially, beginning with 2, according to the order in which they were recorded. For example, 28-37W-10BCD2 indicates that this is the second well or test hole recorded in the SE1/4SW1/4NW1/4 sec.10, T.28 S., R.37 W., Grant County.

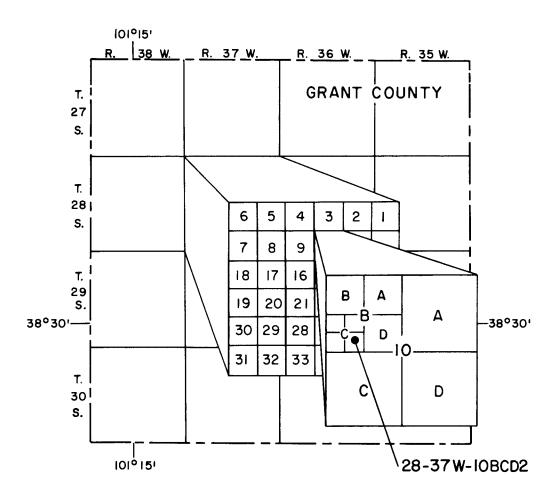


Figure 2.--System of numbering wells and test holes in Kansas.

Metric Units

The inch-pound units of measurement given in this report are listed with equivalent International System(SI) of Units using the following abbreviations and conversion factors:

Inch-pound unit	Multiply by	SI unit
Inch (in)	2.54	Centimeter (cm)
Foot (ft)	0.3048	Meter (m)
Mile (mi)	1.609	Kilometer (km)
Square foot (ft ²)	0.0929	Square meter (m ²)
Acre	0.4047	Square hectometer (hm ²)
Square mile (mi ²)	2.590	Square kilometer (km²)
Gallon (gal)	3.785	Liter (L)
Cubic foot (ft ³)	0.02832	Cubic meter (m ³)
Acre-foot (acre-ft)	0.001233	Cubic hectometer (hm^3)
Gallon per minute (gal/min)	0.06309	Liter per second (L/s)
Cubic foot per second (ft^3/s)	0.02832	Cubic meter per second (m ³ /s)
Foot per day (ft/d)	0.3048	Meter per day (m/d)
<pre>Gallon per minute per foot [(gal/min)/ft]</pre>	0.207	Liter per second per meter [(L/s)/m]
Foot per mile (ft/mi)	0.1894	<pre>Meter per kilometer (m/km)</pre>

Acknowledgments

The authors wish to thank the land owners and farm operators for their cooperation, especially those who permitted the use of their wells or allowed test drilling on their property. Acknowledgment is given to Howard Corrigan, Water Commissioner, Division of Water Resources, Kansas State Board of Agriculture, for his help in this study. Acknowledgment also is given to the District Conservationists of the Soil Conservation Service and the County Executive Directors of the Agricultural Stabilization and Conservation Service who helped in the location of wells and irrigated acreage.

GEOLOGIC FRAMEWORK

Stratigraphy

A primary consideration in a geohydrologic study is the stratigraphic relation of beds that are water bearing to beds that are not water bearing (see table 1).

The oldest beds considered in the study are those of the Lower Permian Blaine Formation, which are easily identified on geophysical logs and are usable in the interpretation of regional structure. The relation of Upper Permian rocks to the geohydrology is significant because the rocks contain highly mineralized water. Upper Jurassic and Lower Cretaceous rocks underlying most of the area contain water-yielding zones and are in hydraulic connection with younger deposits. Upper Cretaceous rocks in the northern part of the area yield little water and retard the movement of vertical flow. Tertiary and Quaternary deposits underlie most of the area and are the principal water-yielding beds in south-western Kansas.

Geologic Structure

Southwestern Kansas lies in a broad marginal syncline on the east side of the Las Animas Arch (Merriam, 1963). The syncline plunges to the northeast away from the Sierra Grande uplift in southeastern Colorado. The top of the Blaine Formation, as shown by a structure map (fig.3), slopes 14.5 feet per mile from the southwestern corner of Morton County to the north-central part The regional structure is cut by two faults that define of Finney County. the northwestern and southeastern limits of the principal aquifer in the unconsolidated deposits. These faults (the Bear Creek Fault in Hamilton, Stanton, Grant. and Kearny Counties and the Crooked Creek-Fowler Fault in Meade County), which are the result of the dissolution and removal by ground water of evaporites within and just below the Blaine Formation, have a vertical displacement The Crooked Creek and Fowler Faults previously have of as much as 250 feet. been considered separately as individual faults (Frye and Schoff, 1942). Present data indicate that the Fowler Fault and the Crooked Creek Fault are part of the same zone of dissolution and collapse. Therefore, it is recommended here that the fault be named the Crooked Creek-Fowler Fault. The Bear Creek and Crooked Creek-Fowler Faults are partially defined on the present land surface by a line of sinkholes and filled sinks.

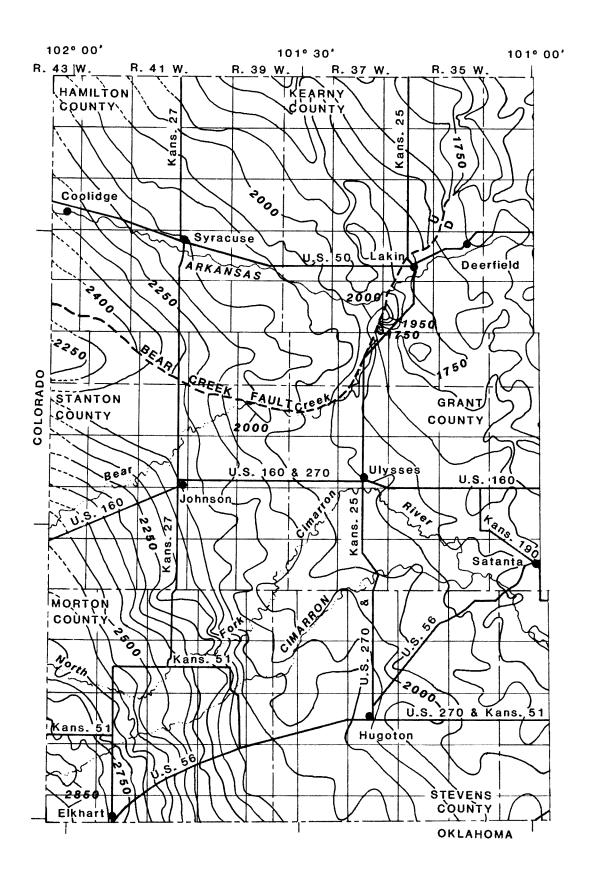
Numerous other structural features are evident on the Blaine surface. A syncline in northwestern Kearny County may be traced for about 15 miles. Small, poorly defined structural features, which may be minor faults, also occur in northwestern Haskell and southwestern Finney Counties. Some of these structural features may have influenced the drainage system during erosion of the bedrock surface and subsequent deposition of the overlying unconsolidated deposits.

Table 1.--Generalized section of geologic formations and their water-bearing properties*

				TOTAL MANAGEMENT AND ADMINISTRATION OF THE PROPERTY OF THE PRO	
System	Series	Stratigraphic unit	Thickness, feet	Physical character	Water supply
		Alluvium	0-80	Stream-laid deposits ranging from silt and clay to sand and gravel that occur along principal stream valleys.	Yields to wells range from 500 to more than 1,000 gal/min in the Arkansas River valley; 50 to 500 gal/min in the Pawnee River valley; and 50 to 1,000 gal/min in the Cimarron River valley.
Quaternary	Pleistocene	Dune sand	0-75	Fine to medium quartzose sand with small amounts of clay, silt, and coarse sand formed into mounds and ridges by the wind.	Lies above the water table and does not yield water to wells. The sand has a high infiltration rate and is important as area of groundwater recharge.
		Loess	0-45	Silt with subordinate amounts of very fine sand and clay deposited as windblown dust.	Lies above the water table and does not yield water to wells. Serves as minor area of ground-water recharge.
		Undifferentiated deposits	0-550	Sand, gravel, silt, clay, and caliche overlie Ogallala Formation when both formations are present; composite of stream-lain and windblown deposits.	The sand and gravel of the undiffer- entiated Pleistocene deposits and
Tertiary	Pliocene	Ogallala Formation	0-200	Poorly sorted clay, silt, sand, and gravel generally calcareous; when cemented by calcium carbonate, forms caliche layers or mortar beds.	the Ugallala Formation are the principal water-bearing deposits in the area. Yields range from 100 to 3,100 gal/min.
		Niobrara Chalk	0-250	Upper unit (Smoky Hill Chalk Member)yellow to orange-yellow chalk and light- to dark-gray beds of chalky shale. Lower unit (Fort Hays Limestone Member)consists of a white to yellow massive chalky limestone; contains thin beds of dark-gray chalky shale.	Initially (1968-72), yielded 500 to 2,500 gal/min to wells in northern Finney and eastern Kearny Counties where the Fort Hays Limestone Member has been honeycombed by fractures and solution openings. Because of increased irrigation development, yields have been reduced by 100 to as much as 2,000 ral/min
	Upper Cretaceous	Carlile Shale	0-330	Upper part consists of a dark-gray to blue-black noncalcareous to slightly calcareous shale that locally is interbedded with calcareous silty very fine-grained sandstone. Lower part consists of very calcareous dark-gray shale and thin gray interbedded limestone layers.	Sandstone in upper part may yield 5 to 10 gal/min to wells.
Cretaceous		Greenhorn Limestone	0-200	Chalky light yellow-brown shale with thin-bedded limestone. Dark-gray calcareous shale and light-gray thin-bedded limestone; contains layers of bentonite.	Not known to yield water to wells in southwestern Kansas.

		Graneros Shale	0-130	Dark-gray calcareous shale interbedded with black calcareous shale; contains thin beds of bentonite. Also contains thin-bedded gray limestone and finegrained silty sandstone layers.	Not known to yield water to wells in southwestern Kansas.
	Lower Cretaceous	Undifferentiated	0-450	Upper unit (Dakota Formation)—-brown to gray fineto medium-grained sandstone; interbedded with gray sandy shale and varicolored shale; contains lignite lenses (0-160 feet). Middle unit (Kiowa Formation)—dark-gray to black shale; interbedded with light yellow-brown and gray sandstone (0-150 feet). Lower unit (Cheyenne Sandstone)—-gray and brown very fineto medium-grained sandstone; interbedded with darkgray shale (0-125 feet).	The sandstone units commonly yield from 50 to 500 gal/min to wells. Yields of more than 1,000 gal/min are reported in a few areas. Water may be more mineralized in the lower unit than in the upper unit.
Jurassic	Upper Jurassic	Undifferentiated	0-350	Dark-gray shale; interbedded with grayish-green and bluish-green calcareous shale. Contains very fineto medium-grained silty sandstone and some thin limestone beds at the base.	In Morton and Stanton Counties, sandstone beds are yielding in combination with the overlying Lower Cretaceous units. In the northernmost counties where the aquifer is deepest, the water may be mineralized.
	Upper	Big Basin Formation	0-160	Brick-red to maroon siltstone and shale; contains very fine-grained sandstone.	Where not highly mineralized, may yield small quantities of usable water for domestic and stock purposes.
	Permian	Day Creek Dolomite	0-80	White to pink anhydrite and gypsum; contains interbedded dark-red shale.	Solution cavities have yielded large quantities (300 to 1,000 gal/min) of high sulfate water to wells in Morton County.
Permian		Whitehorse Formation	100-350	Red to maroon fine-grained silty sandstone, silt- stone, and shale.	Fresh to highly mineralized water. Not known to yield significant amounts of water to wells in south- western Kansas.
	Lower	Dog Creek Formation	15-60	Maroon silty shale, siltstone, very fine sandstone, and thin layers of dolomite and gypsum.	Not known to vield cianificant
	D	Blaine Formation	20-150	Generally consists of four gypsum and anhydrite beds separated by red shale; contains bedded ha- lite at some sites.	amounts of water to wells in south- western Kansas. Water probably highly mineralized.

* The classification and nomenclature of the stratigraphic units used in this report are those of the Kansas Geological Survey and differ somewhat from those of the U.S. Geological Survey.



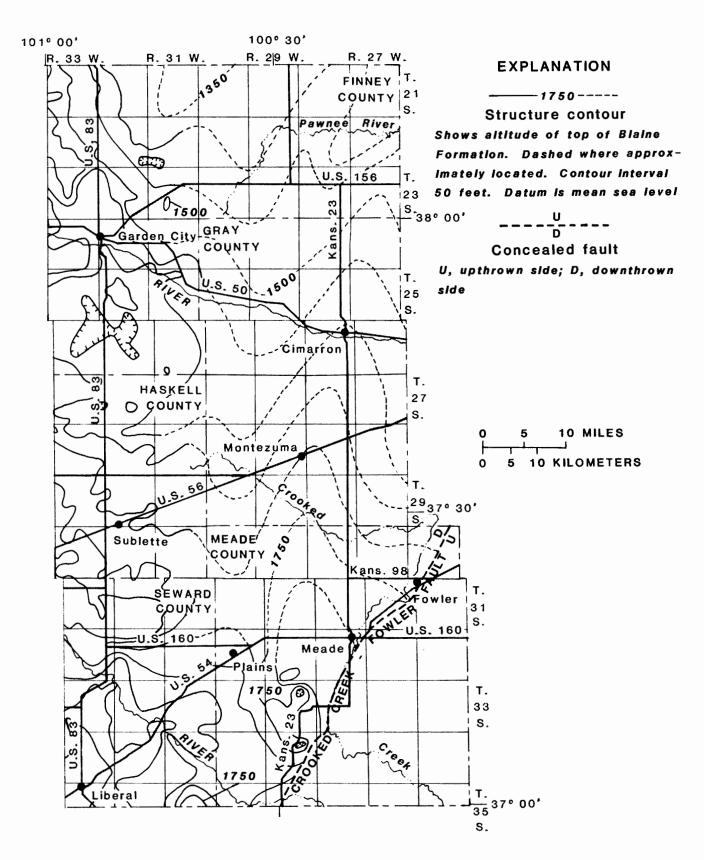


Figure 3.--Structure contours on top of the Blaine Formation.

Permian Surface

The configuration of the Permian surface (fig. 4) shows general patterns of folding, faulting, and sculpturing by post-depositional events. The general slope of the Permian surface is 15.4 feet per mile in a northeasterly direction. A period of erosion occurred prior to the deposition of the Upper Jurassic and Lower Cretaceous rocks upon the Permian surface. In parts of Haskell, Meade, Morton, Seward, and Stevens Counties, the Permian surface underwent additional erosion prior to deposition of Tertiary and Quaternary deposits. Thus, the Permian surface converges toward the top of the Blaine Formation, and the distance between these surfaces varies from slightly over 600 feet in southwestern Morton County to less than 150 feet in northeastern Finney County and southcentral Meade County. The Permian surface is formed on the Whitehorse Formation, the Day Creek Dolomite, and the Big Basin Formation.

Bedrock Surface

Consolidated rocks of Late Permian to Late Cretaceous age, which underlie the unconsolidated deposits of Tertiary and Quaternary age, are referred to as bedrock in this report. The bedrock surface, as shown in plate 1, is an erosional surface influenced and modified by structure, with an average slope of 13.7 feet per mile toward the southeast. The local relief, which may be as much as 250 feet, is the result of erosion in Seward and Stevens Counties and of subsidence along the Bear Creek and Crooked Creek-Fowler Faults. In contrast, the bedrock surface in central Haskell County is nearly flat.

The bedrock surface in the southern part of the area is formed on Permian rocks and is coincident with the Permian surface. In the central part, the bedrock surface is formed on stratigraphically younger undifferentiated rocks of Late Jurassic and Early Cretaceous age. The bedrock surface in the northern part of the study area is formed on rocks of Late Cretaceous age. The comparative altitudes of the various formations as they subcrop on this bedrock surface generally indicate a northeast dip of the bedrock units.

Surface Topography

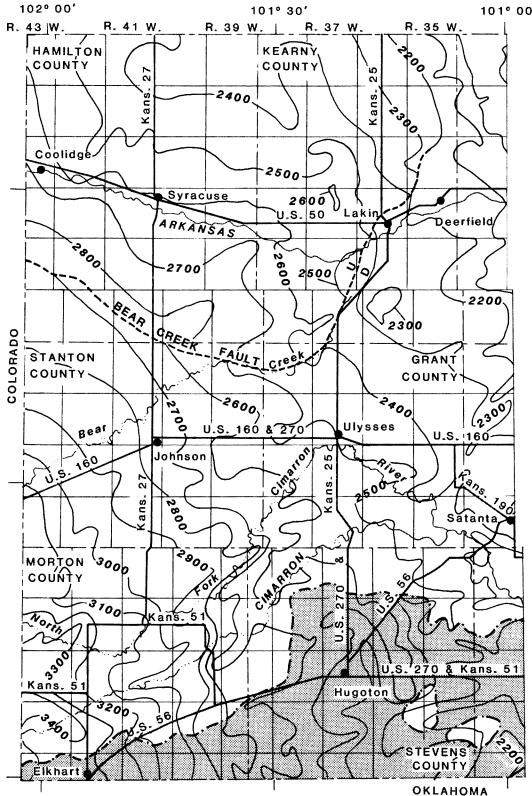
Southwestern Kansas lies in the High Plains section of the Great Plains physiographic province (Fenneman, 1931) and is part of the broad treeless plain that slopes gently eastward from the Rocky Mountain front. In the study area, altitudes of the land surface range from about 3,850 feet in the northwestern corner of Hamilton County to 2,150 feet along the Cimarron River in the southeastern corner of Meade County. The prevailing slope on the topographic surface is about 12.5 feet per mile in a southeasterly direction.

HYDROLOGY

Ground-Water Occurrence

Bedrock Aquifers

The bedrock aquifers are the gypsum aquifer in Upper Permian rocks, the sandstone aquifer in the Upper Jurassic and Lower Cretaceous rocks, and the chalk aquifer in Upper Cretaceous rocks. These aquifers differ from the unconsolidated aquifer in that they generally lie at a greater depth, are more difficult to drill, contain water that generally is under artesian head, commonly contain more highly mineralized water, and generally will not sustain large yields.



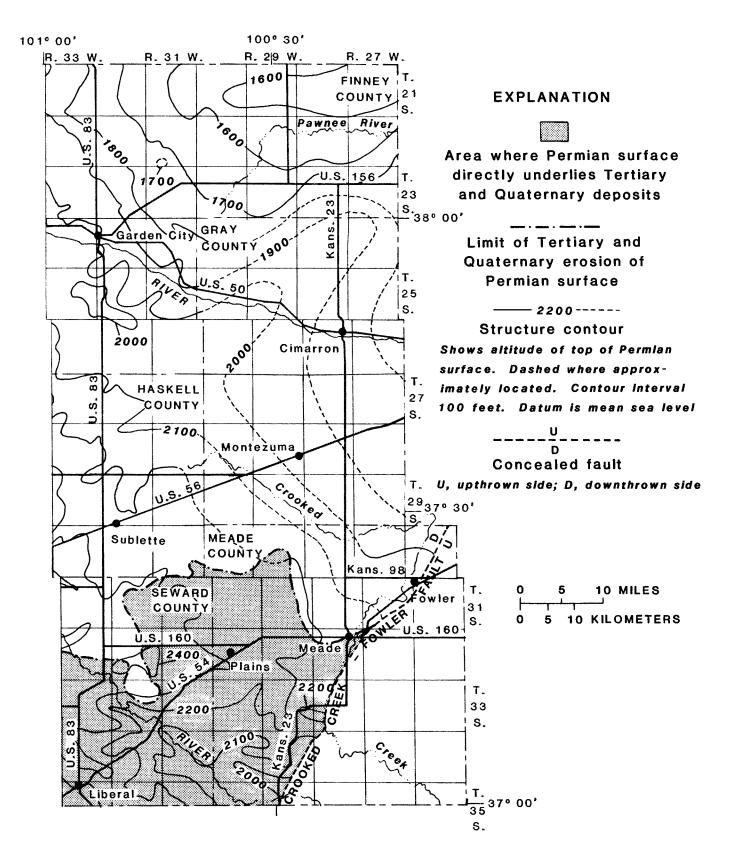


Figure 4.--Configuration of top of the Permian surface.

Gypsum Aquifer.--The gypsum aquifer is defined here as the highly permeable zones within the Upper Permian Day Creek Dolomite. In Morton County, the gypsum aquifer consists of locally cavernous white to pink anhydrite and gypsum that are interbedded with dark-red shale. The presence of cavities commonly is indicated by a suddendrop of the drill stem and a loss in circulation of fluid during drilling. Stock and irrigation wells, which tap the Day Creek, pump from water-filled solution cavities in the evaporite deposits. Depth of the Day Creek below land surfaces ranges from about 200 feet in the southwestern part of Morton County near the Cimarron River to about 800 feet in northeastern Morton County. The gypsum aquifer has been tapped only in central Morton County, where solution cavities yield 300 to 1,000 gal/min. Because water from wells in the Day Creek is highly mineralized, utilization of this water for irrigation is limited (see section on "Quality of Water for Irrigation").

<u>Sandstone Aquifer.</u>—The sandstone aquifer, as used in this report, refers to the permeable sandstone beds contained throughout the Upper Jurassic and Lower Cretaceous rocks in southwestern Kansas. The sandstone beds within the two rock units are discontinuous, and thicknesses differ greatly from one area to another.

Upper Jurassic rocks consist chiefly of red siltstone interbedded with buff, green, and white sandstone. The rocks are similar in lithology and probably are equivalent to the Entrada Sandstone and Morrison Formation of southeastern Colorado (Voegeli and Hershey, 1965).

Lower Cretaceous rocks, which contain the sandstone aquifer, are comprised of the Cheyenne Sandstone, the Kiowa Formation, and the Dakota Formation. The Cheyenne Sandstone consists of a white to rust-colored fine-to coarse-grained quartzose sandstone. The Kiowa Formation generally consists of a dark-gray to black silty shale containing calcareous shale lenses and interbedded sandy

siltstone, fine sandstone, and tan calcareous shale. Where the Kiowa Formation consists predominantly of sandstone beds, it is difficult to distinguish from the underlying Cheyenne Sandstone or the overlying sandstone beds of the Dakota Formation. The Dakota Formation in most areas consists of fine- to medium-grained reddish-brown to yellowish-brown ferruginous sandstone that contains yellow and gray silty shale beds.

Only the loose to slightly cemented sandstone beds in the sandstone aquifer contain significant amounts of recoverable water. Locally, the silty or tightly cemented sandstone beds yield only enough water to wells in the aquifer for domestic or stock supplies. In areas where the sandstone beds are loosely cemented, such as northeastern Finney County, yields of more than 1,000 gal/min have been obtained from the aquifer by irrigation wells. In other areas of Grant, Morton, and Stanton Counties, many multiple-aquifer wells obtain part of their yield from the sandstone aquifer.

Chalk Aquifer. -- The chalk aquifer is defined as that part of the Niobrara Chalk that contains saturated fractures and solution openings. Because the occurrences of fractures and solution openings are irregular, it is difficult to predict the occurrence of water. A well drilled in limestone or chalk must penetrate a sufficient amount of water-filled fractures or solution openings to provide an adequate yield. Therefore, it is commonly necessary to drill several test holes to locate a well that will yield enough water for the intended use.

In northern Finney County and eastern Kearny County, about 45 irrigation wells produce water, solely or in part, from several zones of fractures and solution openings in the Fort Hays Limestone Member (lower unit of the Niobrara Chalk). In the area where the zones of fractures and solution openings are productive, the Fort Hays subcrops beneath the Tertiary and Quaternary deposits. These 1- to 2-foot zones occur approximately 20 feet and 40 feet above the

contact with the underlying Carlile Shale. It is possible that similar saturated fractures and solution openings in the Fort Hays Limestone Member also may be found near the Fort Hays-Carlile contact in northern Hamilton and Kearny Counties. However, the potential for large yields is not indicated in these areas.

Initial yields (1968-72) of 500 to 2,500 gal/min were available to wells from the Fort Hays Limestone Member in northern Finney and eastern Kearny Counties. Because of irrigation development and lowering water levels, well yields (1976) have been reduced 100 to 2,000 gal/min.

The data indicate that the fractures and solution openings in the Niobrara Chalk are limited both in thickness and in areal extent and that water is transported only short distances. The fractures and solution openings are hydraulically connected and obtain their water supply from the overlying thinly saturated (less than 10 feet) Ogallala and undifferentiated Pleistocene deposits.

Unconsolidated Aquifer

The saturated part of the Ogallala Formation of Pliocene age, the undifferentiated Pleistocene deposits, and the Quaternary alluvium are defined here as the unconsolidated aquifer. These unconsolidated deposits, which comprise the aquifer in southwestern Kansas, consist of a heterogeneous assortment of alluvial sediments. Individual beds of silt, clay, sand, gravel, and caliche may be correlated with confidence only for short distances.

Yields differ from one area to another owing to the water-producing zones within the aquifer. Coarse sand and gravel deposits, which probably represent channel-fill of a large stream, commonly yield 1,000 to 2,500 gal/min to wells, and yields of as much as 3,000 gal/min have been measured. Coarse sand and gravel interbedded with silt and clay probably represent deposits of num-

erous streams as they migrated laterally across an ancient flood plain. Yields to wells from these deposits may range from about 100 to 1,000 gal/min. In the Arkansas and Cimarron River valleys, very coarse gravel and cobbles interbedded with silt and clay layers yield about 500 to 1,000 gal/min. In the Pawnee River valley, medium to coarse gravel, interbedded with silt and clay layers, yields about 50 to 500 gal/min to wells.

Potentiometric Surface. -- The configuration of the potentiometric surface, which may reflect water levels in unconfined or confined layers of the aquifer, is shown on plate 2. Data on water levels were obtained during the winter (January 1975) when effects of seasonal pumping for irrigation were at a minimum. Many hydrologic features are shown by the shape and slope indicated by contours on this surface. Contours are not shown in areas where water levels are at or near the bedrock surface or are isolated from the main part of the unconsolidated aquifer.

Ground water in the unconsolidated aquifer occurs predominantly under unconfined conditions, although confined conditions may occur locally. When water is withdrawn from a confined layer in the aquifer during the irrigation season, the head declines. Owing to the differences in head, water leaks through the confining layer and results in a water-level decline in the overlying unconfined layer of the aquifer (Gutentag and others, 1972). In the nonirrigation season, the head in the confined layer of the aquifer is increased as water moves into the pumped area from surrounding areas of little or no pumping. In response to the increase in head, water levels rise in the unconfined layer of the aquifer. The difference in heads in the two aquifer layers can be indirectly related to the intensity of withdrawal during the previous pumping season, the vertical hydraulic conductivity and extent of the confining layer, and the duration of time available for recovery during the nonpumping season.

In much of southwestern Kansas, the alluvial deposits are lenticular and heterogeneous. The potentiometric surfaces have not been differentiated with respect to individual aquifer layers because most wells tap all the water-yielding material at a given location. In some areas, wells also may have a contribution from the underlying sandstone aquifer where it is in contact with the unconsolidated aquifer. Water-level data from multiple-aquifer wells used in this study tend to indicate trends in the unconsolidated aquifer because most of the yields are from the unconsolidated aquifer.

The water surface slopes generally eastward across the study area at about 10.5 feet per mile, and the water movement is in that direction. Flattening of the gradient, as indicated by widely spaced contours, probably results from a high hydraulic conductivity of the material through which the water is moving and an increased thickness of water-bearing materials. Areas defined by widely spaced contours, such as southeastern Haskell County, generally are well suited for development of large-capacity wells. An area of apparently flat gradient north of Garden City, however, is the result of a distorted flow pattern caused by very intensive pumping in a localized area.

Closely spaced contours in the study area indicate a steep slope of the potentiometric surface caused by low hydraulic conductivity and reduced thickness of water-bearing materials. A belt of closely spaced contours extends across parts of Grant, Haskell, Seward, and Stevens Counties. Water-well drillers report that fine-grained deposits of low hydraulic conductivity commonly occur in the same areas as those shown by closely spaced contours.

The Cimarron River from the U.S. Highway 83 bridge to the Kansas-Oklahoma State line and the Arkansas River in Gray County are examples of gaining streams because they intercept the water table. Thus, the upstream flexures of the contours show flow toward the streams. The lack of upstream flexures in other

areas where contour lines cross stream valleys indicates that the water table lies below the streambed and that the streams receive no contribution from ground water in those reaches.

Saturated Thickness.--The area of the unconsolidated aquifer underlain by sufficient saturated material to support irrigation is about 6,600 square miles, or about 75 percent of the total 8,900 square miles in southwestern Kansas. This area of saturated material is referred to as the main part of the unconsolidated aquifer, as shown on plate 3. In other parts of the area, the unconsolidated aquifer is extremely thin or absent.

The saturated thickness of the unconsolidated deposits is shown on plate 3. Within the main part of the unconsolidated aquifer, the saturated thickness ranges from less than 50 feet to about 630 feet, with a median saturated thickness of 284 feet. Generally, the areas of greatest saturated thickness coincide with areas where unconsolidated deposits overlie the deepest channels in the bedrock surface. An example is the area in southwestern Seward County.

Saturated thickness may be used as an approximation in locating a possible well site. However, the collective thickness, degree of sorting, and hydraulic conductivity of water-yielding materials within the saturated section are important considerations in developing an irrigation supply. In test drilling for a well site, contractors commonly estimate discharge from the well by assigning arbitrary values of yield per foot of water-yielding material.

The unconsolidated aquifer, in general, has a specific yield (storage coefficient) that reflects unconfined conditions. Results of aquifer tests in in Finney County (Meyers and others, 1970) indicate a range in specific yield of 0.05 to 0.22 and in Haskell County (Gutentag and Stullken, 1976) indicate a range of 0.15 to 0.20.

In some areas of relatively great saturated thickness, the water-yielding layers are separated by numerous fine-grained layers, which result in confined conditions. Early in the development of irrigation in Grant and Stanton Counties, aquifer tests in the principal water-yielding layers indicated storage coefficients that ranged from 0.001 to 0.0001 (Fader and others, 1964). As pumpage for irrigation greatly increased, however, water-level declines reduced the confining effects of the upper layers. Subsequent tests probably would indicate a storage coefficient nearly equal to that of an unconfined aquifer.

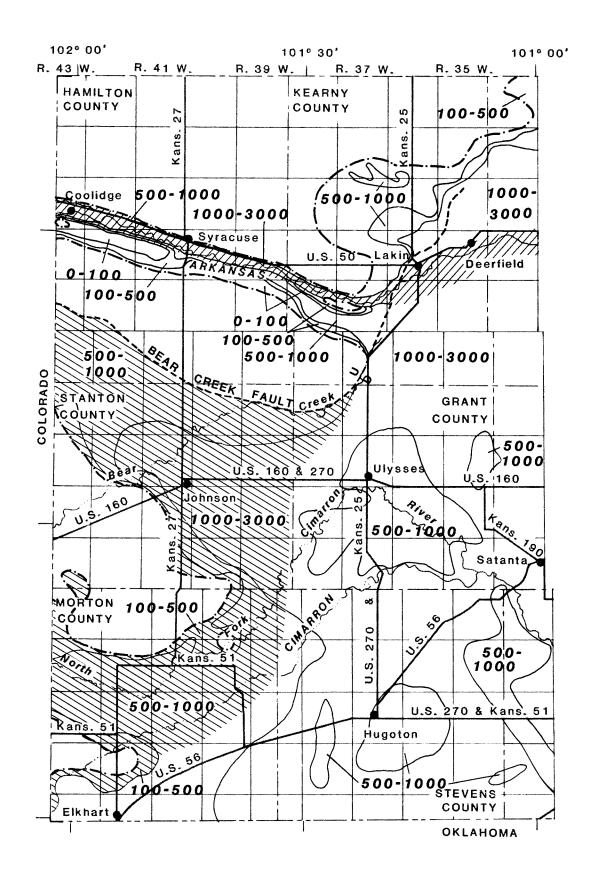
It is estimated that the specific yield for the principal water-yielding zones ranges from 0.15 to 0.20 and that the weighted average for the unconsolidated aquifer would be about 0.15.

The amount of ground water stored in the unconsolidated aquifer in south-western Kansas was determined by computing the area of each saturated thickness interval shown on plate 3, multiplying by the average thickness of each interval, summing the products, and multiplying their summation (total volume) by the specific yield. Assuming that the average specific yield is 0.15 for the whole saturated thickness, the total volume of water in storage in southwestern Kansas is computed to be about 150 million acre-feet as of January 1975. Assuming that only 70 percent of the total volume of water is economically recoverable by wells, approximately 105 million acre-feet are available for pumping.

Potential Yield.—The potential yield, as used in this report, is the calculated quantity that could be pumped from a well when the water-level drawdown is equivalent to 70 percent of the effective thickness of the unconsolidated aquifer. The effective thickness, or aggregate thickness of water-yielding material in the saturated part of the aquifer, probably is the most important factor in estimating well yield.

The map showing the potential yield to wells (fig. 5) was drawn on the basis of driller's well-production tests during which drawdowns were measured at different stages of increasing discharge. The computed potential yield to irrigation wells in the unconsolidated aquifer ranges from less than 100 gal/min to as much as 3,000 gal/min. Potential yields of more than 1,000 gal/min are very speculative, owing to a deficiency in the data available and the method of computing values from well-production tests. The actual yield of an individual well depends on many factors including well construction, method of completion, density of well development in the surrounding area (mutual interference), and transmissivity of the water-yielding deposits at the well site. Because wells normally are designed for irrigation requirements and pump efficiency rather than aquifer potential, the estimated yields are useful chiefly as a general guide in planning. Before selecting a site for installation of a large-capacity well, test drilling is a requisite to ensure the greatest yield for the least pumping lift.

The area delineated as the shallow alluvial aquifer along the Arkansas River indicates the location of Quaternary alluvium where large quantities of ground water may be obtained in addition to the quantities indicated for the principal part of the unconsolidated aquifer.



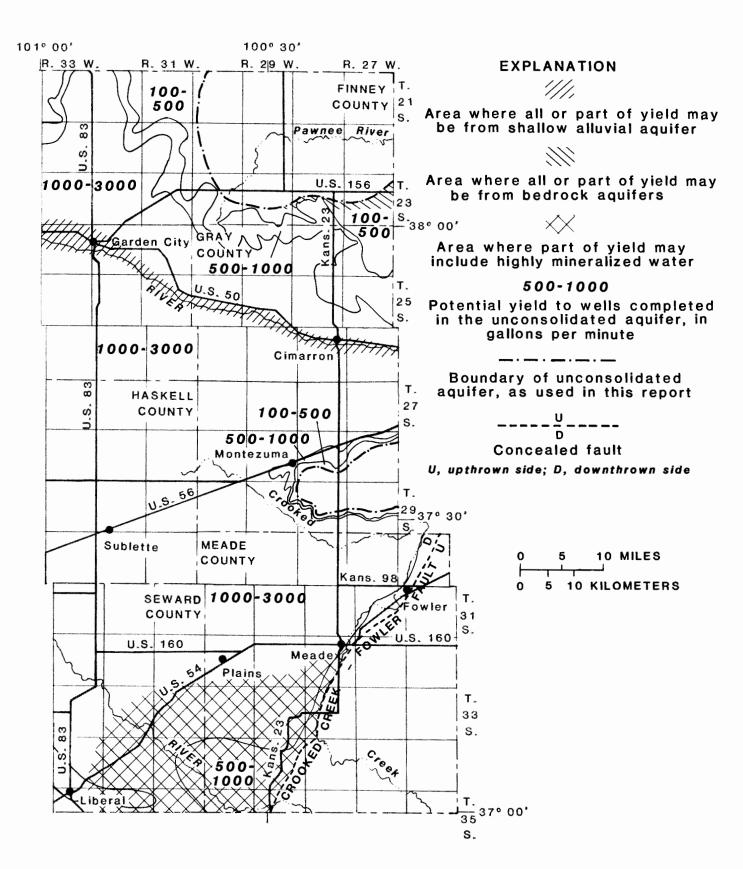


Figure 5.--Potential yield of the unconsolidated aquifer, 1975

In southwestern Meade and southeastern Seward Counties, the potential yield ranges for 500 to 3,000 gal/min. However, it may be necessary to restrict well yields from the unconsolidated aquifer because mineralized water commonly is present in the deep water-yielding layers. In these areas, extreme caution should be used in developing the potential yield of water. It is suggested that test drilling be done and electric logs be run to determine the probable water quality in the deep parts of the aquifer. At some sites, it may be desirable to install test wells and collect water samples to determine the water quality.

QUALITY OF WATER FOR IRRIGATION

The chemical quality of water in southwestern Kansas generally is the result of conditions within the hydrologic system. The quality of surface-water inflow, as shown by the analyses listed in table 2, is largely controlled by the effects of stream regulation and return flow from irrigation use occurring outside the study area. The quality of surface-water outflow, which is contributed mostly from ground-water storage, is dependent on geohydrologic conditions within the area. The quality of ground water in the various geologic formations, as shown by the analyses listed in table 3, is a result of the quantity and quality of recharge and the interaction with chemical constituents in each aquifer system.

In this report, water is classified by type according to the principal constituents and by general categories in terms of dissolved-solids concentrations in milligrams per liter (mg/L). Freshwater is defined as having less than 1,000 mg/L dissolved solids; saline water, as having 1,000 to 10,000 mg/L; brackish water, as having 10,000 to 35,000 mg/L; and saltwater or brine, as having more than 35,000 mg/L dissolved solids.

Table 2.--Chemical analyses of surface water in southwestern Kansas

[Concentrations in milligrams per liter]

Location	Site num- ber	Date of collec- tion	Dis- charge (ft ³ /s)	Tem- per- a- ture (°C)	Dis- solved silica (SiO ₂)	Dis- solved cal- cium (Ca)	Dis- solved mag- ne- sium (Mg)	Dis- solved sodium (Na)	Dis- solved po- tas- sium (K)	Car- bon- ate (CO ₃)	Bicar- bonate (HCO ₃)
				Arkar	nsas River	gaging stat	ions				
Near Coolidge At Dodge City	-	01/08/76 01/06/76	21 2.2	1.0 1.0	15 14	440 130	180 42	640 96	12 6.8	0 0	329 320
				Cima	rron River	sampling s	ites				
32 33W 21CCA 32 33W 36BDA 33 32W 20ACD 33 32W 25ACC 34 30W 31BBC 34 31W 15CBA 35 29W 08DDC 35 29W 10BCD 35 30W 09CCB 35 30W 13BBB	2 3 4 5 7 6 10 11 8 9	11/14/74 11/14/74 11/14/74 11/14/74 11/14/74 11/14/74 11/14/74 11/14/74 11/14/74	.01 .35 11.5 19.1 41.9 39.6 57.7 56.5 56.3	3.0 6.0 8.5 10.0 11.5 10.5 11.0 6.0 9.0	20 15 20 20 20 20 20 21 21	94 78 77 83 93 88 93 94 86 96	31 30 24 23 34 27 37 42 32 38	61 36 43 50 120 86 380 410 140 370	5.0 5.5 3.8 4.0 4.5 5.8 5.8 5.2	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	390 300 260 240 240 240 230 240 240 250
Location	Site num- ber	Dis- solved sul- fate (SO ₄)	Dis- solved chlo- ride (C1)	Dis- solved fluo- ride (F)	Dis- solved ni- trate (NO ₃)	Dis- solved solids (resi- due at 180°C)	Hard (Ca,Mg)	Non- car- bon- ate	So- dium ad- sorp- tion ratio	Specific conduc- tance (μπhos/cm at 25°C)	ı pH
	•			Arka	nsas River	gaging sta	tions				***************************************
Near Coolidge At Dodge City	-	2,500 370	200 43	0.6	10.2 30.5	4,510 903	1,800 500	1,600 240	6.5 1.9	5,000 1,320	8.8 7.6
				Cim	arron Rive	r sampling	sites				
32 33W 21CCA 32 33W 36BDA 33 32W 20ACD 33 32W 25ACC 34 30W 31BBC	2 3 4 5 7	140 120 140 150 150	23 19 21 40 190	.8 .8 .8	0.2 0.4 5.4 6.2 5.2	566 452 461 492 739	360 320 290 300 370	42 72 74 110 170	1.4 0.9 1.1 1.3 2.7	900 720 730 780 1,260	7.8 7.9 7.9 7.6 8.1
34 31W 15CBA 35 29W 08DDC 35 29W 10BCD 35 30W 09CCB 35 30W 13BBB	6 10 11 8 9	150 180 180 150 170	98 620 650 220 580	.8 .8 .8	4.8 4.6 4.2 4.4 4.0	608 1,460 1,520 772 1,400	330 380 410 350 400	120 190 210 150 190	2.1 8.4 8.9 3.3 8.1	1,010 2,590 2,650 1,340 2,460	7.9 7.9 7.9 7.8 8.0

Table 3.--Chemical analyses of ground water in southwestern Kansas [Concentrations in milligrams per liter]

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Po- tas- sium (K)	5.4	17 7.1 3.2 3.2	Hg.	7.8	7.7
Sodium (Na)	61 176 34 121 46		Specific conduc- tance (µmhos/cm at 25°C)	760 820 790 2,100	3,530 1,030 370 380
Dis- solved mag- ne- sium (Mg)	36 1.1 34 91 21	134 34 9.0 6.8	So- dium ad- sorp- tion ratio	1.7 14 .8 1.7 1.2	1.6 4.0 3.
Dis- solved cal- cium (Ca)	38 11 73 248 83	360 107 50 61	Hardness Non- Car- bon-	29 0 126 845 144	1,170 222 10 10
Dis- solved man- ga- nese (Mn)	0.00 .02 .00 .00	00.00.00	Hard 	243 32 322 993 294	1,450 406 162 180
Total grinn n (Fe) (0.01 .06 .01 .10		Dis- solved solids (resi- due at 180°C)	434 508 465 1,680	2,870 728 214 232
Dis- solved T silica i (SiO ₂) (31 0 6.1 24		Dis- solved ni- trate (NO ₃)	0.0 1.8 12 10 6.6	38 15 4.9 7.1
Tem- Di per- Di a- so ture si (°C) (S	18.0 14.5 14.5		Dis- solved fluo- ride (F)	3.6 2.3 1.0 .8	1.8 0.1 3.3 1.0
	12/60 . 15/70 1 19/60 . 19/69 1		Dis- solved chlo- ride (Cl)	27 77 31 117 20	168 38 7.0 11
Date of collec- tion	10/1 07/1 11/1 05/1 03/1	05/07/64 07/31/70 04/29/63 04/10/68	Dis- solved sul- fate (SO ₄)	109 106 138 912 199	1,620 308 20 16
Geologiç source ¹ 7	00,10 kD 00,10 01,10	QA QU,TO QU,TO QU,TO	Bicar- bonate (HCO ₃)	261 244 239 181 183	334 224 185 200
Well depth (ft)	203 485 261 309 280	45 300 205 200	Car- bon- ate (CO ₃)	00000	0000
Local well	21 32W 20CB 22 27W 14BD 23 32W 20DC 23 34W 26CCC 24 32W 18CC	24 33W 12CB 25 31W 02A 26 32W 26CD 26 33W 19DAC	Local well	21 32W 20CB 22 27W 14BD 23 32W 20DC 23 34W 26CCC 24 32W 18CC	24 33W 12CB 25 31W 02A 26 32W 26CD 26 33W 19DAC

GRANT COUNTY

Po- tas- sium (K)	5.5	4.4	.8.3.3 3.3.3 8.3.3	Н	7.5	7.6	
Po ta Sodium s (Na)	75 45	46 54 86	51 102 32 35 46	Specific conduc- tance (umhos/cm at 25°C)	850 670 780 1,220	790 870 760 570 600	
Dis- solved mag- ne- sium (Mg)	35 12	28 30 58	27 23 27 19 24	So- dium ad- sorp- tion ratio	1.8 1.4 1.2 1.4	1.3 3.0 1.0 1.3	
Dis- solved cal- cium (Ca)	70 55	67 67 89	75 51 74 60 54	Hardness Non- car- bon-	82 30 74 122 274	100 44 138 72 55	
Dis- solved man- ga- nese (Mn)	0.00	00.00	88888	Hardı (Ca,Mg)	318 186 282 290 460	298 222 296 228 233	
Total giron r	0.00	.00 .16	.03 .13 .01	Dis- solved solids (resi- due at 180°C)	596 327 461 514 793	491 557 438 371 408	
Dis- solved silica (SiO ₂)	23	19 22 25	23 25 22 15 17	Dis- solved ni- trate (NO ₃)	26 4.1 18 19 15	8.0 3.3 9.2 7.5	
Tem- D per- D a- s ture s (°C) (16.5		18.5	Dis- solved fluo- ride (F)	2.0 1.2 1.5 2.1	1.2	
of -5e	05/07/64 10/28/41	05/04/64 03/20/68 07/20/59	05/25/60 08/14/75 08/14/75 05/14/64 05/14/64	Dis- solved chlo- ride (Cl)	24 11 15 24 57	16 30 67 26 13	
	05/	05//002//	05/ 08/ 08/ 05/ 05/	Dis- solved sul- fate (SO ₄)	193 104 137 191 349	171 210 107 110 110	
Geologi 9	QU,TO QU,TO	01,10 01,10 01,10	01,10 10,KJ 01,10 01,10 01,10	Bicar- bonate (HCO ₃)	288 190 254 205 227	242 217 193 190 217	
Well depth (ft)	340 220	4 38 300 285	460 645 380 310 560	Car- bon- ate (CO ₃)	00000	0000	
Local well	27 37W 11AB 28 35W 15BB	28 36W 13AC 28 37W 21DAA 28 38W 04CC	29 35W 15AB 29 36W 04BAB 29 36W 04BCC 30 38W 05BB 30 38W 13CC	Local well	27 37W 11AB 28 35W 15BB 28 36W 13AC 28 37W 21DAA 28 38W 04CC	29 35W 15AB 29 36W 04BAB 29 36W 04BCC 30 38W 05BB 30 38W 13CC	1,

QA, Quaternary alluvium; QU, undifferentiated Pleistocene deposits; TO, Ogallala Formation; KN, Niobrara Chalk; KD, Dakota Formation; KJ, Upper Jurassic-Lower Cretaceous rocks; PW, Whitehorse Formation; PD, Day Creek Dolomite. Geologic source:

Table 3.--Chemical analyses of ground water in southwestern Kansas--Continued [Concentrations in milligrams per liter]

GRAY COUNTY

Po- tas- sium (K)	5.2 6.3 7.6 3.8 4.1	3.0	퓝	7.6 7.7 7.5 7.6	7.7
Sodium (Na)	22 30 45 19	16 14	Specific conduc- tance (µmhos/cm at 25°C)	550 600 1,060 430 410	172 340
Dis- solved mag- ne- sium (Mg)	25 25 40 11 9.8	11,	So- dium ad- sorp- tion ratio	6. 8. 9. 9.	က်က
Dis- solved cal- cium (Ca)	53 58 130 56 60	57 45	Hardness Non- Car- bon-	57 72 261 8 8	15 0
Dis- solved man- ga- nese (Mn)	00000	00.	Hard 	235 248 489 184 190	187 144
D S Total g iron n (Fe) (05 02 05	.04	Dis- solved solids (resi- due at 180°C)	356 396 740 270 259	256 206
Dis- solved T silica i (Si0 ₂) (36 0 445 21 16	19 18	Dis- solved ni- trate (NO ₃)	20 15 26 12 9.3	10 11
Tem- Di per- Di a- so ture si (°C) (S	16.5 3 15.0 4 14.5 2 15.5 1	16.0 1	Dis- solved fluo- ride (F)	2.7 2.7 .8 .4	မို့
			Dis- solved chlo- ride (Cl)	22 22 35 9.0 7.0	10
Date of collec- tion	06/07/67 05/07/70 07/06/70 05/12/70 07/28/64	05/08/64 05/21/70	Dis- solved sul- fate (SO ₄)	65 84 284 26 17	26 14
Geologiç source ¹⁷	00,10 00,10 0A 00,10	QU,TO QU,TO	Bicar- bonate (HCO ₃)	217 215 278 278 215 232	210 183
Well depth (ft)	200 170 80 246 100	204	Car- bon- ate (CO ₃)	00000	00
Local well number	24 29W 23BAA2 24 30W 01BCB 26 28W 06D 26 29W 08B 27 27W 10DCB	29 28W 28CDC 29 30W 36C	Local well number	24 29W 23BAA2 24 30W 01BCB 26 28W 06D 26 29W 08B 27 27W 10DCB	29 28W 28CDC 29 30W 36C

HAMILTON COUNTY

Po- tas- sium (K)	5.2 21 	7.2	Æ	8.2 7.4	:
Sodium (Na)	220 505 37 37 54	140	Specific conduc- tance (µmhos/cm at 25°C)	960 4,500 3,310 970	1,800
Dis- solved mag- ne- sium (Mg)	2.0 127 116 48 39	35	So- dium ad- sorp- tion ratio	21 5.3 4.5 .7	2.4
Dis- solved cal- cium (Ca)	4.8 472 276 167 105	200	Hardness Non- Car- bon-	0 1,460 958 354 230	470
Dis- solved man- ga- nese (Mn)	000000000000000000000000000000000000000	00.	Hard 	20 1,700 1,170 616 422	650
Total grinn (Fe) (.1 .00 .20 .7 .13	.01	Dis- solved solids (resi- due at 180°C)	598 3,660 2,510 843 678	1,250
Dis- solved T silica i (SiO ₂) (15 1 25 22 22 25	55	Dis- solved ni- trate (NO ₃)	0.4 10 16 159 14	19
Tem- Di per- Di a- so ture si (°C) (S	14.5 14.5	2	Dis- solved fluo- ride (F)	2.8 1.0 1.4 1.5	.5
	06/21/72 04/30/64 09/02/60 11/26/40	·	Dis- solved chlo- ride (Cl)	38 311 122 56 56 25	84
Date of collection	06/2 04/3 09/0 11/2 04/2	04/23/62	Dis- solved sul- fate (SO ₄)	121 2,040 1,480 215 291	620
Geologiç source ¹⁷	κD QA QU, TO QU, TO	QU,T0	Bicar- bonate (HCO ₃)	398 295 254 320 234	220
Well depth (ft)	70 70 60 60	06	Car- bon- ate (CO ₃)	00000	0
Local well	42W 03CB 42W 26DCA 43W 26BCC 43W 10DD 41W 36CCD	39W 35CBA	Local well number	42W 03CB 42W 26DCA 43W 26BCC 43W 10DD 41W 36CCD	39W 35CBA
۲	23 23 24 26	24	Lo	21 23 24 26	24

Table 3.--Chemical analyses of ground water in southwestern Kansas--Continued

[Concentrations in milligrams per liter]

HASKELL COUNTY

Po- tas- sium (K)	2.2 2.8 3.2 3.2	5.2	五	7.7	7.8
Sodium (Na)	20 16 24 19	20 41	Specific conduc- tance (µmhos/cm at 25°C)	400 360 380 420 430	390 690
Dis- solved mag- ne- sium (Mg)	7.8 5.9 11 13	11 30	So- dium ad- sorp- tion ratio	7.0 6. 6.	1.1
Dis- solved cal- cium (Ca)	53 53 43 51 48	51 62	Hardness Non- Car- bon-	0 12 0 32 3	8 106
Dis- solved man- ga- nese (Mn)	000.000.000	00.	Hard 	164 156 152 180 165	172 278
Total (Fe)	0.00 .08 .09 .12	.13	Dis- solved solids (resi- 180°C)	249 230 245 258 266	248 465
Dis- solved l silica i (SiO ₂) (18 18 18 19 16	17 25	Dis- solved ni- (NO ₃)	14 12 6.2 11 1.8	4.3 9.7
Tem-Diper-Dia-scrape siture sit(°C) (9	16.0 1 17.0 1 17.0 1	18.0 2	Dis- solved fluo- (F)	4.0 4. 8. 8.	1.1
Jate of a collect to			Dis- solved chlo- (Cl)	8.0 10 8.0 20 14	7.0
004	05/04/66 04/30/70 04/30/70 04/30/70 08/04/64	05/05/64 04/30/70	Dis- solved sul- (SO ₄)	23 26 36 31 47	.36 154
Geologjç source ¹⁷	00,10 00,10 00,10 00,10	QU,TO QU,TO	Bicar- (HCO ₃)	205 176 185 181 198	200 210
Well depth (ft)	250 620 590 408 384	270 532	Car- bon- (CO ₃)	00000	00
Local well number	27 31W 11CBB 28 33W 04A 28 33W 36D 28 34W 15DAB 29 32W 26CB2	30 31W 14DB 30 34W 28ABB	Local well number	27 31W 11CBB 28 33W 04A 28 33W 36D 28 34W 15DAB 29 32W 26CB2	30 31W 14DB 30 34W 28ABB

KEARNY COUNTY

Po- tas- sium (K)	6.8 11 17 13	5.0	풘	8.0	7.3
Sodium (Na)	42 43 95 362 164	416 401 35 41	Specific conduc- tance (µmhos/cm at 25°C)	610 1,800 3,330 2,180	3,810 3,810 590 480
Dis- solved mag- ne- sium (Mg)	27 22 49 101 100	115 94 24 26	So- dium ad- sorp- tion ratio	1.2 1.5 1.5 2.3	5.0 1.0 1.3
Dis- solved cal- cium (Ca)	51 64 251 354 210	346 367 56 29	Hardness Non- Car- bon-	46 103 664 1,090 733	1,120 1,170 32 0
Dis- solved man- ga- nese (Mn)	0.00	00:00:	Hard (Ca,Mg)	238 255 828 1,300 935	1,340 1,300 238 180
D s Total g iron n (Fe) (1.4 2.4 .01 .0 .07	.02 .01 .07	Dis- solved solids (resi- due at 180°C)	399 402 1,330 2,770 1,650	2,920 2,870 363 298
Dis- solved T silica i (SiO ₂) (8 8 3 3 9	8 0 0 8	Dis- solved ni- trate (NO ₃)	23 13 15 17 8.4	11 10 10 5.3
Tem- Di per- Di a- so ture si (°C) (S	15.0 15.0 14.5 16.0	14.5 1 14.5 1 16.5 1 18.0 1	Dis- solved fluo- ride (F)	1.4 5 5 1.1	1.4 .8 .9 2.4
)5/22/67	19/21/60 1. 19/21/60 1. 14/26/63 1.	Dis- solved chlo- ride (Cl)	28 20 110 116 92	131 139 16 15
Date of collec- tion	05/2; 11/0 05/08 05/0	09/21 09/2 04/26 04/26	Dis- solved sul- fate (SO ₄)	76 144 678 1,660	1,750 1,760 74 35
Geologiç sourcel	KN QU, TO QU, TO QA, QA	QA QU,TO QU,TO KD	Bicar- bonate (HCO ₃)	234 185 200 256 246	268 166 251 200
Well depth (ft)	163 154 320 65 280	40 150 330 300	Car- bon- ate (CO ₃)	00000	0 0 0 25
Local well number	21 35W 27CCA 22 37W 34DD 23 35W 25BB2 24 35W 22CCC 24 36W 23CBB2	25 36W 03CCD 25 36W 18ACC 26 37W 21DDD 26 38W 06BCC	Local well number	21 35W 27CCA 22 37W 34DD 23 35W 25BBB2 24 35W 22CCC 24 36W 23CBB2	25 36W 03CCD 25 36W 18ACC 26 37W 21DDD 26 38W 06BCC

Table 3.--Chemical analyses of ground water in southwestern Kansas--Continued [Concentrations in milligrams per liter]

MEADE COUNTY

Local well number	Well depth (ft)	Geologjç source ¹ /	Date of collec- tion		Tem- per- a- ture (°C)	Dis- solved silica (SiO ₂)	Total grinn rivon	Dis- solved man- ga- nese (Mn)	Dis- solved cal- cium (Ca)	Dis- solved mag- ne- sium (Mg)	Sodium (Na)	Po- tas- sium (K)
	290 583 468 120 720	0U,TO WW TO TO WW	09/10/64 12/17/74 11/22/74 07/28/64 11/21/74			19 8.3 22 21 10	0.00 .86 .00 .00	0.00	58 320 59 58 58 1,500	14 120 15 15 470 10	15 87 27 63 10,800	3.2 10 4.8 4.2 38
	504 260	το QU,ΤΟ	11/20/74 05/11/66	774	0.71	20 22	.36	00.	83 5°	21 20	48 38	4.5
1	Car- bon- ate (CO ₃)	Bicar- bonate (HCO ₃)	Dis- solved sul- fate (SO ₄)	Dis- solved chlo- ride (Cl)	Dis- solved fluo- ride (F)	Dis- d solved ni- trate (NO ₃)	Dis- solved solids (resi- due at 180°C)	Haro (Ca,Mg)	Hardness Non-car-bon-	So- dium ad- sorp- tion ratio	Specific conduc- tance (µmhos/cm at 25°C)	五
1	00000	222 66 200 220 78	30 1,400 73 52 2,800 18	9.0 16 18 79 18,200	0.8 8.8 8.0	12 1.4 3.5 3.5	271 1,960 319 405 33,800	202 1,300 210 206 5,800	20 54 48 48 26 5,600	0.5 1.1 .8 1.9 62	2,300 5,300 57,300 57,300	7.4 7.4 8.0 7.4
27BBB2 09ABC	00	190 212	200 85	21 29	1.0	6.3 5.8	494 369	290 229	140 55	1.2	750 580	7.9

Po- tas- sium (K)	3.6	0.24.2 0.22.8	품	:::::	7.4
Sodium (Na)	30 67 58 44 48	49 83 59	Specific conduc- tance (µmhos/cm at 25°C)	670 2,920 660 790	670 2,520 1,050 740
Dis- solved mag- ne- sium (Mg)	30 47 97 40 37	38 95 28	So- dium ad- sorp- tion ratio	0.8 1.5 1.2 1.2	1.4
Dis- solved cal- cium (Ca)	62 74 597 38 61	39 450 114 64	Hardness Non- car- bon-	110 182 1,750 60 116	42 1,380 279 0
Dis- solved man- ga- nese (Mn)	00.00	00000	Hard (Ca,Mg)	278 380 1,890 260 304	254 1,510 457 274
Total griron n	0.05 1.5 .03 1.8	5 .02 .17	Dis- solved solids (resi- due at 180°C)	399 613 2,670 415 498	426 2,230 738 471
Dis- solved To silica ii (SiO ₂) ((:		Dis- solved ni- trate (NO ₃)	11 6.2 8.0 9.7	11 8.0 6.6 5.8
Tem- Disper- Solution	13.0 18 15.5 19.0 25 16.5 25 14.5 25	18.0 25 25 25	Dis- solved fluo- ride (F)	1.3 1.9 2.3 3.6	2.2
		//25/63 18 //04/62 //25/63	Dis- solved chlo- ride (Cl)	44 24 10 12 24	13 11 16 14
Date of collec- tion	04/25/63 10/13/39 04/09/62 04/24/63	04/25 04/04 04/25 04/12	Dis- solved sul- fate (SO ₄)	98 270 1,780 118 183	114 1,480 367 99
Geologiç sourcel	01,10 01,00 PD 01,10	ου,το ου ου,το ου,το	Bicar- bonate (HCO ₃)	205 242 163 244 229	259 159 217 349
Well depth (ft)	157 170 600 187 422	260 75 385 270	Car- bon- ate (CO ₃)	00000	0000
Local well number	31 43W 20CBB 32 39W 18AA 32 41W 28DB 32 42W 14CCC 33 39W 16ABB	33 43W 15AAC 34 42W 05BDC 35 40W 03BBB 35 43W 24AA	Local well number	31 43W 20CBB 32 39W 18AA 32 41W 28DB 32 42W 14CCC 33 39W 16ABB	33 43W 15AAC 34 42W 05BDC 35 40W 03BBB 35 43W 24AA

Table 3.--Chemical analyses of ground water in southwestern Kansas--Continued [Concentrations in milligrams per liter]

SEWARD COUNTY

Po- tas- sium (K)	8.4 4.6 6.6 6.6	4.4 4.0 680 4.5 320	12 3.2 3.2 3.2
Sodium (Na)	33 58 52	33 36 6,100 82 5,000	670 41 24 32 27
Dis- solved mag- ne- sium (Mg)	15 25 31 18 26	26 26 1,800 25 640	50 17 17 23 24
Dis- solved cal- cium (Ca)	66 66 59 56 69	51 62 3,600 80 1,300	150 70 77 70 53
Dis- solved man- ga- nese (Mn)	00000	800000	000000
Total iron (Fe)	0.20 .00 .02 .05	.08 .03 1.8 1.5	.81 .05 .02 1.3 .03
Dis- solved silica (SiO ₂)	23 22 24 24	23 26 23 33	11 25 31 29 33
Tem- per- a- ture (°C)	:::::		16.0
Date of collec- tion	05/07/74 05/08/74 05/07/74 05/07/74 05/07/74	05/07/74 05/07/74 10/10/74 10/10/74 10/18/74	10/22/74 07/22/75 05/07/74 10/16/74 05/07/74
Geologiç source ¹ /	00,10 00,10 00,10 00,10	QU,10 QU,10 PW QU PW	το
Well depth (ft)	412 347 375 341 386	350 335 465 205 705	460 250 458 562 383
Local well number		32 34W 10DA 32 34W 17DCC 33 32W 28CDD 33 32W 28CDD2 34 31W 30BBB	34 31W 30BBB2 34 31W 30BBB3 34 34W 16DAA 34 34W 17DDD 35 33W 16BCA

,	1		
Н	7.8 7.6 7.7 7.7 7.7	7.8 7.6 7.9 8.0	8.1 7.7 7.6 8.4 7.7
Specific conduc- tance (µmhos/cm at 25°C)	570 690 740 540 730	570 630 950	4,500 700 580 660 530
So- dium ad- sorp- tion ratio	1.0 1.5 1.6	1.0 1.0 21 2.1 28	12 1.1 .6 .9
Hardness Non- car- bon-	46 92 62 44 99	52 80 6,300 120 5,700	510 70 107 120 46
Hard	230 270 270 270 210 280	230 260 16,380 300 5,800	580 244 260 270 230
Dis- solved solids (resi- due at 180°C)	363 432 488 345 48	370 411 33,800 577 19,500	2,420 403 396 423 350
Dis- solved ni- trate (NO ₃)	12 21 5.8 7.3	9.1 8.0 8.0 .2 9.3	2.9 9.6 12 15
Dis- solved fluo- ride (F)	0.9 0.1 1.1 8.	1.1 .874	1.1 4. 5.
Dis- solved chlo- ride (Cl)	23 37 19 15 20	15 23 3,300 96 1,000	1,300 55 17 15 22
Dis- solved sul- fate (SO ₄)	78 108 158 87 171	98 116 1,260 20 150 1,100 1	200 77 120 140 67
Bicar- bonate (HCO ₃)	220 220 259 210 220	220 220 156 220 140	95 212 190 190 220
Carbon- bon- ate (CO ₃)	00000	00000	00000
Local well number	31 32W 03DAD 31 33W 06CBD 31 34W 18BBB 32 31W 26CAA 32 31W 31ACC	32 34W 10DA 32 34W 17DCC 33 32W 28CDD 33 32W 28CDD2 34 31W 30BBB	34 31W 30BBB2 34 31W 30BBB3 34 34W 16DAA 34 34W 17DDD 35 33W 16BCA

Table 3.--Chemical analyses of ground water in southwestern Kansas--Continued [Concentrations in milligrams per liter]

		-So-	Hardness	Ha	Dis-						
3.1	54 29	23	55 44	00.	.00	27 16	16.5	08/26/60 04/26/64	κ <u>J</u> QU, ΤΟ	515 405	29 42W 24CC 30 39W 23BB
4.0	28	19	70	00.	.11	18		04/24/60	ņ	290	39W
3.1 3.3	30 30 30	18 13	69 54	8.8	9.0.	14 14	: :	0//08/64	υυ Το,κ <u>Ί</u>	252 400	27 42W 11DBD 27 42W 31CCC
4.2	56 26	17	69	8.5	8.5	17	:	04/22/64	00,T0	343 252	40M
6.1	51	39	98	00.0	0.00	24	i	04/22/64	KD	208	39W
(K)	(Na)	(Mg)	(Ca)	(Mn)	(Fe)	(SiO ₂)	(၁。)	tion	source ^{1/}	(ft)	number
tas- sium	Sodium	mag- ne- sium	cal-	ga- nese	Total iron	solved silica	a- ture	Date of collec-	Geologjç	Well depth	Local well
P ₀ -		Dis- solved	Dis- solved	Dis- solved man-		Dis-	Tem- per-				
					UNTY	STANTON COUNTY					
				וונבו	ושומ הווא אבו	Leonicentrations in milligrams per liters	בורנטרוסו	اردوااد ا			

7.57.7.5

870 570 550 470 590

1.2 .8 1.0 .8

165 90 92 96

375 242 246 246 188 252

표

ratio

(Ca,Mg)

Specific conductance (µmhos/cm at 25°C)

dium adsorption

> Noncarbonate

7.7

690 480

1.5

35 18

232 188

STEVENS COUNTY

	Po- tas- sium (K)	4.8 5.2 3.8	3.00 8.00	2.8	푒	7.7 7.6 7.7 7.7	7.7	7.6
	Sodium (Na)	37 40 54 42 22	28 26 28 20	26	Specific conduc- tance (µmhos/cm at 25°C)	640 570 880 620 480	550 560 400 660 550	630
	Dis- solved mag- ne- sium (Mg)	29 25 49 29 19	19 14 13 25 19	18	So- dium ad- sorp- tion ratio	1.2	8.6.6.	۲.
	Dis- solved cal- cium (Ca)	54 43 70 46 50	62 77 40 74 66	83	Hardness Non- car- bon-	74 34 200 52 52	82 92 56 130 84	135
	Dis- solved man- ga- nese (Mn)	00000	88888	00.	Hard 	250 210 380 230 200	230 250 150 288 240	280
	S s Total g iron n (Fe) (.02 .02 .02 .02 .02	.02 .02 1.8 2.2 .00	.03	Dis- solved solids (resi- due at 180°C)	401 356 600 394 307	376 360 246 437 357	431
2000	Dis- solved T silica i (SiO ₂) (23 23 28 23 34	29 30 8.7 25 32	31	Dis- solved ni- trate (NO ₃)	10 4.0 12 10 5.1	26 10 4.5 8.6	8.6
5	Tem- Di per- Di a- so ture si (°C) (S	3888		:	Dis- solved fluo- ride (F)	1.1 1.3 1.6 .9	ww.r.44	4.
		05/09/74 05/09/74 05/10/74 05/09/74 05/09/74 05/10/74	05/09/74 05/09/74 10/09/74 08/08/74 05/08/74	. 05/09/74	Dis- solved chlo- ride (Cl)	27 13 32 16 16	19 32 26 12 20	17
	Date of collec- tion	05/0 05/0 05/1 05/1 05/1	05/0 05/0 10/0 08/0 05/0	0/50	Dis- solved sul- fate (SO ₄)	107 97 242 114 46	100 79 65 170 90	155
	Geologjç source ¹ 9	00,10 00,10 00,10 00,10	01,10 01,10 10 10 01,10	QU,T0	Bicar- bonate (HCO ₃)	220 220 220 222 222 220	180 193 120 190 193	180
	Well depth (ft)	420 450 400 495 480	405 456 470 540	530	Car- bon- ate (CO ₃)	00000	00000	0
	Local well number	31 35W 26DCC 31 36W 27BCB 31 38W 17CDA 32 35W 08DDD 32 37W 10DCC	33 38W 20DDB 34 35W 07BCC 34 35W 18BCA 34 39W 14DDD 35 36W 01AAA	35 39W 10CAD	Local well number	31 35W 26DCC 31 36W 27BCB 31 38W 17CDA 32 35W 08DDD 32 37W 10DCC	33 38W 20DDB 34 35W 07BCC 34 35W 18BCA 34 39W 14DDD 35 36W 01AAA	35 39W 10CAD

Surface Water

Most of the streamflow into the area is diverted for irrigation use or percolates to the underlying aquifer. Surface-water outflow generally represents ground-water contributions to the stream from the unconsolidated aquifer.

Arkansas River

The quality of surface water entering the area during medium to low flow commonly is saline. Analyses of samples collected from the Arkansas River at Coolidge, Kans., show that the water contains dissolved solids ranging from 2,000 to 5,000 mg/L and is a mixed type containing sodium, calcium, magnesium, and sulfate. Monthly streamflow records indicate that the water in Hamilton County "...moves from the river to the alluvium during periods of high flow and moves from the alluvium to the river during periods of low flow..." (Lobmeyer and Sauer, 1974). Thus, the chemical quality of surface water and ground water in the river valley are similar in the reach where streamflow normally occurs in Hamilton and western Kearny Counties.

During years of normal to above-normal precipitation, ground water contributes flow to the Arkansas River downstream from the Finney-Gray County line. The quantity of inflow to the stream is greatest during the nongrowing season and decreases as irrigation use and evapotranspiration increase. The analysis of samples collected from the Arkansas River at Dodge City, Kans. (about 10 miles east of the Gray County line), indicates that the quality of surface water leaving the area is fresh (dissolved solids range from about 500 to 1,000 mg/L) and is a mixed type containing calcium, magnesium, sulfate, and bicarbonate.

Cimarron River

Miscellaneous discharge and chemical-quality measurements were made, during November 1974, on a reach of the Cimarron River from a site near the point where flow began (between sites 1 and 2) to about 4 miles upstream from the Oklahoma-Kansas State line (site 11). The locations of measurement sites are shown on plate 3, and the data are listed in table 4. Site 10, included in the list of measurements, is the U.S. Geological Survey gage on the Cimarron River near Forgan, Okla. (Station No. 07156900). The measurements were made after a killing frost to reduce the effects of evapotranspiration on ground-water inflow and during a period when there was no surface-water inflow to the river between sites.

The relation of stream discharge to distance in river miles is shown graphically (fig. 6A). The discharge increases progressively from site 3 (sec.36, T.32 S., R.33 W.) to site 8 (sec.9, T.35 S., R.30 W.) and becomes relatively steady from site 8 to site 11 (sec.10, T.35 S., R.29 W.). Thus, most of the ground-water inflow from the aquifer to the river occurs upstream from site 8.

A water sample was collected at each measurement site for analysis and for an indication of changes in the chemical quality of ground-water inflow to the river. The quality of water being discharged from the study area by the river is saline (about 1,400 mg/L) and is a sodium chloride type.

The concentration of chloride also is related to distance in river miles (fig. 6B). Chloride concentrations increased gradually from site 3 to site 8 and increased rapidly between sites 8 and 9. Thus, most of the ground-water inflow was contributed upstream from site 8, but the greatest increase in chlorides occurred between sites 8 and 9. Much of the chloride increase probably is attributable to a spring that yields salty water to the river in the

Table 4.--Miscellaneous discharge and chemical-quality measurements on Cimarron River, Meade and Seward Counties, Kansas

	Site number	Date (1974)	Discharge (ft ³ /s)	Time (c.s.t.)	Temperature (°C)	Specific conductance (µmhos/cm at 25°C)	Dissolved chloride (mg/L)
32 33W 18AAA	-	Nov. 14	0	0060	!!	!	ł
32 33W 21CCA	2	Nov. 14	.01	0925	3.0	006	23
32 33W 36BDA	ო	Nov. 14	.35	1025	0.9	735	19
33 32W 20ACD	4	Nov. 14	11.5	1025	8.5	730	21
33 32W 25ACC	2	Nov. 14	19.1	1145	10.0	092	40
34 31W 15CBA	9	Nov. 14	39.6	1230	10.5	1010	86
34 30W 31BBC	7	Nov. 14	41.9	1535	11.0	1200	186
35 30W 09CCB	∞	Nov. 14	56.3	1100	0.9	1340	215
35 30W 13BBB	6	Nov. 14	55.7	1330	0.6	2400	280
35 29W 08DDC	10	Nov. 14	57.7	1410	11.0	2600	620
35 29W 10BCD	11	Nov. 14	56.5	1610	10.0	2650	650

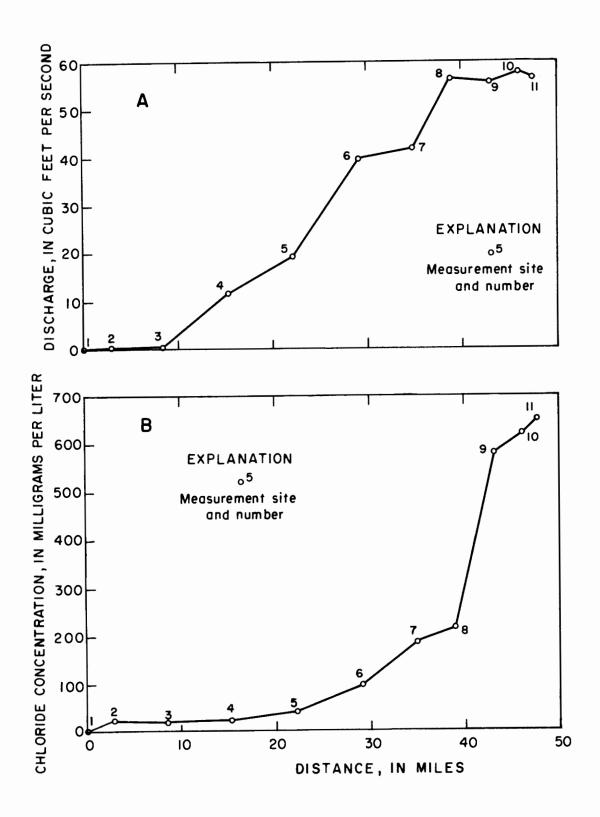


Figure 6.--Relation of distance in miles along Cimarron River to (A) discharge and (B) dissolved chloride on November 14, 1974.

NE1/4 sec.16, T.35 S., R.30 W. The chloride concentration of the spring water is not known, but water samples from nearby wells in the Whitehorse Formation show concentrations ranging from 10,000 to 20,000 mg/L.

Unconsolidated Aguifers

Water quality in the unconsolidated deposits differs chiefly as a result of the source, quantity, and quality of recharge and by association with water in other geologic formations in the subsurface. In general, the chemical quality of water in the unconsolidated aquifer, listed in table 3 and shown by plate 3, improves from west to east.

Quaternary Alluvium

The quality of water in the alluvium of the Arkansas River valley is the cumulative result of saline-water recharge and the concentration of dissolved solids by evapotranspiration. Most soils in the valley are saline because they have been affected by flooding, a shallow water table, and by surface- and ground-water irrigation. Thus, chemical constituents in water percolating to the aquifer are the result of selective precipitation of salts. The concentration of salts in the aquifer also are increased by evaporation from the shallow water table and transpiration by abundant vegetation, such as cottonwood and salt cedar.

Ground water in the alluvium from Coolidge to Garden City contains high concentrations of calcium, magnesium, sodium, and sulfate (pl. 3), and dissolved solids decrease downgradient from about 3,700 to 2,900 mg/L. In Gray County, water in the alluvium contains increased concentrations of calcium and bicarbonate and decreased concentrations of magnesium, sodium, and sulfate. According to McGovern and Long (1974), dissolved solids in the alluvial aquifer "...decrease from 1,600 mg/L at the western county line to about 500 mg/L at the eastern county line."

Ogallala Formation and Undifferentiated Pleistocene Deposits

The quality of water in the unconsolidated deposits commonly is fresh (dissolved solids range from 200 to 600 mg/L) and may be either a calcium bicarbonate type or a mixed type containing calcium, magnesium, sodium, bicarbonate, and sulfate. The chemical quality of water differs from area to area and may differ significantly with depth. These differences probably result from the source and quality of recharge, the depth, thickness, and character of sediments in the aquifer, and the association with water or soluble minerals in the bedrock formations.

In the eastern part of the unconsolidated aquifer (pl. 3), water is a calcium bicarbonate type. In the western and southern parts, magnesium, sodium, and sulfate also are principal constituents. Because precipitation is the major source of recharge within the study area, the chemical constituents in ground water probably were derived from dissolution of minerals within the aquifer and from adjacent bedrock formations. The abundance of calcium carbonate in the unconsolidated deposits provides an ample source for these constituents throughout the area. Jurassic and Cretaceous rocks that underlie the western part of the aquifer, as well as some of the unconsolidated deposits derived from these formations, provide increased percentages of sodium, magnesium, and sulfate.

In parts of northern Kearny and Finney Counties, the chemical quality of water in the aquifer has been affected by the addition of dissolved minerals derived from Upper Cretaceous rocks. The water is fresh (200 to 500 mg/L) and commonly contains sodium, magnesium, and sulfate in combination with calcium bicarbonate. Water in the aquifer north of the Arkansas River valley (pl. 3) also shows the result of extensive surface-water irrigation. Because diversions from the river have been used for many years, this source of saline water has

become a significant part of the recharge. Thus, water in the aquifer, especially at shallow depths, may contain dissolved solids as high as 1,000 to 2,000 mg/L.

In some parts of southern Meade and Seward Counties, saline water occurs near the base of the unconsolidated aquifer. Water samples from three wells, located in the same 10-acre tract of sec.30, T.34 S., R. 30 W., indicate that the chemical quality in the aquifer has been affected by highly mineralized water from the underlying Whitehorse Formation. As shown by the diagrams in figure 7, the chemical characteristics of the saline water in the lower part of the aquifer are different from those of the freshwater in the upper part but are similar to those of the brackish water in the bedrock formation.

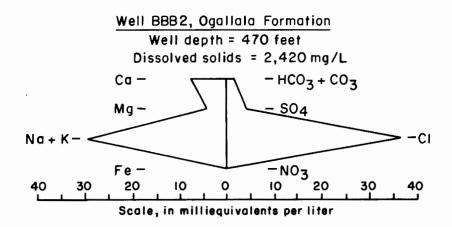
Bedrock Aquifers

Whitehorse Formation

Near the Cimarron River in southwestern Meade County and southeastern Seward County, wells in the Whitehorse Formation yield brackish water with concentrations of dissolved solids as high as 33,900 mg/L. Analyses of samples (table 3) show the water to be a mixed sodium calcium magnesium chloride in central Seward County and a sodium chloride in southwestern Meade County. Water from wells in these areas is not usable for most purposes. Electric logs indicate that the water in the Whitehorse may not be as highly mineralized in northwestern Meade County.

Day Creek Dolomite

The oldest formation in southwestern Kansas that yields usable supplies of water is the Day Creek Dolomite. Water from permeable zones in the formation



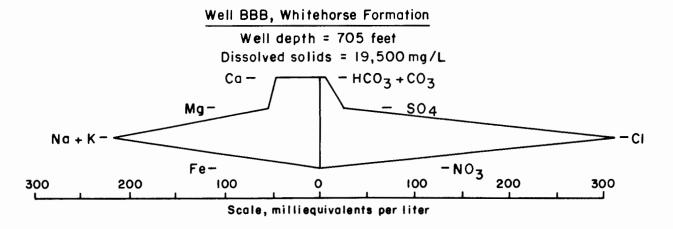


Figure 7.--Chemical characteristics in water from three wells in sec.30, T.34 S., R.30 W. in Seward County.

(gypsum aquifer) is saline, with dissolved solids of about 2,700 mg/L, and is a calcium sulfate. Water from the formation has been used for irrigation in Morton County, although continued use tends to accumulate gypsum in the soil and to rapidly corrode aluminum distribution pipe.

Undifferentiated Upper Jurassic and Lower Cretaceous Rocks

Wells in southern Hamilton County and in Stanton and Morton Counties commonly are screened in all available water-producing sandstones in the undifferentiated Upper Jurassic and Lower Cretaceous rocks and in the unconsolidated deposits. Therefore, the quality of water from those wells is similar to that from wells screened only in the unconsolidated aquifer in the same general area. Where well yields are obtained only from the sandstones, the water has a slightly higher concentration of sodium and sulfate than water from nearby wells in the unconsolidated aquifer.

In northeastern Finney County, the upper part of the sandstone aquifer (Dakota Formation) yields water that is fresh, with dissolved solids ranging from 400 to 600 mg/L, and that is a mixed sodium bicarbonate sulfate. Geophysical logs from oil tests in this area indicate that water in the lower part of the sandstone aquifer (Cheyenne Sandstone) is highly mineralized.

Niobrara Chalk

An analysis of water from the Niobrara Chalk by Latta (1944) shows that the chalk aquifer yields a mixed calcium magnesium bicarbonate water similar to that in the overlying unconsolidated aquifer. The composition of water and concentration of dissolved solids generally may be correlated with surficial conditions rather than with the mineralogical composition of the aquifer. In Finney County, Hill and others (1967) showed the constituents in water from the Fort Hays Limestone Member to be almost entirely calcium carbonate.

Suitability of Water for Irrigation

When irrigation water is applied to the land, it is necessary to consider the effects on the salinity and alkalinity of the soils. The most important chemical characteristics in evaluating the suitability of water for irrigation are the total concentration of soluble salts, expressed in terms of electrical conductivity (EC), and the relative proportion of sodium to other principal cations, expressed as the sodium-adsorption-ratio (SAR). The suitability of water from various geologic formations is shown in a diagram (fig. 8) and described according to the classification of the U.S. Salinity Laboratory Staff (1954).

Water from the Ogallala Formation and the undifferentiated Pleistocene deposits generally has a low-sodium and medium-salinity hazard. Water from undifferentiated Jurassic rocks, Lower Cretaceous rocks, and the Niobrara Chalk, which probably is derived indirectly from the unconsolidated aquifer, has similar characteristics. This type of water may be used on most soils and with crops that tolerate moderate amounts of salt.

Water from the Quaternary alluvium and from the Day Creek Dolomite have medium- and low-sodium hazards, respectively, and a very high salinity hazard. These types of water may be used on salt-tolerant crops grown in permeable, coarse-textured soils, but only by utilizing additives and special farming practices.

In the northern part of the area, water from the Dakota Formation has a high-sodium and high-salinity hazard. This water may produce harmful levels of exchangeable sodium in most soils and will require good drainage, leaching, and special additives.

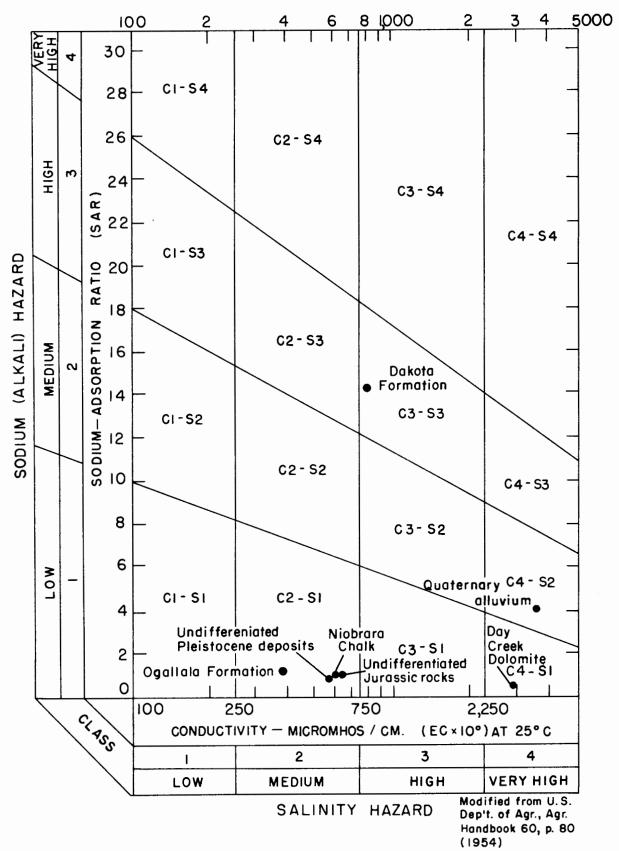


Figure 8.--Classification of irrigation water.

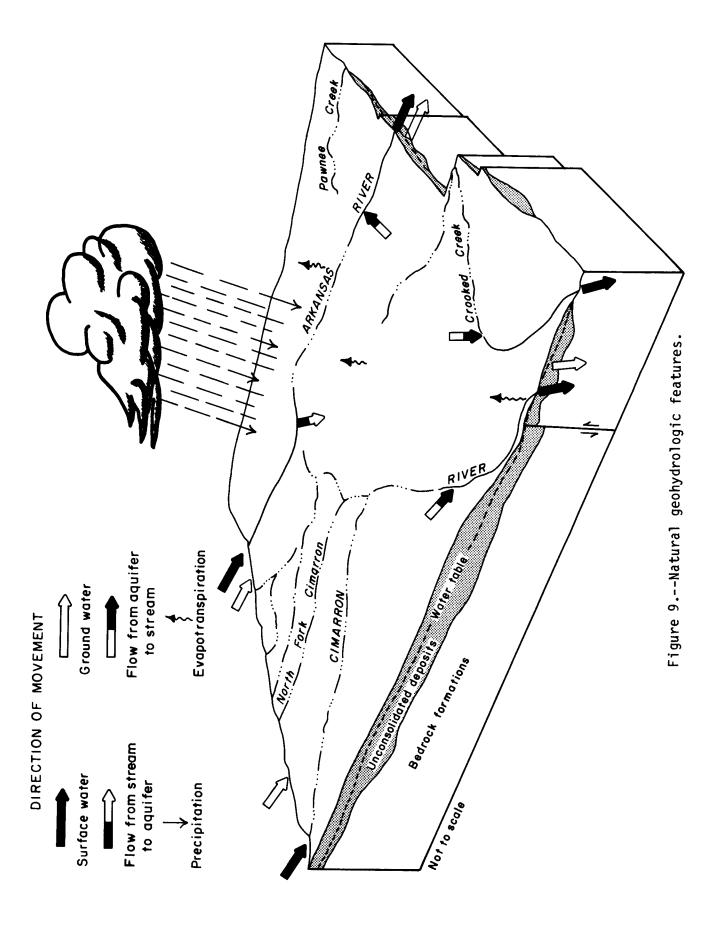
HYDROLOGIC CYCLE

The natural geohydrologic cycle in southwestern Kansas is depicted by a generalized block diagram (fig. 9). Water enters the aquifers by underflow from the west; by seepage from streams, especially in times of high flow; and by recharge of precipitation within the area. Water is discharged to the east and south by underflow, by seepage to perennial streams, and by evapotranspiration where the water table is shallow. This natural cycle has been modified by man's activities to include discharge from the aquifer by pumpage from wells and recharge to the aquifer from deep percolation of applied irrigation water.

Precipitation

The mean annual precipitation ranges from 15.82 inches at Johnson in Stanton County to 22.53 inches at Cimarron in Gray County, according to the records of the National Weather Service (U.S. Dept. of Commerce, 1975). Mean annual precipitation near the center of the area at Sublette is 19.45 inches. About three-fourths of the total annual precipitation falls during the growing season (April-October). Showers and thunderstorms in southwestern Kansas are often of high intensity and short duration and vary in areal distribution so that significant amounts fall in one area while nearby areas receive little or no rainfall.

Owing to summer heat, low humidity, and high wind movement, most precipitation returns rapidly to the atmosphere through evaporation and transpiration by plants. A total potential evaporation of 66.13 inches was measured at the Garden City Experiment Station from May through October 1974. Potential transpiration probably averages 0.70 times the total potential evaporation or about 46 inches (Crippen, 1965).



Recharge

As reported in the Finney County study (Meyer and others, 1970), recharge from precipitation on irrigated areas is significantly greater than from precipitation on nonirrigated areas. In irrigated areas, it is common practice to pump sufficient ground water to maintain soil moisture for crop use and for leaching of salts. Therefore, precipitation that is in excess of the amount needed to overcome soil-moisture deficiencies can percolate to the water table. In nonirrigated areas, vegetation generally utilizes all precipitation supplied to the soil so that excess water for percolation below the root zone is available only during periods of abnormally high rainfall. For this report, estimates of recharge from precipitation during the growing season (April-October) are assumed to be 10 percent of precipitation on irrigated land and 1 percent of the precipitation on nonirrigated land (Gutentag and Stullken, 1976).

Recharge to the aquifer is calculated for 6,600 square miles, which is the part of the area that is underlain by sufficient saturated material to support irrigation. From the following section on "Annual Withdrawals," records for 1975 show that about 1,400,000 acres were irrigated; the remaining 2,824,000 acres were not irrigated. Annual recharge to the aquifer, based on about 15 inches of precipitation during the growing season, is computed to be 210,000 acre-feet (175,000 acre-feet in the irrigated area and 35,000 acre-feet in the nonirrigated area).

Runoff of precipitation to streams also is a source of recharge to the aquifer in southwestern Kansas. The streams generally have sandy channels and are underlain by permeable deposits of sand and gravel. Water infiltrates the channel sides and bottom during periods of flow after heavy rains, and much of this water percolates to the water table. Some of the runoff that collects in shallow depressions of the land surface also percolates to the water table and

recharges the ground-water reservoir. However, the bottoms of the depressions often are filled with clayey soils that retard infiltration; consequently, most of the water evaporates. The amount of annual recharge from runoff into surface depressions and streams is assumed to be included with the total estimate of recharge from precipitation.

An additional 163,500 acre-feet per year of water enters the area as stream-flow in the Arkansas and Cimarron Rivers (U.S. Geological Survey, 1975).

Water also enters the area as subsurface inflow from the north and west. Based on the hydraulic gradient, the cross-sectional area of saturated deposits, and an average hydraulic conductivity, the inflow is calculated to be about 8,400 acre-feet per year.

Discharge

Outflow through the subsurface and seepage to streams comprise the primary modes of natural discharge of ground water from the area. Subsurface outflow, which is principally to the east, is calculated in a manner similar to that of subsurface inflow to be about 15,300 acre-feet per year.

The ground-water contribution to streamflow is considered as ground-water discharge. Parts of three streams in the area, the Arkansas River, the Cimarron River, and Crooked Creek, receive flow from ground-water seepage. As reported by Busby and Armentrout (1965), the 20-year average base flow (ground-water contribution) of the Cimarron River at Mocane, Okla. (Station No. 07157000), is $46.1~\rm ft^3/s$ or $33,400~\rm acre-feet$ per year, and the base flow of Crooked Creek near Nye, Kans. (Station No. 07157500), is $12.2~\rm ft^3/s$ or $8,800~\rm acre-feet$ per year. Figures reported in Meyer and others (1970) and in McGovern and Long (1974) indicate that about $11,300~\rm acre-feet$ per year of ground water leaves the area as base flow in the Arkansas River.

Discharge from the unconsolidated aquifer by evapotranspiration is negligible in southwestern Kansas because the water table in most of the area is too far below the land surface to be affected by evaporation and transpiration.

Annual Withdrawal

Withdrawals by wells far exceed all other discharges of ground water in southwestern Kansas. Based on records of the U.S. Department of Agriculture as discussed in the section "Ground-Water Development," it was estimated that pumpage for irrigation of 1,400,000 acres during 1975 was between 2.1 and 2.8 million acre-feet.

Some of the water withdrawn by wells and applied for irrigation is returned to the aquifer. Figures experimentally derived by Meyer and others (1970) for irrigated land in Finney County showed that about 20 percent of the water applied to irrigated land in southwestern Kansas was returned to the aquifer by percolation below the root zone. Based on the average annual withdrawal by wells for irrigation of 2.1 to 2.8 million acre-feet, calculations suggest that about 420,000 to 560,000 acre-feet per year returns to the ground-water reservoir. On the basis of 1975 data, the net withdrawal of water by wells for irrigation in southwestern Kansas is estimated to be 1.7 to 2.2 million acre-feet annually.

Measurements of natural-gas consumption by 119 wells show that an average of 7,000 cubic feet of gas is required to pump 1 acre-foot of water. Based on this figure, the volume of natural gas required to pump the estimated total withdrawal of 2.1 to 2.8 million acre-feet of water would amount to 1.5 X 10^{10} to 2.0 X 10^{10} cubic feet. Data from the Kansas Corporation Commission in 1974 showed that the 5,768 natural gas wells in southwestern Kansas produced 7.95 X 10^{11} cubic feet of natural gas or 1.38 X 10^8 cubic feet per well. Therefore,

the natural gas consumed for withdrawal of ground water in southwestern Kansas in 1974 was about 2 to 2.5 percent of the total natural gas production, or the production from 116 to 152 gas wells.

GROUND-WATER DEVELOPMENT

The number of irrigation wells in southwestern Kansas, as indicated by the records of the Division of Water Resources, Kansas State Board of Agriculture (fig. 10), increased from about 420 in January 1946 to about 7,000 in January 1975. The rate at which wells were installed increased during the mid-1950's and again during the mid-1960's, primarily in response to periods of below normal precipitation. Irrigators have continued to install wells as a means of providing an additional water supply during future dry periods, assuring a maximum crop production, and increasing production of milo and corn for use in cattle feeding.

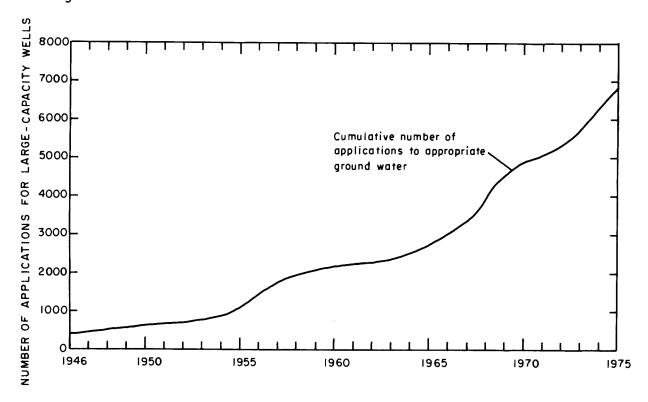


Figure 10.--Cumulative number of applications to appropriate ground water.

Records from the Agricultural Stabilization and Conservation Service and the Soil Conservation Service, U.S. Department of Agriculture, showed that about 1,400,000 acres were irrigated by ground water in 1975. If it is assumed that the application rate ranged from 1.5 to 2.0 feet per acre, as commonly reported by irrigators in the area, the total pumpage would be between 2.1 and 2.8 million acre-feet per year.

Records from the Division of Water Resources, Kansas State Board of Agriculture, also showed that about 150,000 acre-feet, or an additional 5 percent of the water withdrawn in southwestern Kansas, were pumped by municipalities, feedlots, and industries.

The locations of all large-capacity wells (yielding more than 100 gal/min) in southwestern Kansas, March 1975, are shown on plate 2.

EFFECTS OF DEVELOPMENT

Water-Level Declines

Water-level declines in the unconsolidated aquifer since 1940 (pl. 3), which have resulted principally from irrigation withdrawals, range from a few feet to about 135 feet. The greatest declines of about 130 to 135 feet have occurred in Grant County near Ulysses in T.30 S., R.37 W., and T.28 S., R. 37 W. Declines of greater than 50 feet also have occurred in Finney, Haskell, and Stanton Counties. About 10 percent of the study area has experienced 50 feet or more of water-level decline. The median water-level decline for the entire study area is 13 feet.

Water in most of the unconsolidated aquifer in southwestern Kansas is unconfined. Thus, water-level declines generally represent actual dewatering of part of the aquifer. In some of the deep zones, confined aquifer conditions were indicated by previous tests (Fader and others, 1964). However, continued

pumping from these zones has lowered the head and reduced the confining effect of the upper layers.

The amount of water removed from storage in the unconsolidated aquifer can be estimated by determining the volume of aquifer dewatered, from plate 3, and multiplying by the average specific yield of the aquifer. An average specific yield of 15 percent was assumed for the aquifer, including those areas where confinement still prevails. The volume of ground water in storage was reduced by about 14 million acre-feet during 1940-75. The net withdrawal in the 1974 irrigation season, based on 1975 data, was estimated to be 1.7 to 2.2 million acre-feet.

Hydrographs from four wells, constructed from data provided by the Division of Water Resources, Kansas State Board of Agriculture, are shown on figures 11 through 14. The hydrograph of well 27-37W-4DA (fig. 11) illustrates the long-term effects of increasingly heavy development on water levels in an unconfined aquifer. This well is screened only in the upper part of the unconsolidated aquifer. The water level during 1941-51 was stable, which is indicative of minimal early development in an area where recharge to and discharge from the aquifer were about equal. Increased development is shown by a net decline in the water level during 1951-64. The water level has continued to decline at a fairly steady rate from 1964 through 1975.

Wells 27-38W-32BCC (fig. 12) and 29-38W-35CCD (fig. 13), located in the same highly developed area as well 27-37W-4DA (fig. 11), are screened opposite all water-bearing materials in the unconsolidated aquifer, including the lower confined beds. Similar water-level declines in the three wells from 1969 to 1975 indicate that nearly equal changes have occurred over broad areas as a result of irrigation withdrawals from different parts of the aquifer.

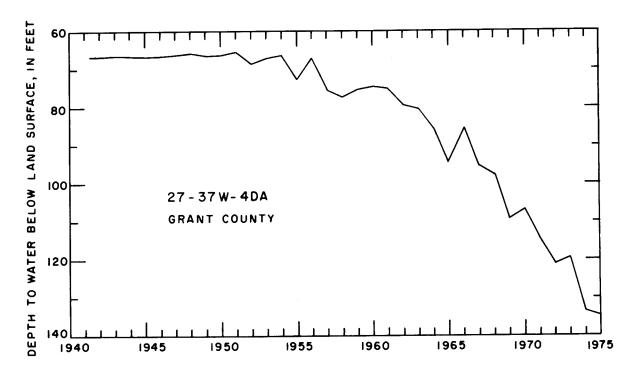


Figure 11.--Hydrograph of observation well 27-37W-4DA.

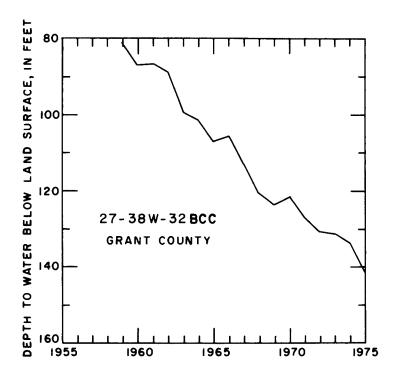


Figure 12.--Hydrograph of observation well 27-38W-32BCC.

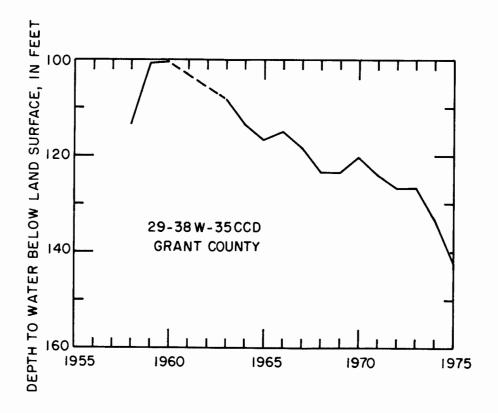


Figure 13.--Hydrograph of observation well 29-38W-35CCD.

Well 27-38W-15BBB (fig. 14), located outside the boundary of the unconsolidated aquifer, produces water only from the sandstone aquifer. However, a hydraulic connection between the two aquifers is indicated because the hydrograph of water levels in the sandstone aquifer shows the effect of pumping from the adjacent unconsolidated aquifers.

A comparison of well locations, shown on plate 2, and the water-level declines, shown on plate 3, suggests the cause and effect relationship between well density and water-level changes. The areas of greatest well density generally correspond to the areas of greatest withdrawals and water-level declines.

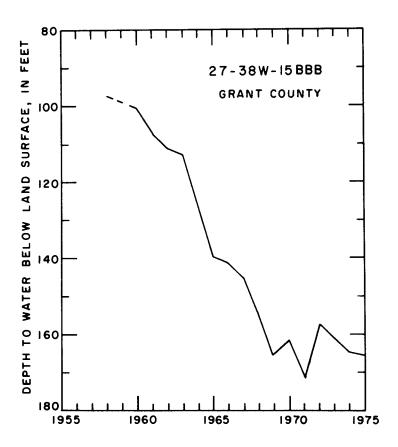


Figure 14.--Hydrograph of observation well 27-38W-15BBB.

Depletion of Ground Water in Storage

Depletion of ground water in storage or ground-water mining is indicated by water-level declines resulting from irrigation development. The relation of long-term irrigation withdrawals to changes in ground-water storage (1940-75) also may be shown (see plate 3) as a percentage decrease in saturated thickness.

The reduction in saturated thickness between 1940 and 1975 ranged from less than 10 percent to almost 60 percent, with a median of 8 percent. In about 5 percent of the area encompassed within the unconsolidated aquifer, the saturated thickness has decreased 40 percent or more since 1940.

Water levels in well 27-37W-4DA and well 27-38W-32BCC have declined about 70 feet and 90 feet, respectively, since 1940. The decrease in saturated thickness of the aquifer from 1940 to 1975 at both locations (pl. 3) is about 30 percent. During the same period, the water level in well 29-38W-35CCD declined about 80 feet, and the saturated thickness decreased about 20 percent. Although areas of greatest declines generally coincide with areas of greatest pumping, these examples indicate that similar amounts of water-level decline in different areas may not represent similar percentages of ground-water depletion. The most significant changes since 1940 are in northern Finney and northern Morton Counties where water-level declines of less than 50 feet have reduced saturated thickness by as much as 50 percent.

Further increases in the rate of withdrawals may shorten significantly the economic life of the aquifer. Those areas that have declines of 40 percent or more have already experienced a large reduction in well yields and a large increase in the cost of pumping.

FUTURE OUTLOOK FOR IRRIGATION

Economic Factors

Irrigation is a principal factor in the economy of southwestern Kansas. Some of the major problems that have greatest economic significance to the irrigator are crop prices, fuel and power costs, dependability of fuel supplies, and the efficient use of available water and power. As government control and farm programs tend to regulate prices and fuel supplies, the individual irrigator probably can gain the most benefit by increasing the efficiency of water and power use.

Additional water may be made available by utilizing potholes and tailwater pits to collect excess runoff from precipitation or waste water from irrigation. Portable pumps and lines could be used to convey the additional water to the crops as needed.

Declining water levels may result in lower well yields, which could necessitate changes in the engineering of the pumping plants. It might be beneficial to lower some pump bowls in order to achieve the maximum yield of the well even if the additional lift required a larger power unit. The condition of the well casing, pumping unit, and distribution system need to be analyzed for the conservation of water and energy.

FUTURE STUDIES

The present study has defined a number of areas that need additional study. Measurements are needed to monitor the rate and areal increase of the water-level declines. Continued analysis is necessary to determine the effects of new well development and to observe possible changes in well yields. Changes in chemical quality of water, which may become evident with declines in water level, need to be continually monitored and evaluated.

Predictive models of ground-water and surface-water relationships with the aquifer system may be used to aid in management planning. Management policies probably will depend on some way of controlling withdrawal from the ground-water reservoir by limiting (1) the amount that can be pumped per well, (2) the number of wells, or (3) the irrigated acreage.

A number of problems of limited areal extent may need further study. The sandstone aquifer needs study in order to evaluate its potential use to supplement declining yields of the unconsolidated aquifer. The relationship of the chalk aquifer to the unconsolidated aquifer needs to be studied. The

relative merits of various allocation techniques need to be tested in areas critically affected by excessive drawdowns. Studies are needed to determine the source and extent of saline water in southwestern Meade and southeastern Seward Counties. Point sources of pollution, such as urban areas, water-disposal areas, and cattle-feeding operations, need monitoring so that remedial action may be adopted.

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GLOSSARY OF GEOHYDROLOGIC TERMS

Most of the definitions of geohydrologic terms given below are taken from Lohman and others (1972).

- Acre-foot The amount of water needed to cover 1 acre to a depth of 1 foot; equals 325,851 gallons.
- Aquifer Formation, group of formations, or part of a formation that contains sufficient saturated permeable material to yield significant quantities of water to wells and springs.
- <u>Caliche</u> A deposit of clay, silt, sand, or gravel cemented by porous calcium carbonate to form a concrete-like deposit (mortar beds).
- Confined ground water Ground water that is under pressure significantly greater than atmospheric and that has as its upper limit the bottom of a bed of distinctly lower hydraulic conductivity than that of the material in which the confined water occurs.
- <u>Confining bed</u> A body of impermeable or distinctly less permeable material stratigraphically adjacent to one or more aquifers.
- Head When used alone, head is understood to mean static head, which is the height above a standard datum of the surface of a column of water that can be supported by the static pressure at a given point (see potentiometric surface).
- Hydraulic conductivity The volume of water at the existing kinematic viscosity that will move through an isotropic porous medium in unit time under a unit hydraulic gradient through a unit area measured at right angles to the direction of flow.

- <u>Hydraulic gradient</u> The change in static head per unit of distance in a given direction.
- Lenticular Describes deposits shaped like lenses when viewed in cross section.
- <u>Percolation</u> Laminar flow of water, moving by the force of gravity or hydrostatic pressure, through a porous material.
- Potentiometric surface A surface that represents the hydrostatic head. In a confined (artesian) aquifer, the water is under a pressure significantly greater than atmospheric, and the surface is defined by the levels to which water stands in wells above the water body tapped. In an unconfined aquifer, the surface coincides with the water table.
- Reentrant A transverse valley extending into an escarpment.
- <u>Saturated thickness</u> The amount (thickness) of aquifer material that is saturated.
- Specific capacity The rate of discharge of water from the well divided by the drawdown of water level within the well.
- <u>Specific conductance</u> A measure of the ability of water to conduct an electrical current and related to the concentration of specific chemical ions in solution.
- Specific yield The ratio of (1) the volume of water that the rock or soil, after being saturated, will yield by gravity to (2) the volume of the rock or soil. The definition implies that gravity drainage is complete.
- Storage coefficient The volume of water an aquifer releases from or takes into storage per unit surface area of the aquifer per unit change in head. In an unconfined water body, the storage coefficient is virtually equal to the specific yield.

<u>Transmissivity</u> - The rate at which water of the prevailing kinematic viscosity is transmitted through a unit width of the aquifer under a unit hydraulic gradient.

<u>Water table</u> - That surface in an unconfined ground-water body at which the water pressure is atmospheric. It is defined by the levels at which water stands in wells that penetrate the water body enough to hold standing water. The water table is a particular potentiometric surface.