

DANIEL F. MERRIAM, Editor

**FORTAN IV CDC 6400  
COMPUTER PROGRAM  
FOR CONSTRUCTING  
ISOMETRIC DIAGRAMS**

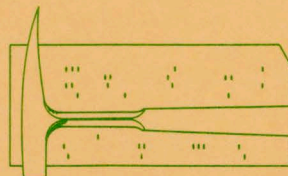
By

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in cooperation with the  
American Association of Petroleum Geologists  
Tulsa, Oklahoma



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## Editor's Remarks

The "FORTRAN IV CDC 6400 computer program for constructing isometric diagrams", by W.B. Wray, Jr., will find many uses by earth scientists. Long oriented to use of graphics such as maps, cross sections, and 3-D diagrams, geologists will welcome this contribution. Other COMPUTER CONTRIBUTIONS specifically concerned with graphic output are CC's 15, 23, 36, and 37. Most other programs also have output in graphic form.

For a limited time the Geological Survey will make available this program on magnetic tape for \$20.00 (US). An extra charge of \$10.00 is made if punched cards are required. When ordering a particular program please specify the language and computer facility needed because several versions of many programs are available.

A complete and up-to-date list of available COMPUTER CONTRIBUTIONS can be obtained by writing the Editor, COMPUTER CONTRIBUTIONS, Kansas Geological Survey, The University of Kansas, Lawrence, Kansas 66044.

## Computer Contribution

- |   |                |
|---|----------------|
| 1. Mathematical simulation of marine sedimentation with IBM 7090/7094 computers, by J.W. Harbaugh, 1966 . . . . .   | (out of print) |
| 2. A generalized two-dimensional regression procedure, by J.R. Dempsey, 1966 . . . . .  | \$0.50         |
| 3. FORTRAN IV and MAP program for computation and plotting of trend surfaces for degrees 1 through 6, by Mont O'Leary, R.H. Lippert, and O.T. Spitz, 1966 . . . . . | \$0.75         |
| 4. FORTRAN II program for multivariate discriminant analysis using an IBM 1620 computer, by J.C. Davis and R.J. Sampson, 1966 . . . . .                             | \$0.50         |
| 5. FORTRAN IV program using double Fourier series for surface fitting of irregularly spaced data, by W.R. James, 1966 . . . . .                                     | \$0.75         |
| 6. FORTRAN IV program for estimation of cladistic relationships using the IBM 7040, by R.L. Bartcher, 1966 . . . . .  | \$1.00         |
| 7. Computer applications in the earth sciences: Colloquium on classification procedures, edited by D.F. Merriam, 1966 . . . . .                                     | \$1.00         |
| 8. Prediction of the performance of a solution gas drive reservoir by Muskat's equation, by Apolonio Baca, 1967 . . . . .   | \$1.00         |
| 9. FORTRAN IV program for mathematical simulation of marine sedimentation with IBM 7040 or 7094 computers, by J.W. Harbaugh and W.J. Wahlstedt, 1967 . . . . .      | \$1.00         |
| 10. Three-dimensional response surface program in FORTRAN II for the IBM 1620 computer, by R.J. Sampson and J.C. Davis, 1967 . . . . .                              | \$0.75         |
| 11. FORTRAN IV program for vector trend analyses of directional data, by W.T. Fox, 1967 . . . . .   | \$1.00         |

(continued on inside back cover)

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# FORTRAN IV CDC 6400 COMPUTER PROGRAM FOR CONSTRUCTING ISOMETRIC DIAGRAMS

by

William B. Wray, Jr.

## INTRODUCTION

Isometric pictorial representation has long been favored by geologists as a means of displaying three-dimensional surfaces and bodies. A principal advantage over perspective representation is that plotting and measurement can be made readily anywhere on the diagram. Lobeck (1924, p. 120-121) lists the following properties of isometric diagrams.

- (1) "Measurements may be made to scale anywhere upon the upper surface of the block in the direction of either of the two coordinates, which in the object itself are at right angles to each other.
- (2) Distances in other directions are not commensurate with each other unless measured along lines parallel to each other, and they are not commensurate with distances measured on the sides of the block.
- (3) All the lines parallel in the object itself are parallel in the isometric drawing.
- (4) All lines vertical in the object are vertical in the drawing.
- (5) If the vertical scale of the drawing is the same as its horizontal scale, then the measurements made in the direction of any of the three coordinates are commensurate.
- (6) All angles in an isometric drawing are distorted, and even two angles lying in the same plane cannot be compared with each other unless they lie in exactly similar positions."

The 13D subroutines included with this contribution provide an efficient and fast method of displaying a surface - a single valued function of two variables - in isometric or similar pictorial representation. Numerous options are available through the ISPECS and RSPECS parameter arrays. Among the most important options

- (i) The diagrams can be seen from all theoretically possible viewpoints.
- (ii) The data can be viewed in an unlimited number of rectangular subblocks, all automatically spaced to avoid point overlap (x and y direction spacings are variable). Any rectangular subarea within the data array area may be considered for plotting and any number and configuration of rec-

tangular subblocks within this subarea may be skipped if desired.

- (iii) Scale, line and point spacing, and density of lines and points to be plotted are variable.
- (iv) The vertical (z) scale may be expanded or contracted relative to the horizontal (x, y) scale without restriction. Distances in x and/or y directions can be stretched or foreshortened independently, with scale remaining constant.
- (v) Surfaces may be plotted with or without the traditional block diagram frame, and major and minor scale ticks are available. A standard labelling routine can be used.
- (vi) Data input is flexible. Points can be arranged in north-south (y direction) or east-west (x direction) grid lines.

Possible applications of isometric pictorial representation can be considered within the framework of four general types of surfaces.

- (1) North-south, east-west, elevation surfaces, such as topographic surfaces, tops and bottoms of beds, buried bedrock surfaces, etc.
- (2) North-south, east-west, z surfaces, where z is any measurable quantity, such as, for example, thickness or percent of sand in a sedimentary bed, or Bouguer anomalies.
- (3) X-y-z surfaces, for example equilibrium surfaces in chemical stability diagrams.
- (4) X-y-f(x, y) surfaces, mathematical functions of two variables, including functions of many terms where the values at different points cannot be readily visualized. Many preceding papers in the Computer Contributions series deal with functions of this type. Examples are the double (two-dimensional) polynomial and Fourier series currently important in trend-surface and harmonic and spectral analysis.

Because of wide interest in computer graphics, a number of algorithms have been written which have the capability of generating three-dimensional diagrams (e.g. Rohlf, 1969). Almost all of the algorithms produce perspective rather than isometric diagrams and most have more or less serious bugs and severe limitations in point-array size due to rapid increase of execution time with increase in number of points (A.R. Paradis, personal communication).

Algorithms to construct isometric diagrams seemingly are less common, as I do not know of any, other than I3D.

The I3D subroutines have been subjected to thorough testing, and numerous isometric drawings have been obtained, but it is entirely possible that algorithm defects are present due to the complexity of the subroutines.

Acknowledgments. - Mr. Arthur R. Paradis, in charge of computer graphics at the University of California, Berkeley, Computer Center, gave encouragement and arranged use of computer facilities during the program development. His methodology is evident in both the organization of the latter half of this paper and in the subroutine structuring. The Anaconda Company provided some development computer time and permitted use of the view of the Berkeley open-pit mine in Example 2. Prof. Charles Meyer, Prof. Garniss Curtis, and Mr. Paradis kindly reviewed the manuscript.

### PROGRAM ALGORITHM

I3D1GL, the subroutine which constructs the isometric projection, processes parallel rows of points on the surface to be represented. A visibility or horizon line is constructed and is carried from the front to the rear of the surface. Each point on the surface need be tested only once to define visibility. As a consequence, calculation time increases as the first power of the number of points defining the surface, rather than the square of the number of points. This is of great practical importance in large and detailed projections (see Example 2).

An obvious next step is the development of routines to process multiple-valued functions of two variables. Both upper and lower visibility lines would be carried for each surface, so that the undersides of surfaces could be seen. In this manner, cut-away block diagrams, similar to those used to portray geology of underground mines, could be constructed.

Another useful feature to incorporate is wide-spaced surface gridding as an aid to rapid location of  $(x, y)$  positions. I have written a subroutine, I3D2GL, which permits this option, but it is not in a general form so has not been included in this paper. The subroutine takes longer to execute and requires significantly more core space, and at the present time conversion has not been justified.

I3D1GL and supporting subroutines were written to create projections at least possible cost so that, if desired, the program could be used on a routine basis. All I3D subroutines make use of a common work array BUFI and complete variable dimensioning to reduce central memory core storage requirements to a minimum. I3D1GL requires 3313g storage locations and the remaining subroutines total 3574g, independent of work array requirements. To hold exe-

cution time for all subroutines to a minimum, some care was taken to make the FORTRAN coding of high efficiency. To reduce plotting cost, I3D1GL generates plotter construction codes in such a manner as to reduce as much as possible off-paper pen travel.

Execution data specifications are entered into the various subroutines from a main program via two common parameter arrays, rather than via data cards. This considerably simplifies data input, because the need for variable card formats (for the completely general situation) is eliminated. Also, particular specifications are carried automatically between subroutines unless changed.

### RELATION OF VIEWPOINT TO BLOCK ORIENTATION

It is possible to characterize the orientation of a block in isometric projection by means of an azimuth, or line-of-sight, value and an apparent angle of inclination (looking down from above). The relation can be derived as follows.

Consider a rectilinear isometric block, Figures 1 and 2, with the properties given by Lobeck and with the edges trending north-south and east-west. To permit construction of the projection, it is necessary to solve for angles  $\alpha_1$  and  $\alpha_2$  in terms of  $\psi$  and  $\gamma$ .

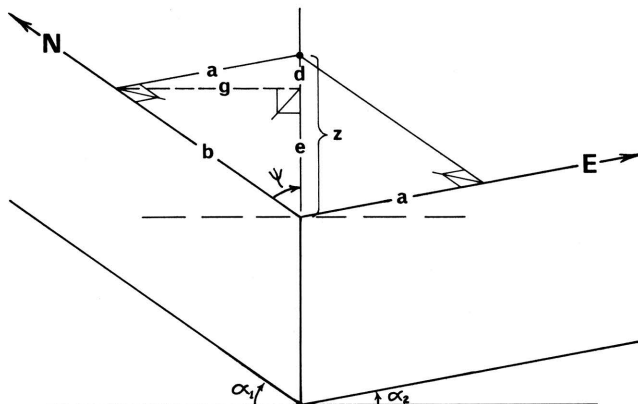


Figure 1.- Normal view of isometric diagram, with elements used to derive equations (12) and (13).

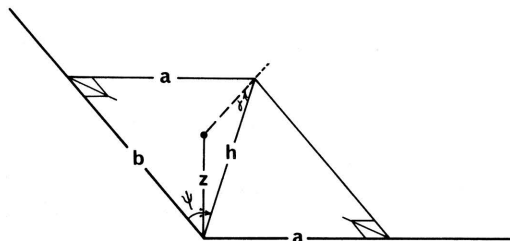


Figure 2.- View of same diagram as in Figure 1, slightly rotated out of plane of paper to show hidden elements.

$$\psi = \arctan (a/b)$$

$$\gamma = \arctan (z/h)$$

$\alpha_1$  is defined as the angle to the N-S line from a horizontal line.  $\alpha_1$  is positive if clockwise (as shown), and negative otherwise.

$\alpha_2$  is defined as the angle to the E-W line from a horizontal line.  $\alpha_2$  is positive if counterclockwise (as shown), and negative otherwise.

From Figure 2,

$$\tan \gamma = z/h = \frac{z \cos \psi}{b}, \quad (1)$$

and from Figure 1,

$$z = e + d,$$

so

$$z/b = e/b + d/b; \quad (2)$$

also

$$e/b = \sin \alpha_1, \quad (3)$$

$$d/g = \tan \alpha_2, \text{ and}$$

$$g/b = \cos \alpha_1.$$

So by multiplying the last two together,

$$d/b = \tan \alpha_2 \cos \alpha_1. \quad (4)$$

Substituting (3) and (4) into (2) yields

$$z/b = \sin \alpha_1 + \tan \alpha_2 \cos \alpha_1. \quad (5)$$

Substituting (5) into (1) results in

$$\tan \gamma / \cos \psi = \sin \alpha_1 + \tan \alpha_2 \cos \alpha_1, \quad (6)$$

which can be rewritten as

$$\tan \gamma / \cos \psi = \sin \alpha_1 + \frac{\cos \alpha_1}{\cos \alpha_2} \sin \alpha_2. \quad * (7)$$

Now

$$\cos \alpha_1 = g/b \quad (8)$$

and

$$\cos \alpha_2 = g/a, \quad (9)$$

thus (8) and (9) combine to yield, after cancelling g,

$$a/b = \cos \alpha_1 / \cos \alpha_2.$$

Because  $\psi = \arctan (a/b)$ ,

$$\psi = \arctan (\cos \alpha_1 / \cos \alpha_2). \quad * (10)$$

Equations (7) and (10) now can be combined, and successively  $\alpha_1$  and  $\alpha_2$  isolated.

$$\frac{\tan \gamma}{\cos \psi} = \sin \alpha_1 + \tan \psi \sin \alpha_2,$$

where  $\tan \psi$ ,  $(\frac{\tan \gamma}{\cos \psi})$  are numbers, call them A

and B respectively. So on substitution and reordering,

$$\sin \alpha_1 = B - A \sin \alpha_2. \quad (11)$$

From (10),

$$\cos \alpha_1 = A \cos \alpha_2, \text{ and}$$

squaring both equations gives

$$\sin^2 \alpha_1 = B^2 - 2AB \sin \alpha_2 + A^2 \sin^2 \alpha_2$$

$$\cos^2 \alpha_1 = A^2 \cos^2 \alpha_2.$$

Adding them together gives

$$\sin^2 \alpha_1 + \cos^2 \alpha_1 = A^2 (\sin^2 \alpha_2 + \cos^2 \alpha_2) + B^2 - 2AB \sin \alpha_2.$$

Because  $\sin^2 + \cos^2 = 1$ ,

$$1 = A^2 + B^2 - 2AB \sin \alpha_2, \text{ and}$$

solving for  $\alpha_2$  yields

$$\alpha_2 = \arcsin \left( \frac{A^2 + B^2 - 1}{2AB} \right).$$

Resubstituting for A and B results in

$$\alpha_2 = \arcsin \left( \frac{\tan^2 \psi + \frac{\tan^2 \gamma}{\cos^2 \psi} - 1}{\frac{2 \tan \psi \tan \gamma}{\cos \psi}} \right).$$

After shuffling and clearing of internal fractions,

$$\alpha_2 = \arcsin \left( \frac{\sin^2 \psi + \tan^2 \gamma - \cos^2 \psi}{2 \sin \psi \tan \gamma} \right). \quad ** (12)$$

Angle  $\alpha_1$  can now be obtained by substituting (12) into (11).

$$\alpha_1 = \arcsin \left( \frac{\tan \gamma}{\cos \psi} - \tan \psi \sin \alpha_2 \right)$$

which, on rewriting, becomes

$$\alpha_1 = \arcsin \left( \frac{\tan \gamma - \sin \psi \sin \alpha_2}{\cos \psi} \right). \quad ** (13)$$

Because of the particular nonEuclidian properties of isometric projection, it turns out that not all combinations of  $\psi$ ,  $\gamma$  will yield real (i.e. not imaginary) diagrams. Table 1 relates  $\alpha_1$  and  $\alpha_2$  to  $\psi$  and  $\gamma$ . Table 1 gives values for one quadrant in  $5^\circ$  intervals of  $\psi$  and  $\gamma$ , and values in  $1^\circ$  intervals are given in the Appendix. Note that a surface can be portrayed in unorthodox orientations. For instance, either  $\alpha_1$  or  $\alpha_2$  can be negative, resulting in a skewed diagram. The other three quadrants are mirror images of the first, as shown in Figure 3.

If  $\psi = \frac{\pi i}{4}$ ,  $i = 1, 3, 5, 7$ , then  $\alpha_1 = \alpha_2$  and equations (12) and (13) reduce to

$$\alpha = \arcsin \left( \frac{1}{\sqrt{2}} \tan \gamma \right). \quad (14)$$

For the standard isometric projection which has  $\alpha = 30^\circ$ ,  $\gamma = 35.2644^\circ$ .

Table 1.- Listing of  $\alpha_1$  and  $\alpha_2$  as a function of  $\psi$  and  $\gamma$ , in five degree intervals for one quadrant.

FIRST LINE, ALPHA1, ANGLE TO N-S LINE FROM HORIZONTAL		SECOND LINE, ALPHA2, ANGLE TO E-W LINE FROM HORIZONTAL	
55			
50		83.2 77.5 72.8 68.5 64.5 60.8 57.4 54.5 52.1 50.6 50.5 53.4 64.0	
		64.0 53.4 50.5 50.6 52.1 54.5 57.4 60.8 64.5 68.5 72.8 77.5 83.2	
45	90.0 85.0 80.0 75.0 70.0 65.0 60.0 55.0 50.0 45.0 40.0 35.0 30.0 25.0 20.0 15.0 10.0 5.0 -0.1		
	-0.0 5.0 10.0 15.0 20.0 25.0 30.0 35.0 40.0 45.0 50.0 55.0 60.0 65.0 70.0 75.0 80.0 85.0 90.0		
40		84.0 75.6 68.8 62.3 55.5 49.5 43.1 36.4 29.5 22.1 14.1 5.0 -6.2 -21.9 -53.9	
		-53.9 -21.9 -6.2 5.0 14.1 22.1 29.5 36.4 43.1 49.5 55.9 62.3 68.8 75.6 84.0	
35		72.7 63.2 54.7 46.5 38.2 29.7 20.6 10.6 -0.8 -14.9 -35.2	
		-35.2 -14.9 -0.8 10.6 20.6 29.7 38.2 46.5 54.7 63.2 72.7	
30		68.9 56.4 45.6 35.0 24.1 12.4 -0.8 -16.8 -39.4	
		-39.4 -16.8 -0.8 12.4 24.1 35.0 45.6 56.4 68.9	
GAMMA			
25		62.7 47.1 33.2 19.3 4.2 -13.5 -37.3	
		-37.3 -13.5 4.2 19.3 33.2 47.1 62.7	
20		52.7 33.3 14.9 -5.0 -30.1	
		-30.1 -5.0 14.9 33.3 52.7	
15		70.5 36.7 10.9 -17.2 -61.5	
		-61.5 -17.2 10.9 36.7 70.5	
10		49.3 7.2 -39.0	
		-39.0 7.2 49.3	
5		3.5	
		3.5	
0		0.0	
		-0.0	
	0 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75 80 85 90		
		PSI	

### I3D SUBROUTINES - INTRODUCTION

#### General Attributes

The remainder of this paper can be considered a manual on how to use the I3D subroutines, with examples. Each subroutine is treated in detail so as to make all execution alternatives as clear as possible, and each section can be read independently of the others.

I3D subroutines deal with points arranged in parallel equally spaced rows called grid lines. For input into I3D1GL, the points must be evenly spaced along each line. I3DPTS may be used to calculate additional lines. I3DPTA can calculate evenly spaced points from grid lines of irregularly spaced points. I3DCVT converts Hollerith card data to binary data suitable for input into I3DPTS, I3DPTA, or

I3D1GL. Because Hollerith data must be arranged in a specific manner (see the section on Point Coordinate Data Structure), I3DCHK is available to catch gross keypunching errors and misplaced data cards.

Execution times (CP) are printed for each subroutine called. Some typical timings are

- I3DCHK: 800-1400 points per second.
- I3DCVT: 1000-1600 points per second.
- I3DPTS: 800-1400 input points per second, less if many intermediate points are calculated.
- I3DPTA: 9000-10000 final points per second.
- I3D1GL: 1500-2600 points per second.

For I3D1GL, a subequal amount of plotter post-

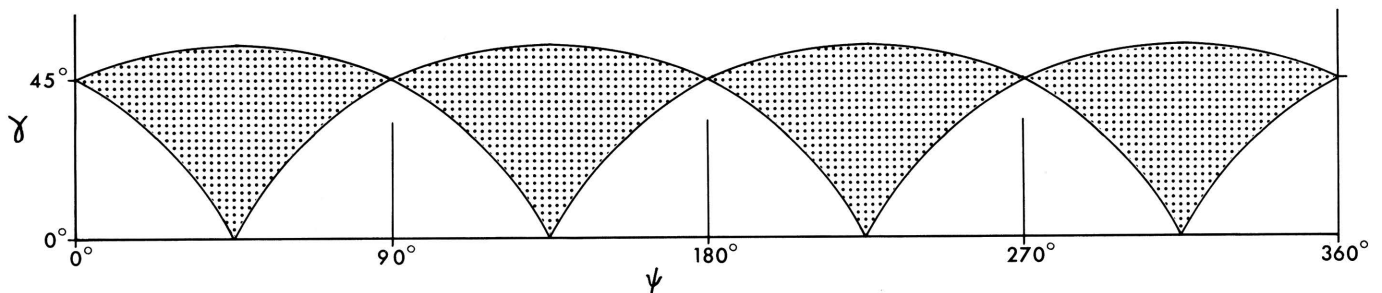


Figure 3.-Plot of  $\gamma$  versus  $\psi$  showing area within which isometric diagrams can be drawn.

processor time is needed in addition.

I3D1GL and the other subroutines can, in principle, process an unlimited number of (x, y, z) points, although the practical limit at Berkeley (due to limitations of one-job disk storage capacity) is about 1,800,000 points.

Selection of the value for final point spacing (FPS) along the grid lines is of importance because the positioning of the end point of a visible line as it passes into a hidden line can be in error by an average of one-half the FPS. Spacing depends upon values of RSPECS(7), RSPECS(10), ISPECS(10). Sixty to 80 points per inch give pleasing results; a general purpose range might be 10 to 100 points per inch. Also, for best results the FPS should be less than the final row spacing (FRS), which depends on RSPECS(1), RSPECS(10), ISPECS(9). Common usage has  $FRS = (3 \text{ to } 4) * FPS$ , or approximately 20 lines per inch.

### Terminology

Some special terminology as used in this paper:  
 (A) grid lines and points (Fig. 4 illustrates terminology);  
 (B) viewing the surface.

The attitude of the plotted surface is determined by the direction of sight (RSPECS(14),  $\psi$ ) and the apparent angle of inclination (RSPECS(13),  $\gamma$ ). Psi can range from  $0^\circ$  (looking due north, or in the +y direction) through  $90^\circ$  (looking due east, or in the +x direction) around to  $359.9^\circ$ . Note particularly the requirement that the positive y direction be due north. Gamma can range from  $0^\circ$  (horizontal) to approximately  $54.7^\circ$ . See Table 1 and Figure 3 for relation of  $\alpha_1$  and  $\alpha_2$  to  $\psi$  and  $\gamma$ .

### Program Specifications

I3D subroutines require a work array BUFI, dimensioned in the calling program, and two parameter arrays placed in labelled common as follows:

COMMON /WSPECS/RSPECS(30),ISPECS(10)

RSPECS and ISPECS are described below. Distances given in inches refer to the actual distances as they appear when drawn on paper. Distances not so specified are data distances.

List and Description of the RSPECS Array (real (FP) numbers)

Parameter	Mnemonic	Suggested Subroutines	Description
RSPECS(1)	SPACEL	PTS IGL	Space between adjacent grid lines (final, after calculation of intermediate lines, if any). Value remains the same regardless of value of ISPECS(9).
RSPECS(2)	TSTART	IGL	Transverse axis coordinate of first (westernmost if N-S, or northernmost if E-W) final grid line input.

RSPECS(3)	PSTART	CHK IGL	Parallel axis coordinate of first point (southernmost if N-S grid line or westernmost if E-W grid line) of any grid line.
RSPECS(4)	ZBOTM	IGL	Reference elevation or z-coordinate, generally $\leq$ smallest $z_{ij}$ . ZBOTM is used to position blocks on paper, or if frames are to be drawn, ZBOTM will be the z-coordinate of the bottom of the frames. ZBOTM ties data z-coordinates to RSPECS(12), the paper position of the near corner of block 1.
RSPECS(5)	ZTOP	IGL	Reference elevation or z-coordinate, generally $\geq$ largest $z_{ij}$ . ZTOP helps control block spacing: if $ZTOP = \text{largest } z_{ij}$ , then spacing is entirely a function of RSPECS(28) and RSPECS(29). If $ZTOP > \text{largest } z_{ij}$ , then spacing increases by that difference.
RSPECS(6)	DELFACT	PTS	DELFACT is used in the subroutine equation $DELTA D = DELFACT * \text{width}$ between basic grid lines, to define the point influence distance used to calculate intermediate points. DELFACT = 1.732 (or $\sqrt{3}$ ) is my standard value. See also the angularity algorithm under section I3DPTS.
RSPECS(7)	PS	PTA IGL	Distance interval between adjacent final grid-line points.
RSPECS(8)	PFNISH	CHK	Parallel axis coordinate of last point (northernmost or easternmost) of any basic grid line.
RSPECS(9)	ZDIFF	CHK	Maximum difference in adjacent z-coordinate points along basic grid lines. Used to catch gross errors in data preparation and coding.
RSPECS(10)	SCALE	IGL	Scale of the diagram, in real (user) units per inch on the paper.
RSPECS(11)	APX	IGL	Paper x-coordinate, given in inches, of the near corner of the first block position of the rectangular subarea considered (see Figure 7), whether or not the block is actually plotted.
RSPECS(12)	APY	IGL	Paper y-coordinate, as above.
RSPECS(13)	GAMMA	IGL	Apparent angle of view, in degrees, measured from the horizontal downward. The possible range of values is 0. to approximately $54.7^\circ$ .
RSPECS(14)	PSI	IGL	Direction of line-of-sight, in degrees, measured clockwise from due north, 0. to $359.9^\circ$ . Refer to Table 1 for tables of conversion into $\alpha_1$ and $\alpha_2$ , or to equations (12) and (13). No internal check is made on compatibility of $\psi$ and $\gamma$ , so select values with care.
RSPECS(15)	FRAME	IGL	Set = 1. if frames are wanted, or = 0. if frames are not wanted.  If no frames are wanted, no need to specify RSPECS(16) through (20) inclusive.
RSPECS(16)	TICKS	IGL	Set = 1. if tick marks are wanted, or = 0. if not.  If no tick marks are wanted, no need to specify RSPECS(17) through (20) inclusive.
RSPECS(17)	MAJINT	IGL	Major tick interval, i.e. the distance (in real user units) between adjacent major tick marks.
RSPECS(18)	MININT	IGL	Minor tick interval, i.e. the distance between adjacent minor tick marks. Caution: MININT must divide evenly into MAJINT. If only one size tick

mark is desired, either set RSPECS(20) = RSPECS(19) or set RSPECS(18) = RSPECS(17).

RSPECS(19)	MAJLNT	IGL	Major tick mark length, given in inches.
RSPECS(20)	MINLNT	IGL	Minor tick mark length, given in inches.
RSPECS(21)	LABEL	IGL	Set = 1, if the standard explanation is wanted, or = 0, if it is not (i.e. if you want to make your own explanation or if you do not want an explanation). See Example 2 for the format of the standard explanation.
If standard explanation is not wanted, no need to specify RSPECS(22) and (23). RSPECS(24) through (27) inclusive are returned from I3D1GL and can be used for new or additional labelling.			
RSPECS(22)	YPOSL	IGL	Paper y-coordinates, given in inches, of base of top line of standard explanation, if standard explanation is used. YPOSL must be $\geq 3.8$ inches above the lower edge of the paper to allow room for the full explanation.
RSPECS(23)	XPOSL	IGL	Paper x-coordinate, given in inches, of left edge of any line of the standard explanation. If XPOSL set = -1., then explanation will automatically be placed starting 9 inches to the left of the left-most data point position, or if that is not possible, at 1 inch to the right of the defined plotting area.
RSPECS(24)	VDATAP	IGL	(Returned from I3D1GL). Elevation (z-coordinate) of the near corner data point of the first drawn block. For elevation reference in labelling.
RSPECS(25)	XFRSVE	IGL	(Returned from I3D1GL). Paper x-coordinate, given in inches, of the left-most data point position of the plot. For use in placing explanation.
RSPECS(26)	CPC1	IGL	(Returned from I3D1GL). Parallel-axis coordinate of the near corner of the first block position (not necessarily the first block drawn).
RSPECS(27)	CTC1	IGL	(Returned from I3D1GL). Transverse-axis coordinate of the near corner of the first block position.
RSPECS(28)	PLSEP	IGL	Separation of blocks along parallel-axis direction, given in inches. One-half inch (.5) is commonly used. If only one block is to be drawn, set = 0.
RSPECS(29)	TLSEP	IGL	Separation of blocks along transverse-axis direction, as above.
RSPECS(30)	ZFACTR	IGL	Factor of vertical exaggeration or contraction. If no exaggeration wanted (i.e. true scale), set = 1. If 10x vertical exaggeration wanted, set = 10. If one-fourth vertical scale wanted, set = .25, etc. Tick marks are scaled accordingly.

List and Description of the ISPECS Array (Integer Numbers)

Suggested			
Parameter	Mnemonic	Subroutines	Description
ISPECS(1)	MAXBGP	CHK CVT PTS	Maximum number of basic grid-line data points per grid line.
ISPECS(2)	NUMGL	CVT PTS PTA IGL	Number of grid lines total, including intermediate lines if any. The total number of grid lines (hence logical records) input into TAPE83 for use by I3D1GL.
ISPECS(3)	INTLIN	CVT PTS	Number of intermediate lines between two adjacent basic grid lines.

ISPECS(4)	MAXIGP	PTS PTA	Maximum number of calculated skeleton points per intermediate grid line. If the points are calculated using I3DPTS, then MAXIGP = 2 * ISPECS(1).
ISPECS(5)	NUMFPT	PTA IGL	Number of final grid-line points in any final grid line.
ISPECS(6)	LNEDIR	CHK IGL	Direction of data grid lines. Set = 1 if N-S lines, set = 2 if E-W lines.
ISPECS(7)	BLOCKP	IGL	Number of rows of blocks that are running parallel to data grid lines. BLOCKP + 1 is the size of CTC array (part of BUFI array). See Figure 7.
ISPECS(8)	BLOCKT	IGL	Number of rows of blocks running transverse to data grid lines. BLOCKT + 1 is the size of CPC array (part of BUFI array). See Figure 7.
ISPECS(9)	LSKIP	IGL	The number plus one of grid lines in file 83 to skip at execution of I3D1GL, e.g. if you want to draw only every third grid line (i.e. skip 2), set LSKIP = 3. If none to be skipped, set LSKIP = 1. Note that RSPECS(1) and ISPECS(2) remain the same regardless of value of LSKIP. See section D of I3D1GL.
ISPECS(10)	PTSKIP	IGL	The number plus one of data (z-coordinate) points in file 83 to skip at execution time, examples as above. Note that RSPECS(7) and ISPECS(5) remain the same regardless of value of PTSKIP. See section D of I3D1GL.

In addition, for I3D1GL, provision must be made for general plotting system parameters. At Berkeley, parameters are held in a special array, SPECS(30). SPECS(1-8), (11-12) are declared in the MAIN program and define general plotting bounds, data scaling and system constants. I3D1GL calculates projected data-point coordinates in graph-paper inches, so in your plotting system no data scaling should be used.

SPECS(13-15), (17-23), (28) are calculated within I3D1GL and its subroutines, so you should not declare them in the MAIN program. The following definitions, abstracted from the Berkeley Graphical Display System (GDS) manual, are given in order that appropriate parameters may be substituted when I3D1GL is adapted to other computer systems.

- SPECS(13) specifies the total number of data points to be plotted.
- SPECS(14) specifies the number plus one of X-array points to be skipped between adjacent plotted points.
- SPECS(15) specifies the number plus one of Y-array points to be skipped.
- SPECS(17) specifies the base dimension of the rectangle in which a plot symbol or character is defined.
- SPECS(18) specifies the height dimension of the rectangle.



- SPECS(19) specifies the additional separation distance between adjacent text characters.
- SPECS(20) specifies the rotation in degrees of a line of text.
- SPECS(21) specifies the character set to be used for text.
- SPECS(22) specifies the X distance to the lower left corner of the first character of text.
- SPECS(23) specifies the Y distance to the lower left corner of the first character of text.
- SPECS(28) specifies the number of decimal places to be used.

### Point Coordinate Data Structure

Some details are given under subroutine headings, but an overview here is necessary. Points defining the surface in space are described by  $(x, y, z)$  coordinates. For purposes of the I3D subroutines, the points must be arranged in parallel rows called grid lines (see Fig. 4 and 5). Grid lines may be north-south trending (parallel to the  $y$ -axis) or east-west trending (parallel to the  $x$ -axis), as defined by ISPECS(6). Each grid line of points constitutes a logical record.

Because of the regular (gridded) arrangement of data points, the I3D subroutines require only partial coordinate information, calculating the rest internally. I3DCHK, I3DCVT, I3DPTS, and I3DPTA require for each grid line a sequence of point coordinate pairs  $(x, z)$  or  $(y, z)$  depending on line direction. The points must be arranged (or calculated) in sequential order so that  $(x \text{ or } y)_{i+1} > (x \text{ or } y)_i$ . Grid lines

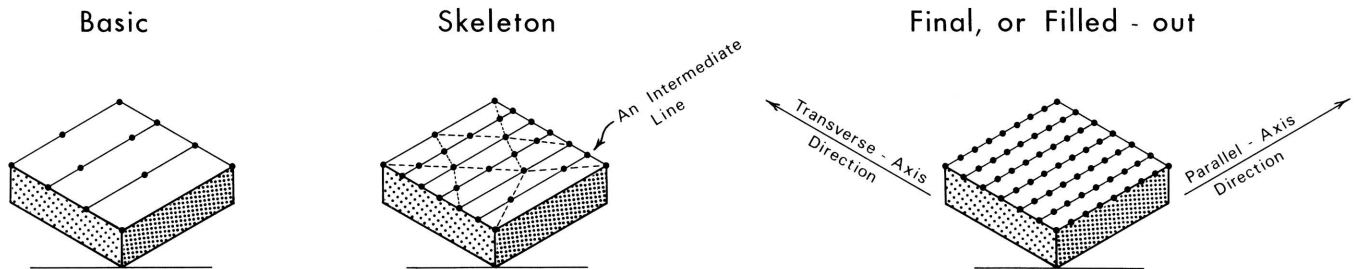


Figure 4. - Types of grid lines and points.

Three GDS subroutines are called from I3D1GL and its subroutines, and these, similar to the SPECS array, must be replaced by their counterparts if I3D1GL is used elsewhere than Berkeley. SLLILI serially connects a set of points with straight lines. TITLEG prints a Hollerith explanation. DECVAL prints a floating-point or integer number. GDSSEND, used in MAIN programs, terminates plotting records.

must be considered sequentially as well. Figure 5 illustrates point and line relationships. I3D1GL requires even less point coordinate information, because all points on grid lines are spaced equally. A logical record (one grid line) for use of I3D1GL consists of sequential  $z$ -coordinates only, each  $z$ -coordinate representing one point.

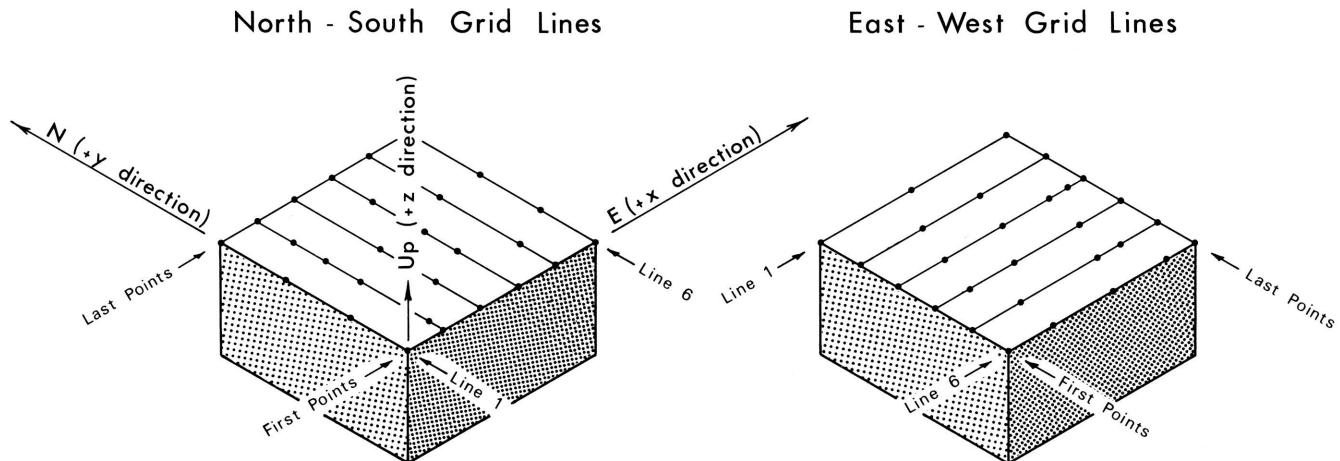


Figure 5. - Grid line and point conventions.

## I3D SUBROUTINES - USAGE

### Calling Program

The calling program, although variable in detail according to the needs of specific subroutines, must contain the following nonexecutable elements.

- (a) JOB CARD, naming all input/output files required by the subroutines to be called, as well as any other needed files. File combinations required are given under each subroutine heading. There is no conflict of file names between subroutines.
- (b) COMMON/WSPECS/RSPECS(30), ISPECS(10)
- (c) Work array BUFI (LNGTHB), where LNGTHB is the maximum array length required by individual I3D subroutines. If LNGTHB is large, it is advantageous to place BUFI into unlabelled common where it will overlay the loader. A maximum of about 1680<sub>10</sub> locations may be saved this way.

### Subroutine I3D1GL

I3D1GL maps a three-dimensional surface, a single-valued function of two variables, into isometric or other similar pictorial representation. One direction of grid lines is used for shading and relief. Because of this subroutine's importance it is discussed first, although in the calling sequence it would be called after other I3D subroutines. It can also be used alone (see Fig. 6).

#### A. JOB CARD with possible file combinations.

- (1) PROGRAM MAIN (OUTPUT, TAPE83, TAPE99)

For use when point data already exists on TAPE83. Point data logical records must not be preceded on TAPE83 by other logical records. TAPE99 is the logical tape unit for recording construction codes generated by the plotting subroutines.

- (2) PROGRAM MAIN (INPUT, OUTPUT, TAPEi = INPUT, TAPE83, TAPE99)

For use when the logical records are punched on binary cards (i.e. from I3DCVT, I3DPTA, or other routines). Your main program must read the records off the INPUT file (TAPEi) and transfer them to TAPE83 prior to calling I3D1GL.

#### B. Required specifications. These must be declared

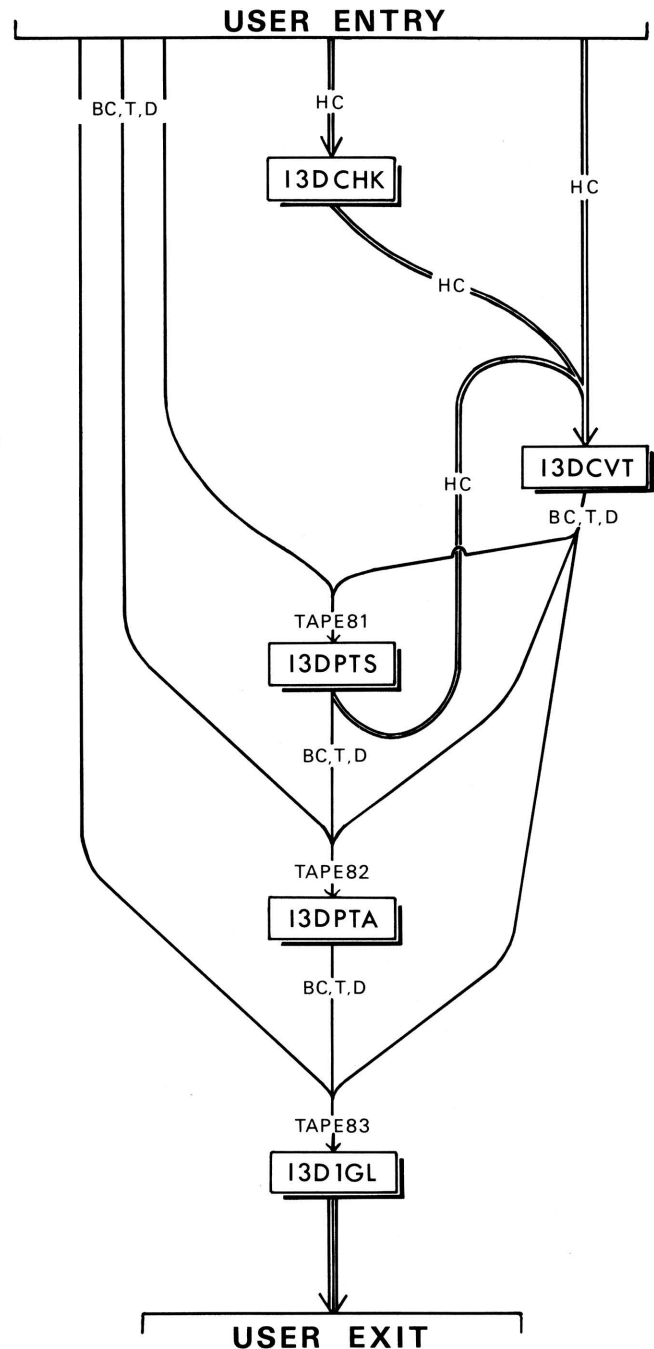


Figure 6. - User flowsheet guide to use of I3D subroutines. HC means Hollerith cards, BC means binary cards, T means magnetic tape, and D means disk storage.

in the main program prior to calling I3D1GL.

RSPECS (1-5), (7), (10-23), (28-30)

Depending on options chosen, some of these do not have to be declared. See RSPECS listing for details.

RSPECS (24-27) are returned from I3D1GL and may be used for labelling.

ISPECS (2), (5-10)

C. FORTTRAN calling sequence.

CALL I3D1GL (BUFI, LNGTHB, SPECS)

LNGTHB must be set  $\geq 4*ISPECS(5) + 2*ISPECS(7)*ISPECS(8) + ISPECS(7) + ISPECS(8) + \text{larger of } ISPECS(7), ISPECS(8) + 2*ISPECS(2) + 3$

D. Other information required.

Certain information must be entered into portions of the array BUFI prior to calling I3D1GL. Array addresses in BUFI are tabulated as follows.

$$\begin{aligned} AA1 &= 4*ISPECS(5) + 1 \\ AA2 &= AA1 + ISPECS(7)*ISPECS(8) - 1 \\ AA3 &= AA2 + ISPECS(7)*ISPECS(8) + 1 \\ AA4 &= AA3 + ISPECS(7) \\ AA5 &= AA4 + 1 \\ AA6 &= AA5 + ISPECS(8) \end{aligned}$$

- (1) That portion of BUFI array from (AA1) to (AA2) inclusive is used to determine if a particular rectangular block of data points is to be plotted or skipped. Blocks are bounded by CPC and CTC coordinates (see Fig. 7). Block number 1 is always in the southwest corner of the subarea to

be considered for plotting, regardless of the angle-of-sight, RSPECS(14), or direction of grid lines, ISPECS(6). Block number 2 is always in the next position in the transverse direction, and so on as illustrated. If block  $i$  is to be plotted, set  $BUFI(AA1 + i - 1) = 1$ . If not, set it = 0.

- (2) Those portions of BUFI from (AA3) to (AA4) and from (AA5) to (AA6) are used to determine the bounds of blocks within the subarea considered for plotting. The first portion can be thought of as equivalent to a dummy array CTC of length  $ISPECS(7) + 1$ , and the second portion can be thought of similarly as a dummy array CPC of length  $ISPECS(8) + 1$ .  $CPC(1)$  is always the smallest parallel direction coordinate, and so on in increasing order if grid lines are north-south. If grid lines are east-west,  $CTC(1)$  is the largest transverse direction coordinate and so on in decreasing order. Figure 7 illustrates the situation for east-west grid lines.

Some restrictions exist on possible values for CTC and CPC. All  $CTC(i)$  must be equal to the transverse-axis coordinate of a grid line. Furthermore, if  $ISPECS(9) > 1$ , that is if lines are to be skipped at execution, additional caution is needed. The first block may start on any grid line, which thus becomes the first line, but all succeeding block  $CTC(i)$  must lie on a drawn (not skipped) grid line.

An exactly parallel situation exists for CPC.

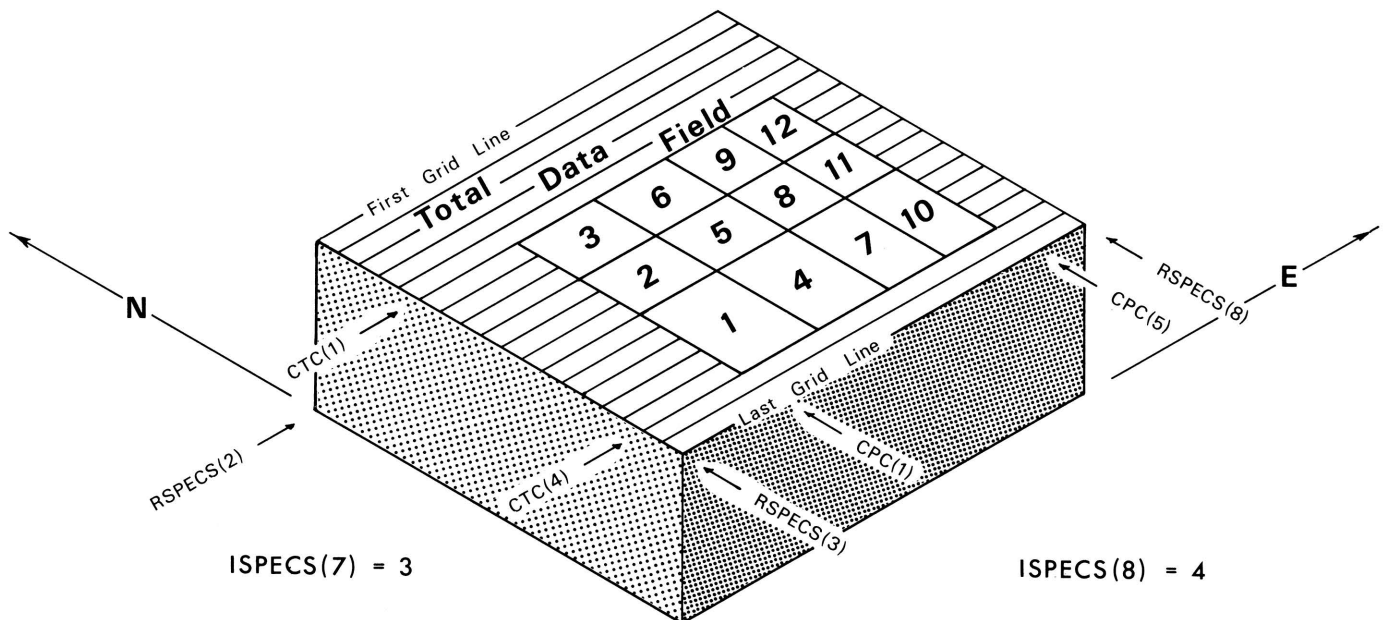


Figure 7. - Block diagram showing a possible relationship of input data points to drawn subareas. See text for explanation.

All CPC(i) must be equal to the parallel-axis coordinate of a point on a grid line and if ISPECS(10) > 1, the same caution must be exercised.

#### Subroutine I3DCHK

I3DCHK is a small, independent subroutine which can be used to catch gross keypunching errors and data cards out of place in a Hollerith data deck. Basic and skeleton data points, in order to be acceptable to I3DCVT, must satisfy the following relationships.

- (1) Points are arranged in data grid lines.
- (2) All lines must begin and end by data points with parallel-axis coordinates RSPECS(3) and RSPECS(8) respectively.
- (3) Each data point is represented by a pair of coordinates, (y, z) if north-south grid lines or (x, z) if east-west grid lines. The north (or east) coordinate must be monotonically increasing (e.g.  $x_i + 1 > x_i$  for all i).
- (4) Each grid line (logical record) must be terminated by a user-option special end-of-record (EOR) punch in the last north (or east) coordinate position on a data card.
- (5) The set of logical records is terminated by a 'double' EOR, the identical EOR punch in the z-coordinate position as well.
- (6) Any configuration of blank cards or spaces is allowed. This permits easy data change or update. Note that, because of this feature, any point with a parallel-axis coordinate of 0. is ignored.

#### A. JOB CARD with files required.

- (1) PROGRAM MAIN (INPUT, OUTPUT)

#### B. Required specifications.

RSPECS (3), (8-9)  
ISPECS (1), (6)

#### C. FORTTRAN calling sequence.

CALL I3DCHK (BUFI, LNGTHB, NUMPTC, FMT, EOR)  
LNGTHB must be set  $\geq 2 * \text{NUMPTC}$   
NUMPTC is the number of data point pairs per data card. Maximum value is thus 40.  
FMT represents up to 25 Hollerith characters describing the format of the data on a card.

Example: 16H(10X, 6(F6.3, F5.1)), 16 Hollerith characters.

EOR is the special (and unique) number to be used as an end-of-record and end-of-file marker. The use of this is described above.

#### Subroutine I3DCVT

I3DCVT reads a Hollerith data deck, possibly with embedded blanks, and reduces the data to a set of binary logical records, on TAPE81, TAPE82, or TAPE83 as specified in the calling list, suitable for direct input into I3DPTS, I3DPTA, or I3D1GL respectively. Remember to rewind or make certain the tape unit is at the load point prior to calling I3DCVT. Any of the units can be equivalenced to PUNCHB in the JOB CARD, thus permitting a binary deck to be punched. After calling I3DCVT, if I3DPTS or I3DPTA is to be called from this main program, you must rewind the tape unit to just before the first logical record written.

#### A. JOB CARD with possible file combinations. See Figure 6 also.

- (1) PROGRAM MAIN (INPUT, OUTPUT, TAPEi)  
i = 81, or 82, or 83

For use when I3DPTS, I3DPTA, or I3D1GL is called from the same main program, or when the data logical records are written onto magnetic tape for later use.

- (2) PROGRAM MAIN (INPUT, OUTPUT, PUNCHB, TAPEi=PUNCHB)

For use if data are to be punched on binary cards for later use.

#### B. Program specifications.

ISPECS (1-3)

#### C. FORTTRAN calling sequence.

CALL I3DCVT (BUFI, LNGTHB, NUMPTC, FMT, EOR,

[6HTAPE81], [6HTAPE82], [6HTAPE83], [6HPNCHOT], [6HNOPNCH] )

LNGTHB must be set  $\geq 4 * \text{ISPECS}(1) + \text{ISPECS}(2)$   
NUMPTC, FMT, EOR are described in the section on FORTRAN calling sequence of I3DCHK.

The tape parameter, which must be one of the three given, must correspond to the tape unit declared on the JOB CARD.

The punch parameter, which must be one of the

two given, determines whether or not a binary record, the array NUMPT, will be punched, each word of which contains in order the number of points on a single grid line. Word 1 corresponds to grid line 1, and so on. There are three possible situations which may arise.

- (1) I3DPTS, I3DPTA, or I3D1GL will be called from the same main program. No data binary cards are to be punched and the punch parameter chosen must be 6HNOPNCH.
- (2) No other I3D subroutine will be called now, TAPEi is equivalenced to PUNCHB in the JOB CARD, and data binary cards are to be punched. If i is equal to 81 or 82, choose 6HPNCHOT as the punch parameter; the last logical record punched will be the array NUMPT.
- (3) No other I3D subroutine will be called now. The data logical records are to be stored on magnetic tape equivalenced to the files TAPE81, TAPE82, or TAPE83. If tape unit is 81 or 82, choose 6HPNCHOT as the punch parameter; the array NUMPT will be written as the last record on the tape.

#### Subroutine I3DPTS

I3DPTS reads an array of data points on basic grid lines and calculates points on any number of intermediate lines, resulting in an array of points on skeleton grid lines. Points on basic grid lines may be regularly or irregularly spaced, and the number of points per line may range between the limits 2 and ISPECS(1). Each line, however, must begin and end with fixed parallel-axis coordinates RSPECS(3) and RSPECS(8) respectively, and each successive point parallel-axis coordinate must be greater than the preceding one, within a given grid line (e.g.  $x_{i+1} > x_i$  for all i).

I3DPTS uses linear interpolation between points on adjacent basic grid lines to calculate points on intermediate lines. I3DPTS is unusual, however, in that angularities between horizontal and inclined portions of the data surface are preserved in calculation of intermediate line points. Ordinary linear interpolation of irregularly spaced points would generally result in intermediate lines showing rounded corners where they should be angular. This may be of some importance in the representation of artificially created topography (see Example 2) and other surfaces. Data points ideally need only be entered at breaks in slope, thus minimizing the number of points needed to represent the surface fully.

The algorithm for preserving angularities is not perfect, and certain extreme and generally unusual

basic data point arrangements will cause aberrations. Perfection may be difficult to achieve, in part because of the problem of unintentional angularity situations created by a normally rolling surface. As a guide to proper selection of data-point positions to minimize plot aberrations, the basic algorithm is given. Numbers and letters correspond to numbers and letters in comment cards in I3DPTS listing. If you are not concerned with angularities and wish a simple linear interpolation, there is little need to study the algorithm, except to note the importance of DELTAD, derived from RSPECS(6), in 2iv.

#### I3DPTS angularity algorithm

- (1) Consider a first grid line A and a second, adjacent, grid line B. Consider a point i on line A.
- (2) Consider the point j on line B last used for interpolation and the next point j + 1.
  - (i) If both  $B_j$  and  $B_{j+1}$  are of the same elevation (z-coordinate) as  $A_i$ , then use both with  $A_i$  to form two new grid points for each intermediate line (linear interpolation).
  - (ii) If  $B_j$  is not at the same elevation as  $A_i$  but  $B_{j+1}$  is, then consider  $B_{j+2}$ .
    - (a) If  $B_{j+2}$  is at the same elevation as  $B_{j+1}$  and  $A_i$ , and at least one of  $B_{j+1}$ ,  $B_{j+2}$  is within DELTAD parallel-axis distance of  $A_i$  (see RSPECS(6) description), then use  $B_{j+1}$ , for linear interpolation.
    - (b) If  $B_{j+2}$  is not at the same elevation, and if at least one of  $B_j$ ,  $B_{j+1}$  is within DELTAD of  $A_i$ , then use  $B_j$ ,  $B_{j+1}$  for linear interpolation.
  - (iii) If  $B_j$  is at the same elevation as  $A_i$ , but  $B_{j+1}$  is not, and if at least one of  $B_j$ ,  $B_{j+1}$  is within DELTAD of  $A_i$ , then use  $B_j$ ,  $B_{j+1}$  for linear interpolation.
  - (iv) If neither  $B_j$  nor  $B_{j+1}$  is at the same elevation as  $A_i$ :
    - (a) Test additional B points to see if there are two consecutive B points, at least one of which is within DELTAD of  $A_i$ , that are both equal to the elevation of  $A_i$ . If so, use the two B points for linear interpolation. If not, go on to b.
    - (b) Starting with  $B_j$ , consider, in order, up to a maximum of two B points for linear interpolation. Each B point so used must be within DELTAD of  $A_i$ .
  - (v) Cycle until all A points and all B points are exhausted.

If I3DPTS calculates erroneous points and these prove objectionable when plotted, they may be corrected as follows. Run I3DPTS a second time, specifying a Hollerith format in the argument list.

A complete skeleton-array data deck will be punched, and the point coordinates in error can be readily corrected. Rerun the corrected deck, calling I3DCVT, I3DPTA, and I3DIGL.

I3DPTS presents one general approach to the problem of calculating additional data lines. Other algorithms may prove equally or better suited to your particular application. The I3D subroutines are structured so that substitution of one or several other subroutines as needed should be fairly simple and straightforward.

A. JOB CARD with possible file combinations.  
See Figure 6 also.

- (1) PROGRAM MAIN (OUTPUT, TAPE81, TAPE82)

For use when basic point data to be read are contained on TAPE81, generally direct from I3DCVT, and I3DPTA will be called next from the current main program, or the calculated skeleton point array logical records are to be written onto magnetic tape for later use.

- (2) PROGRAM MAIN (INPUT, OUTPUT, TAPE81=INPUT, TAPE82)

For use when basic point data to be read are contained in file INPUT, that is when a binary card deck is to be read.

- (3) PROGRAM MAIN ( $\overline{\text{INPUT}}$ , OUTPUT, PUNCHB,  $\left[ \begin{array}{l} \text{TAPE81} \\ \text{TAPE81=INPUT} \end{array} \right]$ , TAPE82=PUNCHB)

For use when the skeleton point array calculated by I3DPTS is to be output as punched binary cards, one logical record per grid line.

- (4) PROGRAM MAIN ( $\overline{\text{INPUT}}$ , OUTPUT PUNCH,  $\left[ \begin{array}{l} \text{TAPE81} \\ \text{TAPE81=INPUT} \end{array} \right]$ )

For use when the skeleton point array is to be output as punched Hollerith cards, according to the format specified in the CALL I3DPTS argument list. Terminating each set of cards which contains the coordinate-pairs of all points on a single grid line is a blank card.

- (5) PROGRAM MAIN ( $\overline{\text{INPUT}}$ , OUTPUT, PUNCH, PUNCHB,  $\left[ \begin{array}{l} \text{TAPE81} \\ \text{TAPE81=INPUT} \end{array} \right]$ ,

TAPE82=PUNCHB)

For use as number 4, but in addition at the end a binary logical record is punched, each word of which contains the number of points on a single grid line.

B. Program specifications.

RSPECS (1), (6)  
ISPECS (1-4)

C. FORTTRAN calling sequence.

CALL I3DPTS (BUFI, LENGTB,  $\left[ \begin{array}{l} \text{6HPNCHOT} \\ \text{6HNOHOLP} \\ \text{6HNOPNCH} \end{array} \right]$ ,  $\left[ \begin{array}{l} \text{FMT, NUMPTC} \end{array} \right]$ )

LENGTB must be set  $\geq 4*ISPECS(1) + ISPECS(2) + 2*ISPECS(3)*ISPECS(4)$

The punch parameter, which must be either 6HNOPNCH or 6HPNCHOT, determines whether or not a binary record, the array NUMPT, will be punched, each word of which, in order, contains the number of points on a single skeleton grid line. Word 1 in the array corresponds to grid line 1, and so on. There are four possible situations which may arise.

- (1) I3DPTA will be called from the same main program. No data binary cards are to be punched and the punch parameter chosen must be 6HNOPNCH.
- (2) I3DPTA will not be called now, and the data logical records are to be stored on magnetic tape equivalenced to file TAPE82. Choose 6HPNCHOT as the punch parameter; the array NUMPT will be written as the last record on the tape. For later entry into I3DPTA, this record must be read from tape into the work array BUFI at location SA3 prior to calling the subroutine.
- (3) I3DPTA will not be called now, TAPE82 is equivalenced to PUNCHB in the JOB CARD, and data logical records are to be punched. Choose 6HPNCHOT as the punch parameter; the NUMPT array will be punched as the last logical record. Note that, for later entry into I3DPTA, this last record must be placed first and a single READ executed prior to calling the subroutine, to place the record into the work array BUFI beginning at location SA3.
- (4) Hollerith skeleton-array data cards are to be punched according to the format specified in the subroutine argument list.

- (a) If NUMPT array is desired (note that it is not necessary for entry into I3DCVT), specify 6HPNCHOT. The record is written in binary at the end of the Hollerith deck.
- (b) If NUMPT array is not desired, specify 6HNOPNCH.

The format parameter must be either 6HNOHOLP or a combination of FMT and NUMPTC in the order given. If 6HNOHOLP is specified, then no Hollerith data cards are punched. If a Hollerith format is given (see the section on FORTRAN calling sequence of I3DCHK for explanation), then each grid-line logical record is punched in Hollerith mode on cards, with a blank card separating records. Note that all EOR punches must be added afterwards. A word of caution: Hollerith output is punched with the decimal point included, so be certain to include the decimal point in the format declaration. Example: the number 32500. can be read in under format F5.0, but must be punched under format F6.0.

D. Other information required.

If data point logical records are on binary cards or magnetic tape, and I3DCVT has not been called from this main program, then part of the work array BUFI must be filled with the array NUMPT as punched on cards or written on magnetic tape from I3DCVT. Location AA1 within BUFI is equal to  $4 * ISPECS(1) + 1$ .

- (a) If the data are on binary cards, take the last logical record punched from I3DCVT and place it first in the data deck. NUMPT must be read into the work array BUFI beginning at location AA1, prior to calling I3DPTS. Because ISPECS(2) is, and must be, greater than the number of basic grid lines, the words in this first logical record must be spaced in BUFI accordingly. An example will make this clear.

Example: Number of basic grid lines = 101  
 ISPECS(2) = final number of grid lines = 301  
 (ISPECS(3) = 2)  
 and say ISPECS(1) = 200  
 READ (81) (BUFI(I), I=801, 1101, 3)

CALL I3DPTS (BUFI, LNGTHB, . . .)

- (b) If the data are on magnetic tape, the

procedure is identical except NUMPT will be read directly from the tape.

Subroutine I3DPTA

I3DPTA reads an array of data points on skeleton grid lines and calculates a final, or filled-out, orthogonal array of points suitable for direct input into I3D1GL. Points read are defined by two coordinates, elevation and parallel-axis, whereas points calculated within I3DPTA are defined by only one coordinate, elevation, because the other two may be calculated as needed. Linear interpolation is used to calculate final points.

A. JOB CARD with possible file combinations.

- (1) PROGRAM MAIN (OUTPUT, TAPE82, TAPE83)

For use when skeleton point data to be read are contained on TAPE82, generally direct from I3DPTS, and I3D1GL will be called next from the current main program, or the calculated filled-out point array logical records are to be written onto magnetic tape for later use.

- (2) PROGRAM MAIN (INPUT, OUTPUT, TAPE82=INPUT, TAPE83)

For use when skeleton point data to be read are contained in file INPUT, that is when a binary card deck is to be read.

- (3) PROGRAM MAIN ( $\overline{[INPUT]}$ , OUTPUT, PUNCHB,  $\left[ \begin{array}{l} TAPE82 \\ TAPE82=INPUT \end{array} \right]$ , TAPE83=PUNCHB)

For use when the filled-out point array is to be output as punched binary cards, one logical record per grid line.

B. Program specifications.

RSPECS(7)  
 ISPECS(2), (4-5)

C. FORTRAN calling sequence.

CALL I3DPTA (BUFI, LNGTHB)  
 LNGTHB must be set  $\geq 2 * ISPECS(4) + ISPECS(2) + ISPECS(5)$

D. Other information required.

As in the case with I3DPTS, if data point logical records are contained in binary cards or

magnetic tape, and I3DPTS or I3DCVT has not been called from this main program, then part of the work array BUFI beginning at location  $2 * ISPECS(4) + 1$  must be filled with the complete array NUMPT as punched on cards or written on magnetic tape from I3DCVT or I3DPTS. The procedure is exactly analogous to that described in section D. of I3DPTS, except that the NUMPT array is complete so that, in the example given, the READ statement should be

```
READ (82) (BUFI(I), I=801, 1101).
```

## EXAMPLES

Three examples are included to illustrate use of I3D subroutines. The calling programs show the parameters used. Subroutine listings are given with Examples 1 and 2 (see Appendix).

Example 1 illustrates use of I3DCHK. Errors were introduced into the first seven grid lines of a data deck to show the types of diagnostic messages printed. Figure 8 reproduces the printed output, and Figure 9 is a listing of the complete data deck.

Example 2 illustrates use of I3DCVT, I3DPTS, I3DPTA, and I3D1GL called from the same main program. Seventy-six basic grid lines of data points

were read in, containing a total of approximately 4500 (north, elevation) points taken at breaks in slope. From these initial points, 121,102 final points were calculated using I3DPTS and I3DPTA, and these points were transformed into the isometric diagram shown in Figure 10, by I3D1GL. Execution times (central processor) for the various subroutines are:

I3DCVT	3.9 seconds
I3DPTS	4.4 seconds
I3DPTA	13.3 seconds
I3D1GL	61.0 seconds

The plotted surface resembles the actual surface, and elevation variations of only a few feet (at this scale) can be seen easily. Attention is drawn to four east-west streets in the southerly block.

Example 3 (Appendix) illustrates use of I3D1GL alone in portraying a mathematical function. This particular function (see the example main program listing) was chosen to show the effect of sharp peaks in the data (Figure 11). I3D1GL execution time was 12.6 seconds.

All examples were run on a Berkeley Computer Center CDC 6400 computer with disk storage unit. Plotting was done on a 31-inch CalComp plotter monitored by an IBM 360/40. All plotter software were written at Berkeley.

### SUBROUTINE I3DCHK

```
NORTH COORD. OF FIRST POINT ON N-S LINE IS 32000.0000
NORTH COORD. OF LAST POINT ON N-S LINE IS 32800.0000
MAXIMUM ALLOWABLE NUMBER OF POINTS PER N-S LINE IS 110
IF SUCCEEDING ELEVATIONS DIFFER BY MORE THAN 67.0000, AN ERROR MESSAGE IS PRINTED
```

```
THE NORTH COORD. OF N-S LINE NUMBER 3, CARD 1, POINT 3, IS INCORRECT.
CHECK ALSO THE ELEVATION COORDINATE.
```

```
FIRST POINT ON N-S LINE NUMBER 4 IS INCORRECT
```

```
THE NORTH COORD. OF N-S LINE NUMBER 5, CARD 2, POINT 1, IS INCORRECT.
CHECK ALSO THE ELEVATION COORDINATE.
```

```
THE ELEVATION COORD. OF N-S LINE NUMBER 5, CARD 2, POINT 1, IS INCORRECT.
```

```
THE ELEVATION COORD. OF N-S LINE NUMBER 5, CARD 3, POINT 1, IS INCORRECT.
```

```
THE ELEVATION COORD. OF N-S LINE NUMBER 5, CARD 3, POINT 2, IS INCORRECT.
```

```
FOR N-S LINE NUMBER 6, EITHER THE FLAG ELEVATION OR THE PRECEDING POINT ELEVATION IS MISPUNCHED.
NO TEST IS MADE TO CHECK LAST INPUT POINT NORTH COORDINATE.
```

```
THE NORTH COORD. OF N-S LINE NUMBER 7, CARD 2, POINT 4, IS INCORRECT.
CHECK ALSO THE ELEVATION COORDINATE.
```

```
LAST POINT ON N-S LINE NUMBER 7 IS INCORRECT.
```

```
NUMBER OF BASIC GRID LINES = 26
NUMBER OF BASIC GRID POINTS = 349
```

Figure 8. - Printed output from I3DCHK, using data given in Figure 9.



32000	575032059	577032141	576032220	574032360	572032479	570032598	563332800	5633 99999
32000	574532045	577032130	575632200	5734 32300	571532370	570332443	567032520	5633 99999
32618	5633	32800	5633					99999
32000	574032039	576530180	575032180	572032269	569032338	566232406	563332521	5633 99999
32577	560032750	560032800	5600					99999
32477	560032604	560032640	556732800	5567				99999
32000	573532016	576032090	573032152	570032210	568032240	566232280	563332432	5633
32000	573032069	571532121	568032180	566532208	563332311	563332374	560032515	5600 99999
32540	576732600	556732800	5567					99999
32000	572032048	570032150	566032179	563332240	563332260	560332290	560032417	5600 99999
32456	556732520	556732800	5567					5567
32000	571532071	568032130	566032152	563332200	563332208	561232242	560032323	5600 99999
32359	556732420	556732750	556732700	5567				99999
32000	570532033	568032115	565732135	563332174	563332208	562532212	560032270	5600 99999
32300	556732360	556732684	556732723	553332782	553332800	5544		99999
32000	568032050	569032106	565332123	563332159	563332180	563032186	560032240	5600 99999
32261	556732317	556732655	556732700	553332800	5533			99999
32000	568032041	569032096	565032117	563332147	563332163	560032210	560032237	5567
32344	556732430	553332561	553332601	553332700	553332800	5533		99999
32000	569032040	568032090	564732104	563332134	563332150	560032191	560032219	5567
32296	556732338	553332420	553332660	553332727	553332800	5533		99999
32000	569532080	564532091	563332121	563332139	560032178	560032200	556732266	5567
32300	553332377	553332414	550032760	550032786	553332800	5533		99999
32000	567532032	565532069	564032080	563332118	563332130	560032162	560032192	5567
32258	556732290	553332355	553332379	550032800	5500			99999
32000	565532065	563832067	563332106	563332120	560032156	560032180	556732250	5567
32281	553332340	553332370	550032590	550032800	5500			99999
32000	564532058	563532060	563332091	563332109	560032143	560032172	556732250	5567
32279	553332338	553332370	550032500	550032558	546732630	546732710	550032800	5500 99999
32000	564032037	563532041	563332082	563332100	560032141	560032167	556732250	5567
32278	553332338	553332361	550032451	550032478	547032482	546732540	546732660	5467
32730	546732760	550032800	5500					99999
32000	563532016	563332070	563332081	560032130	560032156	556732250	556732280	5533
32339	553332360	550032442	550032450	547532478	546732761	546732782	550032800	5500 99999
32000	563332050	563332068	560032120	560032139	556732250	556732279	553332336	5533 99999
32359	550032435	550032440	548532463	546732779	546732800	5496		99999
32000	563332039	563332050	560032102	560032120	556732242	556732270	553332322	5533
32357	550032430	550032436	549032459	547132463	546732770	546732800	550099999	
32000	563332022	563332035	560032088	560032114	556732222	556732249	553332317	5533
32340	550032431	550032453	548032460	546732748	546732780	550032800	550099999	
32000	563332018	563332025	560032080	560032101	556732190	556732220	553332296	5533
32322	550032439	550032442	549632458	546732726	546732769	550032800	550099999	
32000	563332010	563332021	560032072	560032093	556732162	556732198	553332270	5533
32300	550032440	550032466	546732692	546732728	550032800	5500		99999
32000	563332008	563332018	560032070	560032089	556732157	556732182	553332251	5533
32280	550032459	550032483	546732650	546732695	550032779	550032800	552599999	
32000	563332018	560032066	560032088	556732157	556732186	553332250	553332278	5500
32482	550032540	546732593	546732647	550032742	550032781	553332800	553399999	
32000	562832016	560032064	560032083	556732160	556732200	553332269	553332290	5500
32558	550032700	550032737	553332800	5533				99999
32000	562832018	560032062	560032083	556732180	556732220	553332320	553332350	5500
32613	550032670	553332760	553332790	556732800	5567			9999999999

Figure 9. - Listing of data used for Example 1.

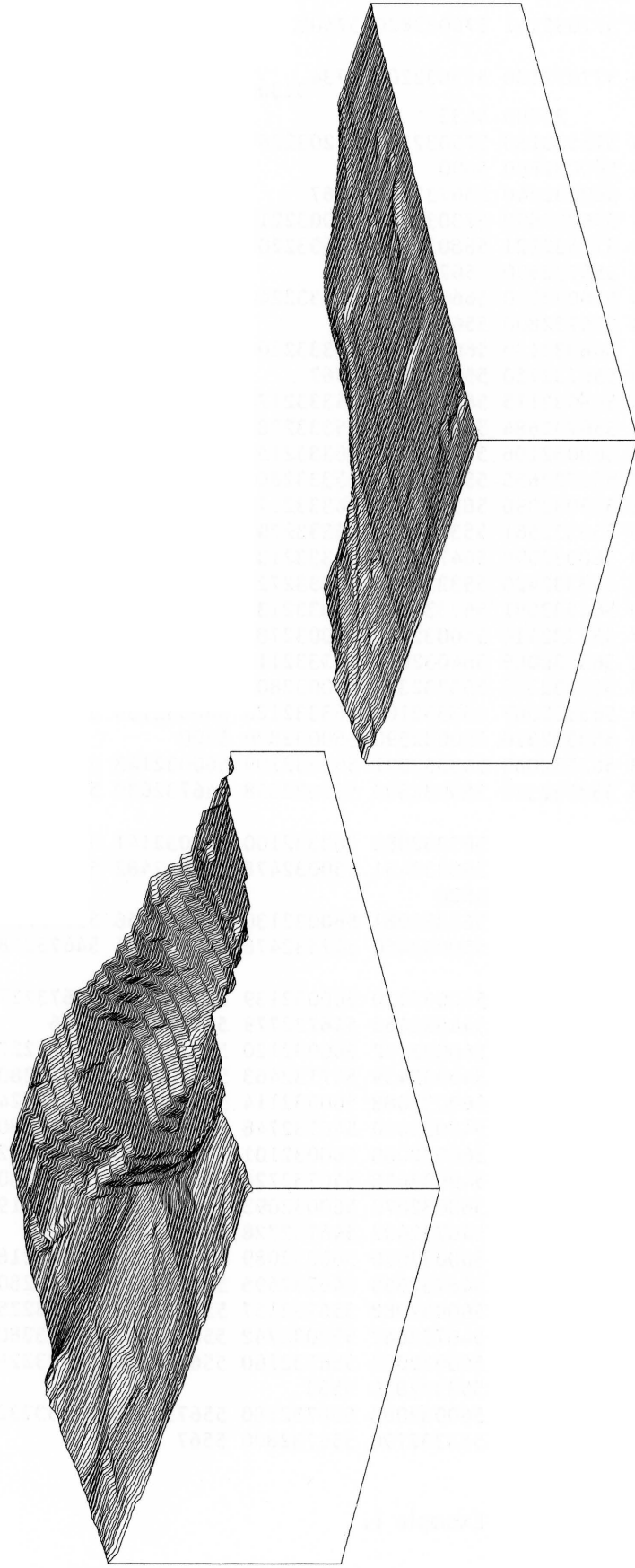
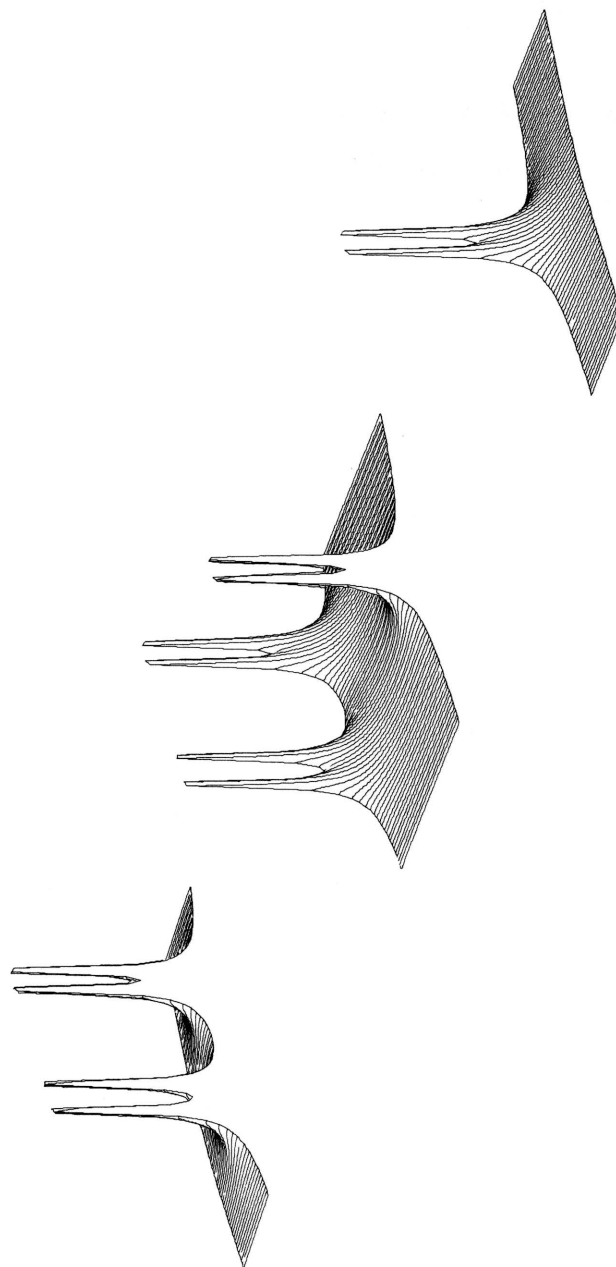


Figure 10. - View of a portion of the Berkeley open-pit mine, Butte, Montana



DIRECTION OF SIGHT N44.0E  
 INCLINATION 23.0 DEGREES

VERTICAL EXAGGERATION = 1.00  
 RESOLUTION = 71 POINTS/INCH

PROGRAM BY W.R. GRAY JR.

Figure 11.- View of mathematical function (see listing).

## REFERENCES

Lobeck, A.K., 1924, Block diagrams: John Wiley & Sons, Inc., New York, 206 p.

Rohlf, F.J., 1969, GRAFPAC, graphic output subroutines for the GE 635 computer: Kansas Geol. Survey Computer Contr. 36, 50 p.

# APPENDIX

## Example 1

```

PROGRAM MAIN (INPUT,OUTPUT)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
RSPECS (3) = 32000.
RSPECS(8) = 32800.
RSPECS (9) = 67.
ISPECS(1) = 110
ISPECS(6) = 1
CALL I3DCHK (8,8H(16F5.0),99999.)
STOP
END

```

```

SUBROUTINE I3DCHK (NP,FMT,EOR)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
COMMON /TIME/ TU
REAL COORDN(40),COORDZ(40)
DIMENSION FMT(3),LDIR1(2),LDIR2(2)
EQUIVALENCE (RSPECS(3),START), (RSPECS(8),FINISH), (RSPECS(9),ELDI
1FF), (ISPECS(1),NPOINT), (ISPECS(6),I6)
LOGICAL FRSTPT
DATA TLBL /6HI3DCHK/
DATA LDIR1(1),LDIR1(2),LDIR2(1),LDIR2(2) /3HN-S,3HE-W,5HNORTH,4HEA
1ST/

```

```

C
C--- SUBROUTINE I3DCHK READS A BASIC GRID POINT DATA DECK AND CHECKS
C--- FOR GROSS ERRORS. I3DCHK MAKES CERTAIN THAT (1) EACH RECORD STARTS
C--- WITH *START* COORDINATE AND ENDS WITH *FINISH*, (2) EACH NORTH (OR
C--- EAST) COORDINATE ON A CERTAIN GRID LINE IS GREATER THAN THE PRECEDING
C--- COORDINATE ON THE SAME LINE, (3) EACH GRID LINE ENDS WITH A SINGLE
C--- EOR AND THE LAST GRID LINE ENDS WITH A DOUBLE EOR, (4) THERE ARE
C--- NO MORE THAN *NPOINT* POINTS PER GRID LINE (A GOOD TEST FOR CATCHING
C--- MISSING EOR PUNCHES), AND (5) EACH ELEVATION COORDINATE ON A CERTAIN
C--- GRID LINE IS WITHIN +/- *ELDIFF* OF THE PRECEDING ELEVATION ( A
C--- TEST TO CATCH GROSS ERRORS IN ELEVATION PUNCHES). IF ERRORS ARE
C--- FOUND, APPROPRIATE ERROR MESSAGES ARE PRINTED.
C--- I3DCHK IGNORES BLANKS ON DATA CARDS AND USES VARIABLE CARD FORMAT,
C--- AS SPECIFIED BY USER.

```

```

C
CALL SECOND (TU)
PRINT 1
1 FORMAT (1H1, 8X, *SUBROUTINE I3DCHK*/)

```

```

C
C--- INITIALIZE COUNTERS. ICARD = NUMBER OF CARDS READ THIS GRID LINE.
C--- IN = NUMBER OF THE POINT ON THE CARD. NUMPT = NUMBER OF REAL
C--- (NON-BLANK) POINTS IN THE GRID LINE. NUMTOT = TOTAL NUMBER OF DATA
C--- POINTS (EXCLUDING FLAGS). IEAST = NUMBER OF THE GRID LINE.

```

```

C
IEAST = 1
NUMTOT = ICARD = IN = NUMPT = 0
FRSTPT = .TRUE.

```

```

    PRINT 4, LDIR2(I6),LDIR1(I6),START,LDIR2(I6),LDIR1(I6),FINISH,
    1LDIR1(I6),NPOINT,ELDIFF
4  FORMAT (10X, A5, * COORD. OF FIRST PCINT ON *, A3, * LINE IS *, F1
12.4/10X, A5, * COORD. OF LAST POINT ON *, A3, * LINE IS *, F12.4/1
20X, *MAXIMUM ALLOWABLE NUMBER OF POINTS PER *, A3, * LINE IS *, I5
3/10X, *IF SUCCEEDING ELEVATIONS DIFFER BY MORE THAN *, F12.4, *, A
4N ERROR MESSAGE IS PRINTED*///)
C
C--- ROUTINE TO CONSIDER THE FIRST NON-ZERO POINT OF THE CARD.
C
5  READ FMT, (COORDN(I), COORDZ(I),I=1,NP)
    ICARD = ICARD + 1
    IF (.NOT. FRSTPT) GO TO 7
9  IF (IN .LT. NP) GO TO 8
    IN = 0
    GO TO 5
6  IN = IN + 1
    IF (COORDN(IN) .EQ. 0.) GO TO 9
C
C--- ROUTE OF THE FIRST NON-ZERO POINT OF A GRID LINE.
C
    IF (COORDN(IN) .EQ. START) GO TO 10
    PRINT 11, LDIR1(I6), IEAST
11 FORMAT (8X, *FIRST POINT ON *, A3, * LINE NUMBER *, I4, * IS INCOR
1RECT*/)
10 FRSTPT = .FALSE.
    NUMPT = 1
    PTNSVE = COORDN(IN)
    PTZSVE = COORDZ(IN)
    IF (IN .EQ. NP) GO TO 5
    IN1 = IN + 1
    GO TO 12
C
C--- THIS ROUTE, CARD HAS JUST BEEN READ, BUT PAST THE FIRST POINT.
C
7  IN1 = 1
C
C--- NOTE THAT HERE, PTNSAVE ETC CANNOT BE ZERO OR UNDEFINED.
C--- DO LOOP TO PROCESS BALANCE OF CARD.
C
12 DO 13 I=IN1,NP
    IF (COORDN(I) .EQ. 0.) GO TO 13
    NUMPT = NUMPT + 1
    IF (COORDN(I) .GT. PTNSVE) GO TO 15
    PRINT 16, LDIR2(I6),LDIR1(I6),IEAST,ICARD,I
16 FORMAT (8X, *THE *, A5, * COORD. OF *, A3, * LINE NUMBER *, I4, *,
1 CARD *, I4, *, POINT *, I2, *, IS INCORRECT.*//16X, *CHECK ALSO TH
2E ELEVATION COORDINATE.*//)
15 IF (ABS(COORDZ(I) - PTZSVE) .LE. ELDIFF) GO TO 17
    IF (I .EQ. NP .AND. COORDN(I) .EQ. EOR) GO TO 13
    PRINT 18, LDIR1(I6), IEAST, ICARD, I
18 FORMAT (8X, *THE ELEVATION COORD. OF *, A3, * LINE NUMBER *, I4,
1 *, CARD *, I4, *, POINT *, I2, *, IS INCORRECT.*//)
17 PTNSVE = COORDN(I)
    PTZSVE = COORDZ(I)
13 CONTINUE
C
C--- TESTS ON THE LAST NON-ZERO POINT OF THE CARD.
C
    IF (NUMPT .LE. NPOINT) GO TO 14

```

```

PRINT 19, LDIR1(I6), IEAST, ECR
19 FORMAT (8X, A3, * LINE NUMBER *, I4, * HAS TOO MANY POINTS, OR A *
1, F12.4, * PUNCH IS MISSING.*/)
14 IF (COORDN(NP) .LT. EOR) GO TO 5
NUMPT = NUMPT - 1
IF (PTNSVE .NE. EOR) GO TO 20
PRINT 21, LDIR1(I6), IEAST, LDIR2(I6)
21 FORMAT (8X, *FOR *, A3, * LINE NUMBER *, I4, *, EITHER THE FLAG EL
ELEVATION OR THE PRECEDING POINT ELEVATION IS MISPUNCHED.*/16X, *NO
2 TEST IS MADE TO CHECK LAST INPUT POINT *, A5, * COORDINATE.*/)
GO TO 22
20 IF (PTNSVE .EQ. FINISH) GO TO 22
PRINT 23, LDIR1(I6), IEAST
23 FORMAT (8X, *LAST POINT ON *, A3, * LINE NUMBER *, I4, * IS INCORR
LECT.*/)
22 IF (COORDZ(NP) .EQ. EOR) GO TO 24
ICARD = IN = 0
IEAST = IEAST + 1
FRSTPT = .TRUE.
NUMTOT = NUMTOT + NUMPT
GO TO 5
24 NUMTOT = NUMTOT + NUMPT
PRINT 25, IEAST, NUMTOT
25 FORMAT (/8X, *NUMBER OF BASIC GRID LINES = *, I4/8X, *NUMBER OF BA
SIC GRID POINTS = *, I6/)
CALL TYME (TLBL)
RETURN
END

```

```

SUBROUTINE TYME(TLBL)
COMMON /TIME/ TO

```

```

C
C--- TYME READS THE SYSTEMS CLOCK AND PRINTS OUT THE TIME SINCE THE
C--- FIRST CALL SECOND.
C
CALL SECOND (A)
T = A-TO
PRINT 1, TLBL, T
1 FORMAT (/105X, *TIME IN *, A6, * =*, F8.3/)
RETURN
END

```

## Example 2

```
PROGRAM MAIN (INPUT,OUTPUT,TAPE81,TAPE82,TAPE83,TAPE99)
DIMENSION SPECS(30)
COMMON BUFI (3518)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
SPECS(1) = 1.
SPECS(2) = 0.5
SPECS(3) = 51.
SPECS(4) = 1.
SPECS(5) = 29.5
SPECS(6) = 0.5
SPECS(7) = 60.
SPECS(8) = 29.
SPECS(11) = 1.
SPECS(12) = 99.
CALL PLOT30 (SPECS)
ISPECS(1) = 110
ISPECS(2) = 151
ISPECS(3) = 1
ISPECS(4) = 220
ISPECS(5) = 801
ISPECS(6) = 1
ISPECS(7) = 1
ISPECS(8) = 2
ISPECS(9) = 1
ISPECS(10) = 1
RSPECS(1) = 20.
RSPECS(2) = 30000.
RSPECS(3) = 31200.
RSPECS(4) = 4500.
RSPECS(5) = 6000.
RSPECS(6) = 1.732
RSPECS(7) = 6.
RSPECS(10) = 400.
RSPECS(11) = 55.
RSPECS(12) = 2.
RSPECS(13) = 20.
RSPECS(14) = 45.
RSPECS(15) = 1.
RSPECS(16) = 0.
RSPECS(21) = 0.
RSPECS(28) = .5
RSPECS(29) = .5
RSPECS(30) = 1.
REWIND 81
REWIND 82
REWIND 83
CALL I3DCVF (BJFI,3518,8,8H(16F5.0),55999.,6HTAPE81,6HNUPNCH)
REWIND 81
CALL I3DPTS (BJFI,3518,6HNUPNCH,6HNOHCLP)
REWIND 82
CALL I3DPTA (BJFI,3518)
BUFI(3205) = BJFI(3206) = 1.
BUFI(3209) = 30000.
BUFI(3210) = 33000.
BUFI(3211) = 31200.
```



```

BUFI(3212) = 33420.
BUFI(3213) = 35000.
CALL I3DIGL (BUFI,3518,SPECS)
CALL GDSEND (SPECS)
STOP
END

```

```

SUBROUTINE I3DIGL (BUFI,LENGTH,SPECS)
DIMENSION BUFI(1),SPECS(30)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
COMMON /TIME/TO
DATA TLBL /5HI3DIGL/
EQUIVALENCE (ISPECS(5),I5),(ISPECS(7),I7),(ISPECS(8),I8),(ISPECS(2
1),I2)

```

```

C
C--- I3DIGL MAPS A THREE-DIMENSIONAL SURFACE - A SINGLE-VALUED FUNCTION
C--- OF TWO VARIABLES - INTO ISOMETRIC, CAVALIER, DIMETRIC, OR CABINET
C--- PICTORIAL REPRESENTATION. ONE SET OF GRID LINES IS USED.
C

```

```

CALL SECOND (TO)
L1 = 4*I5 + 2*I7*I8 + I7 + I8 + 3 + MAX0(I7,I8) + 2*I2
IF (LENGTH .GE. L1) GO TO 1
PRINT 2
2 FORMAT (6X,*LENGTH AS SET BY USER IS TOO SMALL FOR SUBROUTINE I3DI
1GL.*)
STOP
1 N2 = 1 + I5
N3 = N2 + I5
N4 = N3 + I5
N5 = N4 + I5
N6 = N5 + I7*I8
N7 = N6 + I7*I8
N8 = N7 + I7 + 1
N9 = N8 + I8 + 1
N10 = N9 + 1 + MAX0(I7,I8)
N11 = N10 + I2
CALL EXCIGL (BUFI(1),BUFI(N2),BUFI(N3),BUFI(N4),BUFI(N5),BUFI(N6),
1BUFI(N7),BUFI(N8),BUFI(N9),BUFI(N10),BUFI(N11),LENGTH,SPECS)
CALL TYME (TLBL)
RETURN
END

```

```

SUBROUTINE EXCIGL (PLOTZ,XPLOT,YPLOT,YPLSVE,BLOCK,BLOCKH,CEC,CNC,
1CH,BOTEND,TOPEND,LENGTH,SPECS)
REAL PLOTZ(1),XPLOT(1),YPLOT(1),YPLSVE(1),BLOCK(1),BLOCKH(1),
1CEC(1),CNC(1),CH(1),BOTEND(1),TOPEND(1),NSTART,LABEL
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
EQUIVALENCE (ISPECS(6),II6),
1 (ISPECS(7),I7),(ISPECS(8),I8),(ISPECS(9),I9),(ISPECS(10),I10)
EQUIVALENCE (RSPECS(1),SL),(RSPECS(2),ESTART),(RSPECS(3),NSTART),
1 (RSPECS(4),VSTART),(RSPECS(5),VTOP),(RSPECS(7),PS),(RSPECS(10),
2SCALE),(RSPECS(11),APX),(RSPECS(12),APY),(RSPECS(13),GAMMA),
3 (RSPECS(14),PSIDIR),(RSPECS(15),FRAME),(RSPECS(16),TICKS),
4 (RSPECS(21),LABEL),(RSPECS(24),VDATAP),(RSPECS(25),XFRSVE),
5 (RSPECS(26),CNC111),(RSPECS(27),CEC111),(RSPECS(28),PLSEP),
6 (RSPECS(29),ILSEP),(RSPECS(30),ZFACTR)
DIMENSION CXCOR(4),CXCOR(4),SPECS(30),XFRAME(4),YFRAME(4)
LOGICAL EVEN,SOUTH,WEST,UU

```

```

C
C--- CONVERT PSIDIR, TRUE LINE-OF-SIGHT, TO DUMMY PSI, WHICH DEPENDS
C--- ALSO IN DIRECTION OF GRID LINES.
C

```

```

IF (II6 .EQ. 1) GO TO 3
PSI = PSIDIR - 90.
IF (PSI .GE. 0.) GO TO 4
PSI = 360. + PSI
GO TO 4
3 PSI = PSIDIR

```

```

C
C--- DETERMINE SOUTH AND WEST FOR USE IN IF STATEMENTS BELOW.
C

```

```

4 IF (PSI .GE. 90. .AND. PSI .LT. 270.) GO TO 66
SOUTH = .FALSE.
GO TO 67
66 SOUTH = .TRUE.
67 IF (PSI .GE. 180. .AND. PSI .LT. 360.) GO TO 68
WEST = .FALSE.
GO TO 69
68 WEST = .TRUE.

```

```

C
C--- CONVERT GAMMA AND PSI TO RADIAN MEASURE. CALCULATE ALPHA1 AND ALPHA2 AS
C--- FUNCTIONS OF PSI, GAMMA.
C

```

```

69 RGAMMA = GAMMA*.0174532925
IF (GAMMA .EQ. 0.) RGAMMA = .00001
RPSI = 0.
IF (PSI .EQ. 0.) RPSI = .00001
IF (PSI .EQ. 90.) RPSI = 1.57081
IF (PSI .EQ. 180.) RPSI = 3.14161
IF (PSI .EQ. 270.) RPSI = 4.71241
IF (RPSI .EQ. 0.) RPSI = PSI*.0174532925
ALPHA2 = ASIN((SIN(RPSI)**2 + TAN(RGAMMA)**2 - COS(RPSI)**2)/(2.*S
1IN(RPSI)*TAN(RGAMMA)))
ALPHA1 = ASIN((TAN(RGAMMA) - SIN(RPSI)*SIN(ALPHA2))/COS(RPSI))

```

```

C
C--- SET CONSTANTS FOR USE IN RESETTING #BLOCK#.
C

```

```

IBB2 = I7*I8 - I7
IBB3 = I7*I8 + 1
IBB4 = I7 + 1
IBBJ = 2*I7

```

C  
C--- SET VARIABLES FOR RESETTING #BLOCK# ACCORDING TO QUADRANT OF PSI.  
C

```
IF (PSI .GE. 90. .AND. PSI .LT. 180.) GO TO 170
IF (PSI .GE. 180. .AND. PSI .LT. 270.) GO TO 171
IF (PSI .GE. 270. .AND. PSI .LT. 360.) GO TO 172
IF (II6 .EQ. 2) 8,7
172 ALPHA1 = 3.14159265 - ALPHA1
   ALPHA2 = 3.14159265 + ALPHA2
   IF (II6 .EQ. 2) GO TO 7
   8 IB = IBB4
     IB1 = -1
     IBJMP = IBBJ
     GO TO 173
   7 IB = 0
     IB1 = 1
     IBJMP = 0
     GO TO 173
171 ALPHA1 = -ALPHA1
   ALPHA2 = -ALPHA2
   IF (II6 .EQ. 2) 6,5
170 ALPHA1 = 3.14159265 + ALPHA1
   ALPHA2 = 3.14159265 - ALPHA2
   IF (II6 .EQ. 2) GO TO 5
   6 IB = IBB2
     IB1 = 1
     IBJMP = -IBBJ
     GO TO 173
   5 IB = IBB3
     IB1 = -1
     IBJMP = 0
```

C  
C--- REORDER CEC, CNC AS NECESSARY.  
C

```
173 IB1 = IB + 1
   IF (SOUTH) GO TO 143
   IF (PSI .GE. 270. .AND. PSI .LT. 360.) GO TO 144
   GO TO 145
143 DO 149 I=1,IB1
   IH = IB1 - I + 1
149 CH(IH) = CNC(I)
   DO 150 I=1,IB1
150 CNC(I) = CH(I)
   IF (PSI .GE. 180. .AND. PSI .LT. 270.) GO TO 144
   GO TO 145
144 DO 154 I=1,IBB4
   IH = IBB4 - I + 1
154 CH(IH) = CEC(I)
   DO 155 I=1,IBB4
155 CEC(I) = CH(I)
```

C  
C--- DEFINE SIN AND COS VARIABLES FOR USE LATER.  
C

```
145 SALPH2 = SIN(ALPHA2)
   SALPH1 = SIN(ALPHA1)
   CALPH2 = COS(ALPHA2)
   CALPH1 = COS(ALPHA1)
```

C  
C--- REORDER BLOCK AND PLACE INTO BLOCKH USING VARIABLES SET PRIOR.

```

C--- BLOCKH(1) WILL REFER TO THE DIAGRAM AT THE APEX, ETC.
C
  IDE = 0
  I78 = I7*I8
  DO 9 I=1,I78
  IB = IB + I81
  IDE = IDE + 1
  IF (IDE .LE. 17) GO TO 10
  IDE = 0
  IB = IB + I8JMP
10 BLOCKH(I) = BLJCK(I8)
  9 CONTINUE
C
C--- INITIALIZE SYSTEM AND CALCULATE EQUATION CONSTANTS TO BE USED IN
C--- MAIN DO LOOPS BELOW.
C
  I91 = I9 + 1
  I9M1 = I9 - 1
  EVEN = .FALSE.
  I10M = I10 - 1
  I10I = 1-I10
  CNC111 = CNC(1)
  CEC111 = CEC(1)
  C = (VTOP-VSTART)*ZFACTR/SCALE
  HEW = C/(CALPH2*TAN(ALPHA1) + SALPH2) + TLSEP
  HNS = C/(CALPH1*TAN(ALPHA2) + SALPH1) + PLSEP
  XHEW = CALPH2*HEW
  YHEW = SALPH2*HEW
  XHNS = CALPH1*HNS
  YHNS = SALPH1*HNS
  XPART = CALPH1*PS/SCALE
  YPART = SALPH1*PS/SCALE
  XLINEP = SL*CALPH2/SCALE
  YLINEP = SL*SALPH2/SCALE
  XFRSVE = 1000.
  IB = 0
  IBCNT = 0
C
C--- MAIN DO LOOPS TO PROCESS ONE BLOCK DIAGRAM AT A TIME.
C
  DO 11 NI = 1,I8
  DO 12 NN1 = 1,I7
  REWIND 83
  IB = IB + 1
  IF (BLOCKH(IB) .NE. 1.) GO TO 12
  IBCNT = IBCNT + 1
C
C--- CALCULATE CNCOR AND CECOR ARRAYS FROM CURRENT CNC, CEC VALUES.
C
  CNCOR(1) = CNCOR(4) = CNC(NI)
  NI1 = NI + 1
  CNCOR(2) = CNCOR(3) = CNC(NI1)
  CECOR(1) = CECOR(2) = CEC(NN1)
  NN2 = NN1 + 1
  CECOR(3) = CECOR(4) = CEC(NN2)
C
C--- DETERMINE NUMBERS OF FIRST PRIOR AND LAST NEEDED GRID LINES,
C--- INDEPENDENT OF LINES TO BE SKIPPED.
C
  IF (I16 .EQ. 1) GO TO 13

```

```

      IN = IFIX((ESTART-CECOR(1))/SL)
      ILAST = IFIX((ESTART-CECOR(4))/SL) + 1
      GO TO 14
13   IN = IFIX((CECOR(1)-ESTART)/SL)
      ILAST = IFIX((CECOR(4)-ESTART)/SL) + 1
C
C--- DETERMINE FIRST (NEAREST TO VIEWER) AND LAST NEEDED GRID LINE ARRAY
C--- SUBSCRIPTS, INDEPENDENT OF POINTS TO BE SKIPPED.
C
14   IBOT = IFIX((CNCOR(1)-NSTART)/PS) + 1
      ITOP = IFIX((CNCOR(2)-NSTART)/PS) + 1
      IBUTTP = IBOT + ITOP
C
C--- CALCULATE SMALLEST AND LARGEST ARRAY SUBSCRIPTS, IMIN AND IMAX.
C
      IF (SOUTH) GO TO 158
      IMIN = IBOT
      IMAX = ITOP
      GO TO 159
158  IMIN = ITOP
      IMAX = IBOT
C
C--- SKIP FORWARD THROUGH FIRST #IN# GRID LINE ARRAYS TO GET TO FIRST
C--- NEEDED ONE, CORRESPONDING TO DIAGRAM NEAR EDGE.
C
159  IF (IN .EQ. 0) GO TO 44
      DO 112 I=1,IN
112  READ (83)
C
C--- CALCULATE AND INITIALIZE VARIABLES FOR USE IN HIDDEN LINE TEST.
C--- INITIALIZE VARIABLES TO CORRECT VIEW-LINE DRIFT FACTOR.
C
44   SLI9 = SL*19
      PS110 = PS*110
      U = SLI9*CALPH2/CALPH1
      UDEL = U/PS110 - FLJAT(INT(U/PS110))
      IF (UDEL .LE. 0.5) GO TO 45
      ISHIFT = 110*(INT(U/PS110) + 1)
      ICNE = -110
      UD = 1.0 - UDEL
      GO TO 46
45   ISHIFT = 110*INT(U/PS110)
      ICNE = 110
      UD = UDEL
46   UTEST = 0.5
      UCUM = 0.
      UU = .FALSE.
C
C--- CALCULATE VARIABLES WHICH VARY ONLY BETWEEN BLOCKS.
C
      NM = NN1 - 1
      XAPEX = APX + NM*XHEW + ABS(CEC(NN1) - CEC(1))*CALPH2 /SCALE - (NI
1 - 1)*XHNS - ABS(CNC(NI) - CNC(1))*CALPH1 /SCALE
      YAPEX = APY + NM*YHEW + ABS(CEC(NN1) - CEC(1))*SALPH2 /SCALE + (NI
1 - 1)*YHNS + ABS(CNC(NI) - CNC(1))*SALPH1 /SCALE
C
C--- SET DC LOOP RANGE.
C
      IF (WEST) GO TO 150
      IN1 = IN + 1

```

```

GO TO 157
156 IN1 = ILAST
    ILAST = IN + 1
C
C--- OUTER DO LOOP - PROCESS ALL GRID LINES, ONE AT A TIME.
C
157 DO 47 II=IN1,ILAST,I9
    READ (83) (PLOTZ(I),I=1,IMAX)
    IF (WEST) GO TO 160
    IF (I9 .EQ. 1) GO TO 162
    DO 17 I=1,I9M1
17 READ (83)
    GO TO 162
160 DO 16 I=1,I91
16 BACKSPACE 83
162 NCOUNT = I101
C
C--- TEST FOR SERIOUS VIEW-LINE DRIFT, AND CORRECT IF NECESSARY.
C
    IF (UCUM .GT. UTEST) GO TO 70
    IF (.NOT. UU) GO TO 71
    ISHIFT = ISHIFT - IJNE
    UU = .FALSE.
    GO TO 71
70 UTEST = UTEST + 1.0
    UU = .TRUE.
    ISHIFT = ISHIFT + IJNE
71 UCUM = UCUM + JU
C
C--- CALCULATE VARIABLES AND SET LINE PLOT DIRECTION (FORWARD OR REVERSE).
C
    X2X = XAPEX + (II-IN1)*XLINEX
    Y2Y = YAPEX + (II-IN1)*YLINEX
    IF (.NOT. EVEN) GO TO 137
    EVEN = .FALSE.
    SPECS(14) = SPECS(15) = -FLOAT(I10)
    GO TO 138
137 EVEN = .TRUE.
    SPECS(14) = SPECS(15) = FLOAT(I10)
138 IF (II .EQ. IN1 .OR. ISHIFT .EQ. 0) GO TO 64
    YPLOT(IMIN) = Y2Y + (PLOTZ(IBOT) - VSTART)*ZFACTR/SCALE
    YYI = (YPLOT(IMIN) - YPLSVE(IBOT))/ISHIFT
C
C--- INNER DO LOOP - PROCESS ALL POINTS ON A GRID LINE, ONE POINT AT A TIME.
C--- TEST FOR HIDDEN POINTS AND CONSTRUCT THE CURRENT VISIBILITY (HORIZON)
C--- LINE. DRAW VISIBLE LINE SEGMENTS AS NEEDED.
C
64 DO 48 INDEX=IMIN,IMAX,I10
    IF (EVEN) III = INDEX
    IF (.NOT. EVEN) III = IBOTTP - INDEX
    IF (SCUTH) GO TO 176
    IREV = III
    ISH = IREV - ISHIFT
    GO TO 177
176 IREV = IBOTTP - III
    ISH = IREV + ISHIFT
177 XPLOT(III) = X2X - XPART*(III-IMIN)
    YPLOT(III) = Y2Y + YPART*(III-IMIN) + (PLOTZ(IREV) - VSTART)*ZFACT
1R/SCALE
    IF (II .EQ. IN1) GO TO 50

```

```

IF ((III-IMIN) .GE. ISHIFT) GO TO 49
IF (YPLOT(III) .GE. (YPLOT(IMIN) - YPI*(III-IMIN))) GO TO 50
PLOTZ(IREV) = YPLOT(IMIN) - YPI*(III-IMIN)
GO TO 113
50 PLOTZ(IREV) = YPLOT(III)
NCGOUNT = NCGOUNT + 110
GO TO 48
49 IF (YPLOT(III) .GT. YPLSVE(ISH)) GO TO 50
PLOTZ(IREV) = YPLSVE(ISH)
113 IF (NCGOUNT .EQ. 1101) GO TO 48
SPECS(13) = FLOAT((NCGOUNT + 110M)/110)
IF (EVEN) 15 = 111 - NCGOUNT - 110M
IF (.NOT. EVEN) 15 = III + NCGOUNT + 110M
CALL SLLILI (XPLOT(15), YPLOT(15), SPECS)
NCGOUNT = 1101
48 CONTINUE
C
C--- DRAW LAST LINE SEGMENT IF NEEDED, AND LOAD NEW VISIBILITY LINE INTO
C--- YPLSVE.
C
IF (NCGOUNT .EQ. 1101) GO TO 52
SPECS(13) = FLOAT((NCGOUNT + 110M)/110)
IF (EVEN) 15 = IMAX-NCGOUNT+1
IF (.NOT. EVEN) 15 = IMIN+NCGOUNT-1
CALL SLLILI (XPLOT(15), YPLOT(15), SPECS)
52 DO 54 I=IMIN, IMAX, 110
54 YPLSVE(I) = PLOTZ(I)
I6 = II - IN1 + 1
C
C--- SAVE END-LINE POINTS
C
BOTEND(I6) = PLOTZ(I6BOT)
TOPEND(I6) = PLOTZ(I6TOP)
47 CONTINUE
C
C--- ALL VISIBLE GRID LINE SEGMENTS HAVE BEEN DRAWN FOR A SINGLE BLOCK.
C--- NOW DRAW THE FAR-EDGE END LINE.
C
SPECS(14) = SPECS(15) = FLOAT(I9)
I5 = ILAST - IN1 + 1
X3X = XAPEX - XPART*(IMAX-IMIN)
DO 55 I=1, I5, I9
55 PLOTZ(I) = X3X + (I-1)*XLINEP
SPECS(13) = FLOAT((I5 + I9M1)/I9)
CALL SLLILI (PLOTZ, TOPEND, SPECS)
IF (IBCNT .EQ. 1) VDATAP = VSTART + (BOTEND(1)-YAPEX)*SCALE/ZFACTR
IF (PLOTZ(1) .LT. XFRSVE) XFRSVE = PLOTZ(1)
C
C--- DRAW GRID-LINE SIDE FRAME, IF WANTED.
C
IF (FRAME .NE. 1.) GO TO 118
XFRAME(1) = XFRAME(2) = PLOTZ(1)
XFRAME(3) = XFRAME(4) = XAPEX
YFRAME(1) = TOPEND(1)
YFRAME(2) = YAPEX + YPART*(IMAX-IMIN)
YFRAME(3) = YAPEX
YFRAME(4) = BOTEND(1)
SPECS(13) = 4.
SPECS(14) = SPECS(15) = 1.
CALL SLLILI(XFRAME, YFRAME, SPECS)

```

```

C
C--- DRAW TICKS IF NEEDED.
C
  IF (TICKS .NE. 1.) GO TO 118
  SPECS(13) = 2.
  CALL I3DTC1 (YFRAME(1),YFRAME(2),PLOTZ(1),CALPH1,0,-SALPH1,0,SPECS
1)
  CALL I3DTC2 (CNCOR(2),CNCOR(1),SOUTH,XFRAME(2),YFRAME(2),CALPH1,SAL
1LPH1,1,SPECS)
  SPECS(13) = 3.
  CALL I3DTC1 (YFRAME(4),YFRAME(3),XAPEX,CALPH2,CALPH1,SALPH2,
1SALPH1,SPECS)
C
C--- DRAW NEAR-EDGE END LINE.
C
118 DO 56 I=1,15,19
56 PLOTZ(I) = XAPEX + (I-1)*XLINER
  SPECS(13) = FLJAT((15 + I9M1)/I9)
  SPECS(14) = SPECS(15) = FLOAT(I9)
  CALL SLLILI (PLOTZ,BUTEND,SPECS)
  IF (PLOTZ(I5) .LT. XFRSVE) XFRSVE = PLOTZ(I5)
C
C--- DRAW TRANSVERSE-LINE SIDE FRAME, IF WANTED.
C
  IF (FRAME .NE. 1.) GO TO 12
  XFRAME(1) = XFRAME(2) = PLOTZ(I5)
  YFRAME(1) = BUTEND(I5)
  YFRAME(2) = YAPEX + YLINER*(ILAST-IN1)
  SPECS(13) = 3.
  SPECS(14) = SPECS(15) = 1.
  CALL SLLILI(XFRAME,YFRAME,SPECS)
C
C--- DRAW TICKS IF NEEDED.
C
  IF (TICKS .NE. 1.) GO TO 12
  SPECS(13) = 2.
  CALL I3DTC2 (CECOR(1),CECOR(4),WEST,XAPEX,YAPEX, CALPH2,-SALPH2,2,
1SPECS)
  CALL I3DTC1 (YFRAME(1),YFRAME(2),PLOTZ(I5),-CALPH2,0,-SALPH2,0,SPE
1CS)
12 CONTINUE
11 CONTINUE
C
C--- ALL BLOCKS ARE COMPLETED. PRINT STANDARD LEGEND IF WANTED.
C
  IF (LABEL .NE. 1.) GO TO 15
  CALL I3DLBL (SPECS)
15 RETURN
  END

```



```

SUBROUTINE I3DTC1 (YFA,YFB,XTC,CA,CB,SA,SB,SPECS)
DIMENSION SPECS (30),XTIC(3),YTIC(3)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
EQUIVALENCE (RSPECS(4),VSTART),(RSPECS(17),MAJI),(RSPECS(18),MINI)
1,(RSPECS(19),MAJL),(RSPECS(20),MINL),(RSPECS(10),SCALE),(RSPECS(30)
2),ZFACTR)
REAL MINI,MAJI,MINL,MAJL

```

C  
C--- I3DTC1 DRAWS TWO OR THREE POINT TICKS ON VERTICAL FRAME LINES.  
C

```

IS = IFIX(SPECS(13))
IS1 = IS - 1
IZTICS = INT((VSTART + (YFA-YFB)*SCALE/ZFACTR)/MINI) - INT(VSTART/
1MINI)
IF (IZTICS .EQ. 0) GO TO 1
TICDIF = (VSTART/MINI - FLOAT(INT(VSTART/MINI)))*MINI*ZFACTR/SCALE
TICREF = FLOAT(INT(VSTART/MINI))*MINI
XTIC(IS1) = XTC
YT = YFB - TICDIF
SM = MINI*ZFACTR/SCALE
DO 4 I=1,IZTICS
YTIC(IS1) = YT + I*SM
IF (FLOAT(INT((TICREF+MINI*I)/MAJI)) .EQ. (TICREF+MINI*I)/MAJI)
1 GO TO 2
TICVAR = MINL
GO TO 3
2 TICVAR = MAJL
3 XTIC(IS) = XTIC(IS1) + TICVAR*CA
YTIC(IS) = YTIC(IS1) + TICVAR*SA
IF (IS .EQ. 2) GO TO 4
XTIC(1) = XTIC(2)-TICVAR*CB
YTIC(1) = YTIC(2) + TICVAR*SB
4 CALL SLLILI (XTIC,YTIC,SPECS)
1 RETURN
END

```

```

SUBROUTINE I3DTC2 (CORA,CORB,QUADRT,PTA,PTB,C,S,NCALL,SPECS)
DIMENSION SPECS (30),XTIC(2),YTIC(2)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
EQUIVALENCE (RSPECS(10),SCALE),(RSPECS(17),MAJI),(RSPECS(18),MINI)
1,(RSPECS(19),MAJL),(RSPECS(20),MINL),(ISPECS(6),I6)
LOGICAL QUADRT
REAL MINI,MAJI,MINL,MAJL

```

C  
C--- I3DTC2 DRAWS TWO POINT TICKS ON HORIZONTAL FRAME LINES.  
C

```

TICSN = ABS(FLOAT(INT(CORA/MINI))-FLOAT(INT(CORB/MINI)))
IF (TICSN .EQ. 0.) GO TO 1
IF (NCALL .EQ. 1) GO TO 2
IF (I6 .EQ. 1) GO TO 3
IF (QUADRT) 4,3
2 IF (.NOT. QUADRT) 5,4
3 IF (QUADRT) 5,4

```

```

4 TICDIF = (CORA/MINI - FLOAT(INT(CORA/MINI)))*MINI/SCALE
  TICREF = FLOAT(INT(CORA/MINI))*MINI
  SGNTIC = -1.
  GO TO 6
5 TICDIF = (1. - CORA/MINI + FLOAT(INT(CORA/MINI)))*MINI/SCALE
  TICREF = (FLOAT(INT(CORA/MINI)) + 1.)*MINI
  SGNTIC = 1.
6 ITICSN = IFIX(TICSN)
  SM = SGNTIC*MINI
  PTAT = PTA - TICDIF*C
  PTBT = PTB + TICDIF*S
  CMS = C*MINI/SCALE
  SMS = S*MINI/SCALE
  DO 7 I=1,ITICSN
  XTIC(1) = PTAT + I*CMS
  XTIC(2) = XTIC(1)
  YTIC(1) = PTBT - I*SMS
  IF (FLOAT(INT((TICREF-SM*I)/MAJI)) .EQ. (TICREF-SM*I)/MAJI) GOTO 8
  TICVAR = MINL
  GO TO 9
8 TICVAR = MAJL
9 YTIC(2) = YTIC(1) + TICVAR
7 CALL SLLILI (XTIC,YTIC,SPECS)
1 RETURN
  END

```

```

SUBROUTINE I3DLBL (SPECS)
  DIMENSION SPECS(30)
  COMMON /WSPECS/ RSPECS(30),ISPECS(10)
  EQUIVALENCE (RSPECS(22),HITE),(RSPECS(23),XPOSL),(RSPECS(14),PSI),
1 (RSPECS(13),GAMMA),(RSPECS(25),XFRSVE),(RSPECS(7),PS),(RSPECS(10),
2SCALE),(ISPECS(10),I10),(RSPECS(30),ZFACTR)

```

C  
C--- I3DLBL LABELS THE DIAGRAM, GIVING DIRECTION OF SIGHT, INCLINATION  
C--- (APPARENT ANGLE, TO THE HORIZONTAL, OF VIEW), AND POINT RESOLUTION.  
C--- OTHER LETTERING IS LEFT TO THE USER.  
C

```

  SPECS(17) = .2
  SPECS(18) = .2
  SPECS(19) = 0.
  SPECS(20) = 0.
  SPECS(21) = 1.
  IF (XPOSL .EQ. -1.) GO TO 1
  SPECS(22) = XPOSL
  GO TO 2
1 IF (XFRSVE .GE. 10.) SPECS(22) = XFRSVE - 9.0
  IF (XFRSVE .LT. 10.) SPECS(22) = 1.0
2 SPECS(23) = HITE
  CALL TITLEG (18HDIRECTION OF SIGHT,SPECS)
  SPECS(22) = SPECS(22) + 4.2
  IF (PSI .GE. 0. .AND. PSI .LT. 90.) GO TO 166
  IF (PSI .GE. 90. .AND. PSI .LT. 180.) GO TO 167
  IF (PSI .GE. 180. .AND. PSI .LT. 270.) GO TO 168
  CALL TITLEG (6HN W,SPECS)
  PSILBL = 360. - PSI
  GO TO 169

```

```

166 CALL TITLEG (6HN      E,SPECS)
   PSILBL = PSI
   GO TO 169
167 CALL TITLEG (6HS      E,SPECS)
   PSILBL = 180. - PSI
   GO TO 169
168 CALL TITLEG (6HS      W,SPECS)
   PSILBL = PSI - 180.
169 SPECS(28) = 1.
   SPECS(22) = SPECS(22) + .2
   CALL DECVAL (PSILBL,SPECS)
   SPECS(23) = SPECS(23) - .3
   SPECS(22) = SPECS(22) - 4.4
   CALL TITLEG (25HINCLINATION          DEGREES,SPECS)
   SPECS(22) = SPECS(22) + 2.6
   CALL DECVAL (GAMMA,SPECS)
   SPECS(22) = SPECS(22) - 2.6
   SPECS(23) = SPECS(23) - 2.4
   CALL TITLEG (24HVERTICAL EXAGGERATION = ,SPECS)
   SPECS(28) = 2.
   SPECS(22) = SPECS(22) + 4.8
   CALL DECVAL (ZFACTOR,SPECS)
   SPECS(22) = SPECS(22) - 4.8
   SPECS(23) = SPECS(23) - .3
   SPECS(17) = SPECS(18) = .1
   RISP = SCALE/(PS*I10)
   SPECS(28) = 0.
   CALL TITLEG (28HRESOLUTION =          POINTS/INCH,SPECS)
   SPECS(22) = SPECS(22) + 1.3
   CALL DECVAL (RISP,SPECS)
   SPECS(22) = SPECS(22) - 1.3
   SPECS(23) = 2.0
   CALL TITLEG (24HPROGRAM BY W.B. WRAY JR.,SPECS)
   RETURN
   END

```

```

SUBROUTINE I3DCVT (BUFI, LNGTHB, NUMPTC, FMT, EOR, DVCEOT, PNCH)
DIMENSION BUFI(1), FMT(3)
COMMON /WSPECS/ RSPECS(30), ISPECS(10)
COMMON /TIME/ TU
EQUIVALENCE (ISPECS(1), I1), (ISPECS(2), I2)
DATA TLBL /6HI3DCVT/

```

```

C
C--- I3DCVT READS A HOLLERITH CARD DECK, POSSIBLY WITH EMBEDDED BLANKS,
C--- AND REDUCES THE DATA TO A SET OF BINARY LOGICAL RECORDS ON TAPE81,
C--- TAPE82, OR TAPE83 AS SPECIFIED BY USER. OUTPUT IS ON TAPE, DISK,
C--- OR PUNCHED AS BINARY CARDS IF USER EQUIVALENCES PUNCHB. THE
C--- ARRAY NUMPT IS FILLED, AND WILL BE PUNCHED AS THE LAST LOGICAL RECORD
C--- IF 6HPNCHOT IS USED IN THE CALLING ARGUMENT LIST.
C

```

```

CALL SECOND (TU)
L1 = 4*I1 + I2
IF (LNGTHB .GE. L1) GO TO 1
PRINT 2

```

```

2 FORMAT (6X,*LNGBHB AS SET BY USER IS TOO SMALL FOR SUBROUTINE I3DC
1VT*//)
STOP
1 N2 = 1 + I1
N3 = N2 + 3*I1
CALL EXCCVT (BUFI(1),BUFI(N2),BUFI(N3),LNGBHB,NUMPTC,FMT,EOR,DVCEO
1T,PNCH)
CALL TYME (TLBL)
RETURN
END

```

```

SUBROUTINE EXCCVT (GRIDN,GRIDEL,NUMPT,LNGBHB,NUMPTC,FMT,EOR,DVCEOT
1,PNCH)
REAL GRIDN(1),GRIDEL(1),NUMPT(1),FMT(3),COORDN(40),COORDZ(40)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
DATA D1,D2,D3 /6HTAPE81,6HTAPE82,6HPNCFOT /
EQUIVALENCE (ISPECS(2),I2), (ISPECS(3),I3)

```

```

C
C--- PREPARE FOR SELECTION OF OUTPUT TAPE UNIT.
C
IF (DVCEOT .EQ. D1) GO TO 3
IF (DVCEOT .EQ. D2) GO TO 4
IDVCE = 83
GO TO 5
4 IDVCE = 82
GO TO 5
3 IDVCE = 81
C
C--- INITIALIZE COUNTERS AND LIMITS FOR DATA INPUT.
C
5 IE = 0
IEAST = 1
I31 = I3 + 1
L1 = NUMPTC
L2 = L1 - 1
C
C--- BEGIN DATA INPUT AND REDUCTION CYCLE. TESTS FOR END-OR RECORD
C--- FLAGS AND EMBEDDED BLANKS.
C
6 ICOUNT = 0
7 READ FMT, (COORDN(I),COORDZ(I),I=1,L1)
IF (COORDN(L1) .NE. EOR) GO TO 9
IF (L2 .EQ. 0) GO TO 11
DO 8 I=1,L2
IF (COORDN(I) .EQ. 0.) GO TO 8
ICOUNT = ICOUNT + 1
GRIDN(ICOUNT) = COORDN(I)
GRIDEL(ICOUNT) = COORDZ(I)
8 CONTINUE
GO TO 11
9 DO 10 I=1,L1
IF (COORDN(I) .EQ. 0.) GO TO 10
ICOUNT = ICOUNT + 1
GRIDN(ICOUNT) = COORDN(I)
GRIDEL(ICOUNT) = COORDZ(I)
10 CONTINUE
GO TO 7

```

```

C
C--- AT THIS POINT ONE LOGICAL RECORD HAS BEEN REDUCED. NOW INCREMENT
C--- RECORD COUNTERS AND PLACE ARRAYS CNTC CORRECT TAPE.
C
11 IE = IE + 1
WRITE (IDVCE) (GRIDN(I),GRIDEL(I),I=1,ICOUNT)
NUMPT(IEAST) = FLOAT(ICOUNT)
IEAST = IEAST + I31
C
C--- TEST FOR LAST COORDINATE ARRAY LOGICAL RECORD.
C
IF (COORDZ(L1) .NE. EOR) GO TO 6
C
C--- TEST TO MAKE CERTAIN ENOUGH SPACE IS RESERVED FOR NUMPT ARRAY.
C
IEAST = IEAST - I31
IF (IEAST .EQ. I2) GO TO 22
PRINT 21
21 FORMAT (/10X,*ISPECS(2) INCORRECTLY SPECIFIED BY USER. PROGRAM TE
1RMINATED.*/)
STOP
22 PRINT 16,I4
16 FORMAT (1H1,20X,*SUBROUTINE I3DCVT*/10X,*NUMBER OF COORDINATE ARKA
1Y LOGICAL RECORDS PROCESSED = *,I4//)
C
C--- DETERMINE IF NUMPT ARRAY IS TO BE PUNCHED AS LAST LOGICAL RECORD.
C
IF (PNCH .NE.03) GO TO 20
WRITE (IDVCE) (NUMPT(I),I=1,I2)
20 RETURN
END

SUBROUTINE I3DPTA (BUFI,LENGTHB)
DIMENSION BUFI(1)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
COMMON /TIME/ TU
EQUIVALENCE (ISPECS(4),I4),(ISPECS(2),I2),(ISPECS(5),I5)
DATA TLBL /5HI3DPTA/
C
C--- SUBROUTINE I3DPTA GENERATES A FULL SET OF ARRAY POINTS SPACED ACCORDING
C--- TO PS FROM A SKELETON ARRAY INPUT ON TAPE/DISK OR CARDS.
C
CALL SECOND (TU)
L1 = 2*I4 + I5 + I2
IF (LENGTHB .GE. L1) GO TO 1
PRINT 2
2 FORMAT (6X,*LENGTHB AS SET BY USER IS TOO SMALL FOR SUBROUTINE I3DP
1TA.*/)
STOP
1 N2 = 1 + I4
N3 = N2 + I4
N4 = N3 + I2
CALL EXCPTA (BUFI(1),BUFI(N2),BUFI(N3),BUFI(N4),LENGTHB)
CALL TYME (TLBL)
RETURN
END

```

```

SUBROUTINE EXCPTA (GRIDN,GRIDEL,NUMPT,FLOTZ,LENGTHB)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
EQUIVALENCE (RSPECS(7),PS), (ISPECS(2),I2), (ISPECS(5),I5)
REAL GRIDN(1),GRIDEL(1),PLOTZ(1),NUMPT(1)
C
C--- DC LOOP TO FILL OUT ALL I2 GRID LINES.
C
1 DO 3 II=1,I2
  ICGOUNT = IFIX(NUMPT(II))
  READ (82) (GRIDN(I),GRIDEL(I),I=1,ICGOUNT)
C
C--- INITIALIZE VARIABLES TO HANDLE INITIAL POINTS ON GRID LINES, BEFORE
C--- BRANCH TO 300.
C
  FLOTN = GRIDN(1) - PS
  L1 = 2
  GELN = (GRIDEL(2)-GRIDEL(1))/(GRIDN(2)-GRIDN(1))
  GEL = GRIDEL(1)
  GN = GRIDN(1)
  DO 29 I=1,I5
  PLOTN = PLOTN + PS
  IF (PLOTN .LE. GRIDN(L1)) GO TO 30
C
C--- RESET L AND L1 SO THAT NEXT CORRECT PAIR OF SKELETON GRID POINTS IS
C--- USED TO CALCULATE PLOTZ POINTS.
C
300 L1 = L1 + 1
  IF (PLOTN .GT. GRIDN(L1)) GO TO 300
  L = L1 - 1
  GELN = (GRIDEL(L1)-GRIDEL(L))/(GRIDN(L1)-GRIDN(L))
  GEL = GRIDEL(L)
  GN = GRIDN(L)
30 PLOTZ(I) = (PLOTN-GN)*GELN + GEL
29 CONTINUE
3 WRITE (83) (PLOTZ(I),I=1,I5)
  RETURN
  END

```

```

SUBROUTINE I3DPTS (BUFI,LENGTHB,PNCH,FMT,NUMPTC)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
COMMON /TIME/ TU
DIMENSION BUFI(1),FMT(3)
EQUIVALENCE (ISPECS(1),I1),(ISPECS(2),I2),(ISPECS(3),I3),(ISPECS(4),I4)
DATA TLBL /6H13DPTS/
C
C--- SUBROUTINE I3DPTS CALCULATES INTERMEDIATE LINES IN ANY NUMBER FROM
C--- A BASIC ARRAY OF POINTS IN LINES. THE BASIC ARRAY INPUT IS FROM
C--- TAPE81, EITHER MAGNETIC TAPE, DISK, OR BINARY CARDS IF EQUIVALENCED TO
C--- INPUT. OUTPUT IS EITHER IN BINARY OR HOLLERITH MODE. IF TAPE82
C--- IS EQUIVALENCED TO PUNCHB, A BINARY DECK IS PUNCHED AND THE ARRAY
C--- NUMPT IS PUNCHED AS THE LAST LOGICAL RECORD. IF A HOLLERITH FORMAT IS
C--- SPECIFIED IN THE CALL LIST, HOLLERITH DATA CARDS ARE PUNCHED. PUNCH
C--- MUST BE DECLARED. IF BOTH 6HPNCHOT AND A HOLLERITH FORMAT ARE
C--- DECLARED, THEN BOTH HOLLERITH DATA CARDS AND BINARY NUMPT ARRAY
C--- ARE PUNCHED.

```

```

C
CALL SECOND (T0)
L1 = 4*I1 + I2 + 2*I3*I4
IF (LNGTHB .GE. L1) GO TO 1
PRINT 2
2 FCRMAT (6X,*LNGTHB AS SET BY USER IS TOO SMALL FOR SUBROUTINE I3DP
ITS.*/)
STOP
1 N2 = 1 + I1
N3 = N2 + I1
N4 = N3 + I1
N5 = N4 + I1
N6 = N5 + I2
N7 = N6 + I3*I4
CALL EXCPTS (BUFI(1),BUFI(N2),BUFI(N3),BUFI(N4),BUFI(N5),BUFI(N6),
1BUFI(N7),LNGTHB,I3,I4,PNCH,FMT,NUMPTC)
CALL TYME (TBL)
RETURN
END

```

```

SUBROUTINE EXCPTS (GRIDN,GRIDEL,GRIDN1,GRIDL1,NUMPT,XGRIDN,XGRIDZ,
1LNGTHB,I3,I4,PNCH,FMT,NUMPTC)
REAL GRIDN(1),GRIDEL(1),GRIDN1(1),GRIDL1(1),NUMPT(1),XGRIDN(I3,I4)
1,XGRIDZ(I3,I4)
INTEGER PTPLT
DIMENSION FMT(3)
COMMON /WSPECS/ RSPECS(30),ISPECS(10)
COMMON /I3DPS/ INTCT,F13

```

```

EQUIVALENCE (RSPECS(1),SPACE1), (RSPECS(6),DELFAC), (ISPECS(1),
1I1), (ISPECS(2),I2)
DATA D1 /OHPNCHUT/
DATA D2 /OHVHULP/
I32 = I3 + 2
I31 = I3 + 1
ICOUNT = IFIX(NUMPT(1))
READ (81) (GRIDN(I),GRIDEL(I),I=1,ICOUNT)
NUM = 0
F13 = 1./(I3 + 1)
DELTAD = DELFAC*SPACE1*(I3+1)

```

```

C
C--- BEGIN MAIN DO LOOP TO CALCULATE COORDINATES FOR SKELETON POINTS ON
C--- ALL INTERMEDIATE GRID LINES. EACH PASS THROUGH THE LOOP CONSIDERS
C--- ONE PAIR OF BASIC GRID LINES AND THE INTERMEDIATE GRID LINES
C--- BETWEEN.

```

```

C
DO 9 II=I32,I2,I31
ICNT1 = IFIX(NUMPT(II))
READ (81) (GRIDN1(I),GRIDL1(I),I=1,ICNT1)

```

```

C
C--- INITIALIZE VALUES FOR ARRAY SUBSCRIPTS.

```

```

C
J = 1
JL = ICOUNT
K1 = 1
K2 = 2

```

```

      KL = ICNT1
      INTCT = 0
      PTPLT = 0
C
C--- BEGIN TESTS OF POINTS ON THE TWO BASIC LINES. RELATIVE ELEVATIONS
C--- AND DISTANCES APART DETERMINE WHICH POINT PAIRS ARE USED IN THE
C--- CALCULATION OF INTERMEDIATE LINE SKELETON POINTS.
C
      13 IF (GRIDEL(J) .NE. GRIDL1(K1) .OR. GRIDEL(J) .NE. GRIDL1(K2))
          GO TO 10
      16 IF (ABS(GRIDN(J) - GRIDN1(K1)) .GT. DELTAD .AND. ABS(GRIDN(J) - GRIDN1(K2)) .GT. DELTAD) GO TO 107
          GO TO 24
      107 IF (GRIDN(J) .LT. GRIDN1(K2)) GO TO 11
          K1 = K2
          K2 = K2 + 1
          GO TO 13
C
C--- POINTS K1 AND K2 ON LINE B ARE AT THE SAME ELEVATION AS POINT J ON
C--- LINE A. CALL SUBROUTINE INTLINE TWICE TO CALCULATE TWO SETS OF
C--- POINTS ON INTERMEDIATE LINES. TEST 21) IS SUCCESSFUL.
C
      24 CALL INTLINE (K1,J,I3,I4,XGRIDN,XGRIDZ,GRIDN,GRIDEL,GRIDN1,GRIDL1)
      108 CALL INTLINE (K2,J,I3,I4,XGRIDN,XGRIDZ,GRIDN,GRIDEL,GRIDN1,GRIDL1)
      110 J = J + 1
C
C--- SEVERAL TESTS TO SEE IF J BEYOND LAST POINT ON THE GRID LINE (J
C--- .GT. JL). BRANCHING DEPENDENT ON VALUE OF K2.
C
      IF (J .GT. JL .AND. K2 .EQ. KL) GO TO 12
      IF (J .GT. JL .AND. K2 .LT. KL) GO TO 109
      K1 = K2
      K2 = K2 + 1
      IF (K2 .LE. KL) GO TO 13
C
C--- TRY TO MATCH UP ALL REMAINING #J# POINTS ON LINE A WITH THE LAST
C--- (NOW K1) B-LINE POINT.
C
      DO 14 I=J,JL
          IF (ABS(GRIDN(I) - GRIDN1(K1)) .GT. DELTAD) GO TO 14
          CALL INTLINE (K1,I,I3,I4,XGRIDN,XGRIDZ,GRIDN,GRIDEL,GRIDN1,GRIDL1)
      14 CONTINUE
          GO TO 12
C
C--- MATCH UP, ONE AT A TIME, THE LAST (J = JL) POINT ON LINE A WITH
C--- THE REMAINING POINTS ON LINE B. CYCLE THROUGH STATEMENT 108.
C
      109 J = J - 1
          K2 = K2 + 1
          IF (ABS(GRIDN(J) - GRIDN1(K2)) .LE. DELTAD) GO TO 108
          GO TO 110
C
C--- TEST FOR SITUATION 21I)
C
      10 IF (GRIDEL(J) .NE. GRIDL1(K1) .AND. GRIDEL(J) .EQ. GRIDL1(K2))
          GO TO 15
C
C--- TEST FOR SITUATION 21II)
C
      IF (GRIDEL(J) .EQ. GRIDL1(K1) .AND. GRIDEL(J) .NE. GRIDL1(K2))
          GO TO 16

```



```

C
C--- SITUATION 2IV) BY DEFAULT. TEST FOR TWO CONSECUTIVE EQUAL
C--- ELEVATION POINTS SATISFYING DISTANCE REQUIREMENTS.
C
    K3 = K2 + 1
    IF (K3 .GT. KL) GO TO 17
    DIST1 = ABS(GRIDN(J) - GRIDN1(K2))
    DO 18 I=K3,KL
    DIST2 = ABS(GRIDN(J) - GRIDN1(I))
    IF (DIST2 .GT. DELTAD .AND. DIST2 .GT. DIST1) GO TO 17
    I1 = I + 1
    IF (I1 .GT. KL) GO TO 18
    DISTI1 = ABS(GRIDN(J) - GRIDN1(I1))
    IF ((GRIDEL(J) - GRIDL1(I1)) .EQ. 0. .AND. (GRIDEL(J) - GRIDL1(I1))
1 .EQ. 0. .AND. (DIST2 .LE. DELTAD .OR. DISTI1 .LE. DELTAD)) GO TO
2 19
    DIST1 = DIST2
18 CONTINUE
    GO TO 17
15 K3 = K2 + 1
    IF (K3 .GT. KL) GO TO 16
    IF (GRIDEL(J) .NE. GRIDL1(K3)) GO TO 16
    IF (J .EQ. 1) GO TO 20
21 K1 = K2
    K2 = K3
    GO TO 16
C
C--- ROUTINE TO MAKE CERTAIN THAT THERE WILL DEFINITELY BE A POINT ON
C--- THE INT. GRID LINES EQUAL TO NSTART.  THUS, J = 1 POINT WILL BE
C--- USED TO CALCULATE 3 INSTEAD OF 2 SETS OF INT. GRID POINTS.
C
20 CALL INTLINE (K1,J,I3,I4,XGRIDN,XGRIDZ,GRIDN,GRIDEL,GRIDN1,GRIDL1)
    GO TO 21
19 IF (J .EQ. 1) GO TO 22
23 K1 = 1
    K2 = I1
    GO TO 24
C
C--- ROUTINE TO MAKE CERTAIN THAT THERE WILL DEFINITELY BE A POINT ON
C--- THE INT. GRID LINES EQUAL TO NSTART.
C
22 CALL INTLINE (K1,J,I3,I4,XGRIDN,XGRIDZ,GRIDN,GRIDEL,GRIDN1,GRIDL1)
    GO TO 23
C
C--- SITUATION 2IVB) FOR TWO B-LINE POINTS AT UNEQUAL ELEVATIONS - THE
C--- GENERAL, HILLSLOPE CASE.  NOTE - FOR EACH #A# POINT THERE DOES NOT
C--- HAVE TO BE ANY #B# POINTS #USED UP#.  IF ONE OR NO INT. LINE SETS
C--- CALCULATED, K1 REMAINS EQUAL TO K1.  PTPLT USED AS COUNTER.
C
17 KK = K1
    PTPLT = 0
    DIST1 = ABS(GRIDN(J) - GRIDN1(KK))
    DO 25 I=K2,KL
    DIST2 = ABS(GRIDN(J) - GRIDN1(I))
    IF (DIST1 .LE. DELTAD) GO TO 26
27 IF (DIST2 .GT. DELTAD .AND. DIST2 .GT. DIST1) GO TO 11
    DIST1 = DIST2
25 KK = KK + 1
    GO TO 11
C

```

```

C--- K1 SET TO KK SJ THAT K1 WILL BE THE INDEX OF THE LAST USED B POINT
C
26 K1 = KK
   K2 = KK + 1
   PTPLT = PTPLT + 1
   CALL INTLINE (KK,J,13,14,XGRIDN,XGRIDZ,GRIDN,GRIDEL,GRIDN1,GRIDL1)
   IF (PTPLT .EQ. 2) GO TO 11
   GO TO 27
C
C--- NOTE THAT AT STATEMENT 11, K2 CANNOT EQUAL KK+1 WHEN KK = K2,
C--- SINCE AT COMPLETION OF DO LOOP I=K2,KL, PROGRAM GOES DIRECTLY TO
C--- STATEMENT 11.  THUS, K2 CAN NEVER BE .GT. K.
C
11 J = J + 1
   IF (J .LE. JL) GO TO 13
C
C--- THIS STEP BELOW ALWAYS OK.  SEE NOTE JUST ABOVE.
C
   IF (K2 .EQ. KL) GO TO 106
   J = J - 1
   IF (PTPLT .EQ. 2) GO TO 111
   K1 = K2
   K2 = K2 + 1
   GO TO 13
106 IF (KK .LT. KL) GO TO 12
   IF (DIST1 .GT. DELTAD) GO TO 12
   J = J - 1
111 CALL INTLINE (KL,J,13,14,XGRIDN,XGRIDZ,GRIDN,GRIDEL,GRIDN1,GRIDL1)
C
C--- AT THIS POINT, ALL INTERMEDIATE LINES BETWEEN A AND B ARE
C--- COMPLETE.  NOW, PLACE ARRAYS INTO UNIT 82 OR PUNCH.
C
12 IF (FMT(1) .NE. D2) GO TO 200
   WRITE (82)(GRIDN(I),GRIDEL(I),I=1,ICOUNT)
   GO TO 201
200 INDEX = ICOUNT/NUMPTC
   INDEXA = ICOUNT - INDEX*NUMPTC
   DO 206 J=1,INDEX
206 PUNCH FMT, (GRIDN(I),GRIDEL(I),I=1,NUMPTC)
   IF (INDEXA .GT. 0) PUNCH FMT, (GRIDN(I),GRIDEL(I),I=1,INDEXA)
   PUNCH 800
800 FORMAT (80X)
201 NUM = NUM + 1
   DO 51 L=1,I3
   IF (FMT(1) .NE. D2) GO TO 202
   WRITE (82) (XGRIDN(L,I),XGRIDZ(L,I),I=1,INTCT)
   GO TO 203
202 INDEX = INTCT/NUMPTC
   INDEXA = INTCT - INDEX*NUMPTC
   DO 207 J=1,INDEX
207 PUNCH FMT, (XGRIDN(L,I),XGRIDZ(L,I),I=1,NUMPTC)
   IF (INDEXA .GT. 0) PUNCH FMT, (XGRIDN(L,I),XGRIDZ(L,I),I=1,NUMPTC)
   PUNCH 800
203 NUM = NUM + 1
   51 NUMPT(NUM) = FLOAT(INTCT)
   IF (II .LT. I2) GO TO 53
   IF (FMT(1) .NE. D2) GO TO 204
   WRITE (82) (GRIDN1(I),GRIDL1(I),I=1,ICNT1)
   GO TO 205
204 INDEX = ICNT1/NUMPTC

```

```

INDEXA = ICNT1 - INDEX*NUMPTC
DC 208 J=1,INDEX
208 PUNCH FMT, (GRIDN1(I),GRIDL1(I),I=1,NUMPTC)
IF (INDEXA .GT. 0) PUNCH FMT, (GRIDN1(I),GRIDL1(I),I=1,INDEXA)
PUNCH 800
205 GO TO 9
C
C--- LOAD LINE B POINTS INTO LINE A, PRIOR TO NEXT PASS THROUGH LOOP.
C
53 DO 52 I=1,ICNT1
GRIDN(I) = GRIDN1(I)
52 GRIDL(I) = GRIDL1(I)
ICOUNT = ICNT1
5 CONTINUE
C
C--- DETERMINE IF NUMPT ARRAY IS TO BE PUNCHED AS LAST LOGICAL RECORD.
C
IF (PNCH .NE. 01) GO TO 40
WRITE (82) (NUMPT(I),I=1,I2)
40 RETURN
END

```

```

SUBROUTINE INTLINE (K,J,I3,I4,XN,XZ,GN,GEL,GN1,GL1)
COMMON /I3DPS/ INTCT,F13
REAL XN(I3,I4),XZ(I3,I4),GN(1),GEL(1),GN1(1),GL1(1)

```

```

C
C--- ROUTINE TO CALCULATE ONE POINT FOR EACH OF I3 INT. GRID LINES.
C
INTCT = INTCT + 1
F = F13
DO 1 I=1,I3
XN(I,INTCT) = (GN1(K) - GN(J))*F + GN(J)
XZ(I,INTCT) = (GL1(K) - GEL(J))*F + GEL(J)
1 F = F + F13
RETURN
END

```

Example 3

```

PROGRAM MAIN (OUTPUT,TAPE83,TAPE99)
DIMENSION SPECS(30),Z(283)
COMMON BUFI(1308)
CCOMMON /WSPECS/RSPECS(30),ISPECS(10)
SPECS(1) = 1.
SPECS(2) = 0.5
SPECS(3) = 46.
SPECS(4) = 1.
SPECS(5) = 10.0
SPECS(6) = 0.5
SPECS(7) = 45.0
SPECS(8) = 9.5
SPECS(11) = 1.
SPECS(12) = 99.
ISPECS(2) = 80
ISPECS(5) = 283
ISPECS(6) = 1
ISPECS(7) = 1
ISPECS(8) = 3
ISPECS(9) = 1
ISPECS(10) = 1
RSPECS(1) = .25
RSPECS(2) = 0.
RSPECS(3) = 0.
RSPECS(4) = 0.
RSPECS(5) = 12.5
RSPECS(7) = .07
RSPECS(10) = 5.
RSPECS(11) = 28.
RSPECS(12) = 2.
RSPECS(13) = 23.
RSPECS(14) = 44.
RSPECS(15) = 0.
RSPECS(16) = 0.
RSPECS(21) = 1.
RSPECS(22) = 7.
RSPECS(23) = -1.
RSPECS(28) = .5
RSPECS(29) = .5
RSPECS(30) = 1.
BUFI(1133) = BUFI(1134) = BUFI(1135) = 1.
BUFI(1139) = 0.
BUFI(1140) = 19.75
BUFI(1141) = 0.
BUFI(1142) = 5.11
BUFI(1143) = 14.84
BUFI(1144) = 19.74
REWIND 83
REAST = 0.
DO 1 I=1,80
RNORTH = 0.
DO 2 J=1,283
Z(J) = 1.5/SQRT((REAST - 5.375)**2 + (RNORTH -14.875)**2)
1+      1.5/SQRT((REAST - 7.125)**2 + (RNORTH -14.875)**2)
2+      1.5/SQRT((REAST -13.125)**2 + (RNORTH -14.875)**2)

```

```
3+      1.5/SQRT((REAST -14.375)**2 + (RNORTH -14.875)**2)
4+      1.5/SQRT((REAST - 9.125)**2 + (RNORTH - 5.125)**2)
5+      1.5/SQRT((REAST -10.375)**2 + (RNORTH - 5.125)**2)
  RNORTH = RNORTH + .07
2 CONTINUE
  WRITE (83) (Z(N),N=1,283)
  REAST = REAST + .25
1 CONTINUE
  REWIND 83
  CALL I3D1GL (BUF1,1308,SPECS)
  CALL GDSEND(SPECS)
  STOP
  END
```



FIRST LINE, ALPHA1, ANGLE TO N-S LINE FROM HORIZONTAL  
 SECOND LINE, ALPHA2, ANGLE TO E-W LINE FROM HORIZONTAL

41	85.8	83.7	82.0	80.4	79.0	77.6	76.3	74.9	73.7	72.4
	-58.2	-45.9	-37.6	-31.1	-25.9	-21.5	-17.6	-14.2	-11.1	-8.3
40	86.9	84.0	82.0	80.2	78.6	77.1	75.6	74.2	72.8	
	-70.2	-53.9	-44.2	-36.9	-31.0	-26.1	-21.9	-18.1	-14.8	
39	84.7	82.1	80.1	78.3	76.6	75.0	73.5			
	-61.4	-50.0	-41.8	-35.4	-30.1	-25.5	-21.5			
38	85.6	82.4	80.1	78.0	76.2	74.4				
	-68.9	-55.1	-46.1	-39.2	-33.5	-28.8				
37	87.1	82.8	80.1	77.8	75.7					
	-77.5	-59.8	-49.9	-42.4	-36.4					
36	83.3	80.1	77.5							
	-64.0	-53.1	-45.1							
35	83.8	80.1								
	-67.9	-55.8								
34	84.4									
	-71.5									

GAMMA

33

32

31

30

29

28

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17

PSI





FIRST LINE, ALPHA1, ANGLE TO N-S LINE FROM HORIZONTAL  
 SECOND LINE, ALPHA2, ANGLE TO E-W LINE FROM HORIZONTAL

41	71.1	69.9	66.7	67.4	66.2	65.0	63.8	62.6	61.4	60.1	58.9	57.7	56.5	55.3	54.1	52.9	51.6	50.4
	-5.7	-3.3	-1.0	1.2	3.2	5.2	7.0	8.8	10.6	12.3	13.9	15.5	17.1	18.6	20.1	21.6	23.1	24.5
40	71.4	70.1	68.8	67.5	66.2	64.9	63.6	62.3	61.0	59.8	58.5	57.2	55.9	54.7	53.4	52.1	50.8	49.5
	-11.7	-8.8	-6.2	-3.7	-1.4	.8	2.9	5.0	6.9	8.8	10.6	12.4	14.1	15.8	17.4	19.0	20.6	22.1
39	72.0	70.5	69.1	67.7	66.3	64.9	63.6	62.2	60.9	59.5	58.2	56.8	55.5	54.1	52.8	51.5	50.1	48.8
	-17.8	-14.5	-11.5	-8.7	-6.0	-3.5	-1.2	1.1	3.2	5.3	7.3	9.2	11.1	12.9	14.7	16.4	18.1	19.7
38	72.8	71.2	69.6	68.1	66.6	65.1	63.7	62.2	60.6	59.4	58.0	56.6	55.1	53.7	52.3	50.9	49.5	48.1
	-24.3	-20.4	-16.9	-13.7	-10.7	-7.9	-5.3	-2.8	-.4	1.8	4.0	6.1	8.1	10.1	12.0	13.8	15.7	17.4
37	73.9	72.1	70.4	68.7	67.1	65.5	64.0	62.4	60.9	59.4	57.9	56.4	54.9	53.4	51.9	50.4	49.0	47.5
	-31.2	-26.7	-22.6	-18.9	-15.6	-12.4	-9.5	-6.8	-4.2	-1.7	.7	3.0	5.2	7.3	9.3	11.3	13.3	15.1
36	75.3	73.3	71.4	69.5	67.8	66.1	64.4	62.7	61.1	59.5	57.9	56.3	54.8	53.2	51.6	50.1	48.5	47.0
	-38.8	-33.4	-28.6	-24.4	-20.6	-17.1	-13.8	-10.8	-7.9	-5.2	-2.6	-.2	2.2	4.5	6.7	8.8	10.9	12.9
35	77.3	74.9	72.7	70.6	68.7	66.8	65.0	63.2	61.5	59.8	58.1	56.4	54.7	53.1	51.4	49.8	48.2	46.5
	-47.4	-40.8	-35.2	-30.3	-25.9	-21.9	-18.3	-14.9	-11.8	-8.8	-6.0	-3.3	-.8	1.7	4.0	6.3	8.5	10.6
34	80.1	77.0	74.4	72.0	69.9	67.8	65.8	63.9	62.0	60.2	58.4	56.6	54.8	53.1	51.3	49.6	47.9	46.2
	-58.1	-49.3	-42.4	-35.6	-31.5	-27.0	-23.0	-19.2	-15.8	-12.5	-9.5	-6.6	-3.8	-1.2	1.3	3.8	6.1	8.4
33	85.1	80.1	76.7	73.9	71.4	69.0	66.8	64.7	62.7	60.7	58.8	56.9	55.0	53.2	51.3	49.5	47.7	45.9
	-74.8	-60.0	-50.8	-43.7	-37.7	-32.5	-27.9	-23.7	-19.9	-16.4	-13.0	-9.9	-6.9	-4.1	-1.4	1.2	3.7	6.1
32	85.8	80.0	76.3	73.3	70.6	68.1	65.8	63.6	61.5	59.4	57.4	55.4	53.4	51.4	49.4	47.4	45.4	43.7
	-77.7	-61.5	-52.0	-44.6	-38.5	-33.2	-28.5	-24.3	-20.4	-16.7	-13.3	-10.1	-7.1	-4.1	-1.4	1.3	3.9	6.3
31	80.4	79.8	75.8	72.6	69.8	67.2	64.7	62.4	60.1	58.0	55.8	53.7	51.7	49.6	47.6	45.6	43.6	41.6
	-80.2	-62.5	-52.7	-45.3	-39.1	-33.7	-28.9	-24.6	-20.6	-16.9	-13.4	-10.1	-7.0	-4.0	-1.2	1.6	4.0	6.4
30	86.9	79.5	75.3	71.9	68.9	66.1	63.5	61.1	58.7	56.4	54.2	52.0	49.8	47.7	45.6	43.5	41.4	39.3
	-82.0	-63.2	-53.2	-45.6	-39.4	-33.9	-29.0	-24.6	-20.6	-16.8	-13.2	-9.9	-6.7	-3.7	-.8	4.1	6.5	8.9
29	87.1	79.1	74.6	71.0	67.9	65.0	62.3	59.7	57.2	54.8	52.5	50.2	47.9	45.6	43.3	41.0	38.7	36.4
	-82.9	-63.4	-53.4	-45.7	-39.4	-33.9	-29.0	-24.5	-20.3	-16.5	-12.9	-9.5	-6.2	-3.1	1.1	3.5	5.9	8.3
28	86.8	78.5	73.8	70.0	66.7	63.7	60.9	58.2	55.6	53.1	50.6	48.2	45.8	43.3	40.8	38.4	35.9	33.4
	-82.5	-63.3	-53.2	-45.6	-39.2	-33.6	-28.7	-24.1	-19.9	-16.0	-12.4	-8.9	-5.6	-2.3	1.1	3.5	5.9	8.3

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FIRST LINE, ALPHA, ANGLE TO N-S LINE FROM HORIZONTAL  
 SECOND LINE, ALPHA, ANGLE TO E-W LINE FROM HORIZONTAL

27	86.1	77.7	72.9	69.0	65.5	62.4	59.4	56.6	53.9	51.2	48.7	46.1
	-81.1	-62.8	-52.8	-45.2	-38.8	-33.2	-28.1	-23.6	-19.3	-15.4	-11.6	-8.1
26	85.0	76.8	71.8	67.7	64.2	60.9	57.8	54.8	52.0	49.2	46.5	
	-79.2	-62.1	-52.2	-44.6	-38.1	-32.5	-27.4	-22.8	-18.5	-14.5	-10.7	
25	83.7	75.7	70.6	66.4	62.7	59.2	56.0	52.9	50.0	47.1		
	-76.9	-61.0	-51.3	-43.7	-37.3	-31.6	-26.6	-21.9	-17.5	-13.5		
24	82.2	74.4	69.2	64.9	61.0	57.5	54.1	50.9	47.8			
	-74.5	-59.7	-50.2	-42.7	-36.3	-30.6	-25.5	-20.7	-16.4			
23	80.5	73.0	67.7	63.2	59.2	55.5	52.0	48.7				
	-72.0	-58.2	-48.9	-41.4	-35.0	-29.3	-24.2	-19.4				
22	78.7	71.4	66.0	61.4	57.3	53.4	49.8					
	-69.4	-56.5	-47.4	-40.0	-33.6	-27.9	-22.7					
21	76.8	69.6	64.1	59.4	55.1	51.1						
	-66.7	-54.6	-45.7	-38.3	-32.0	-26.2						
20	74.7	67.6	62.0	57.2	52.7							
	-64.0	-52.5	-43.8	-36.5	-30.1							
19	85.0	72.5	65.4	59.7	54.7							
	-81.6	-61.2	-50.2	-41.7	-34.5							
18	80.8	70.1	63.0	57.2								
	-75.1	-58.3	-47.8	-39.4								
17	77.3	67.4	60.4									
	-70.2	-55.3	-45.1									
16	73.9	64.6										
	-65.7	-52.2										
15	70.5											
	-61.5											
14	81.7											
	-78.1											

PSI

18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35

FIRST LINE, ALPHA1, ANGLE TO N-S LINE FROM HORIZONTAL  
 SECOND LINE, ALPHA2, ANGLE TO E-W LINE FROM HORIZONTAL

55

54	81.7	80.8	80.0	79.3	78.7	78.2	77.7	77.3	77.0	76.7	76.5	76.4	76.3	76.4	76.5	76.8	76.8	77.2	77.7	78.5
	78.5	77.7	77.2	76.8	76.5	76.4	76.3	76.4	76.5	76.7	77.0	77.3	77.7	78.2	78.7	79.3	80.0	80.8	81.7	
53	74.6	73.9	73.3	72.7	72.1	71.6	71.1	70.6	70.2	69.8	69.4	69.1	68.9	68.7	68.5	68.4	68.4	68.4	68.4	68.6
	68.6	68.4	68.4	68.4	68.5	68.7	68.9	69.1	69.4	69.8	70.2	70.6	71.1	71.6	72.1	72.7	73.3	73.9	74.6	
52	70.1	69.4	68.8	68.1	67.5	66.9	66.4	65.8	65.3	64.8	64.4	64.0	63.6	63.2	62.9	62.6	62.4	62.2	62.1	62.1
	62.1	62.2	62.4	62.6	62.9	63.2	63.6	64.0	64.4	64.8	65.3	65.8	66.4	66.9	67.5	68.1	68.8	69.4	70.1	
51	66.6	65.9	65.2	64.5	63.9	63.2	62.6	62.0	61.4	60.8	60.3	59.8	59.3	58.8	58.3	57.9	57.5	57.2	56.9	56.9
	56.9	57.2	57.5	57.9	58.3	58.8	59.3	59.8	60.3	60.8	61.4	62.0	62.6	63.2	63.9	64.5	65.2	65.9	66.6	
50	63.7	63.0	62.2	61.5	60.8	60.1	59.4	58.7	58.1	57.4	56.8	56.2	55.6	55.0	54.5	53.9	53.4	52.9	52.5	52.5
	52.5	52.9	53.4	53.9	54.5	55.0	55.6	56.2	56.8	57.4	58.1	58.7	59.4	60.1	60.8	61.5	62.2	63.0	63.7	
49	61.3	60.5	59.7	58.9	58.1	57.4	56.6	55.9	55.2	54.4	53.7	53.0	52.3	51.7	51.0	50.4	49.8	49.2	48.6	48.6
	48.6	49.2	49.8	50.4	51.0	51.7	52.3	53.0	53.7	54.4	55.2	55.9	56.6	57.4	58.1	58.9	59.7	60.5	61.3	
48	59.1	58.3	57.4	56.6	55.8	55.0	54.2	53.3	52.5	51.8	51.0	50.2	49.4	48.7	47.9	47.2	46.5	45.8	45.1	45.1
	45.1	45.8	46.5	47.2	47.9	48.7	49.4	50.2	51.0	51.8	52.5	53.3	54.2	55.0	55.8	56.6	57.4	58.3	59.1	
47	57.2	56.3	55.4	54.6	53.7	52.8	51.9	51.0	50.2	49.3	48.5	47.6	46.8	45.9	45.1	44.3	43.4	42.6	41.8	41.8
	41.8	42.6	43.4	44.3	45.1	45.9	46.8	47.6	48.5	49.3	50.2	51.0	51.9	52.8	53.7	54.6	55.4	56.3	57.2	
46	55.5	54.6	53.6	52.7	51.8	50.8	49.9	48.9	48.0	47.1	46.1	45.2	44.3	43.4	42.5	41.5	40.6	39.7	38.8	38.8
	38.8	39.7	40.6	41.5	42.5	43.4	44.3	45.2	46.1	47.1	48.0	48.9	49.9	50.8	51.8	52.7	53.6	54.6	55.5	
45	54.0	53.0	52.0	51.0	50.0	49.0	48.0	47.0	46.0	45.0	44.0	43.0	42.0	41.0	40.0	39.0	38.0	37.0	36.0	36.0
	36.0	37.0	38.0	39.0	40.0	41.0	42.0	43.0	44.0	45.0	46.0	47.0	48.0	49.0	50.0	51.0	52.0	53.0	54.0	
44	52.6	51.6	50.5	49.4	48.4	47.3	46.3	45.2	44.1	43.1	42.0	40.9	39.8	38.8	37.7	36.6	35.5	34.4	33.3	33.3
	33.3	34.4	35.5	36.6	37.7	38.8	39.8	40.9	42.0	43.1	44.1	45.2	46.3	47.3	48.4	49.4	50.5	51.6	52.6	
43	51.4	50.3	49.1	48.0	46.9	45.8	44.7	43.5	42.4	41.3	40.1	39.0	37.8	36.7	35.5	34.3	33.1	31.9	30.8	30.8
	30.8	31.9	33.1	34.3	35.5	36.7	37.8	39.0	40.1	41.3	42.4	43.5	44.7	45.8	46.9	48.0	49.1	50.3	51.4	
42	50.2	49.1	47.9	46.7	45.5	44.3	43.2	42.0	40.8	39.5	38.3	37.1	35.9	34.6	33.4	32.1	30.9	29.6	28.3	28.3
	28.3	29.6	30.9	32.1	33.4	34.6	35.9	37.1	38.3	39.5	40.8	42.0	43.2	44.3	45.5	46.7	47.9	49.1	50.2	
36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54		

PSI

FIRST LINE, ALPHA1, ANGLE TO N-S LINE FROM HORIZONTAL  
 SECOND LINE, ALPHA2, ANGLE TO E-W LINE FROM HORIZONTAL

41	49.2	48.0	46.7	45.5	44.2	43.0	41.7	40.5	39.2	37.9	36.6	35.3	34.0	32.7	31.4	30.0	28.7	27.3	25.9
	25.9	27.3	28.7	30.0	31.4	32.7	34.0	35.3	36.6	37.9	39.2	40.5	41.7	43.0	44.2	45.5	46.7	48.0	49.2
40	48.3	47.0	45.7	44.4	43.1	41.7	40.4	39.1	37.7	36.4	35.0	33.7	32.3	30.9	29.5	28.0	26.6	25.1	23.6
	23.6	25.1	26.6	28.0	29.5	30.9	32.3	33.7	35.0	36.4	37.7	39.1	40.4	41.7	43.1	44.4	45.7	47.0	48.3
39	47.4	46.1	44.7	43.3	42.0	40.6	39.2	37.8	36.4	34.9	33.5	32.0	30.6	29.1	27.6	26.1	24.5	23.0	21.4
	21.4	23.0	24.5	26.1	27.6	29.1	30.6	32.0	33.5	34.9	36.4	37.8	39.2	40.6	42.0	43.3	44.7	46.1	47.4
38	46.7	45.2	43.8	42.4	40.5	39.5	38.0	36.5	35.0	33.5	32.0	30.5	28.9	27.4	25.8	24.2	22.5	20.9	19.2
	19.2	20.9	22.5	24.2	25.8	27.4	28.9	30.5	32.0	33.5	35.0	36.5	38.0	39.5	40.9	42.4	43.8	45.2	46.7
37	46.0	44.5	43.0	41.5	40.0	38.4	36.9	35.3	33.8	32.2	30.6	29.0	27.4	25.7	24.0	22.3	20.6	18.8	17.0
	17.0	18.8	20.6	22.3	24.0	25.7	27.4	29.0	30.6	32.2	33.8	35.3	36.9	38.4	40.0	41.5	43.0	44.5	46.0
36	45.4	43.8	42.2	40.7	39.1	37.5	35.8	34.2	32.6	30.9	29.2	27.5	25.8	24.1	22.3	20.5	18.6	16.8	14.8
	14.8	16.8	18.6	20.5	22.3	24.1	25.8	27.5	29.2	30.9	32.6	34.2	35.8	37.5	39.1	40.7	42.2	43.8	45.4
35	44.9	43.2	41.6	39.9	38.2	36.6	34.9	33.1	31.4	29.7	27.9	26.1	24.3	22.5	20.6	18.7	16.7	14.8	12.7
	12.7	14.8	16.7	18.7	20.6	22.5	24.3	26.1	27.9	29.7	31.4	33.1	34.9	36.6	38.2	39.9	41.6	43.2	44.9
34	44.4	42.7	41.0	39.2	37.5	35.7	33.9	32.1	30.3	28.5	26.6	24.8	22.8	20.9	18.9	16.9	14.9	12.8	10.6
	10.6	12.8	14.9	16.9	18.9	20.9	22.8	24.8	26.6	28.5	30.3	32.1	33.9	35.7	37.5	39.2	41.0	42.7	44.4
33	44.1	42.2	40.4	38.6	36.8	34.9	33.0	31.2	29.3	27.3	25.4	23.4	21.4	19.4	17.3	15.2	13.0	10.8	8.5
	8.5	10.8	13.0	15.2	17.3	19.4	21.4	23.4	25.4	27.3	29.3	31.2	33.0	34.9	36.8	38.6	40.4	42.2	44.1
32	43.8	41.9	40.0	38.0	36.1	34.2	32.2	30.2	28.2	26.2	24.2	22.1	20.0	17.8	15.7	13.4	11.1	8.8	6.4
	6.4	8.8	11.1	13.4	15.7	17.8	20.0	22.1	24.2	26.2	28.2	30.2	32.2	34.2	36.1	38.0	40.0	41.9	43.8
31	43.6	41.6	39.5	37.5	35.5	33.5	31.4	29.4	27.3	25.1	23.0	20.8	18.6	16.3	14.0	11.7	9.3	6.8	4.2
	4.2	6.8	9.3	11.7	14.0	16.3	18.6	20.8	23.0	25.1	27.3	29.4	31.4	33.5	35.5	37.5	39.5	41.6	43.6
30	43.4	41.3	39.2	37.1	35.0	32.8	30.7	28.5	26.3	24.1	21.8	19.6	17.2	14.9	12.4	9.9	7.4	4.8	2.1
	2.1	4.8	7.4	9.9	12.4	14.9	17.2	19.6	21.8	24.1	26.3	28.5	30.7	32.8	35.0	37.1	39.2	41.3	43.4
29	43.4	41.2	38.9	36.7	34.5	32.2	30.0	27.7	25.4	23.1	20.7	18.3	15.9	13.4	10.8	8.2	5.5	2.7	-0.2
	-0.2	2.7	5.5	8.2	10.8	13.4	15.9	18.3	20.7	23.1	25.4	27.7	30.0	32.2	34.5	36.7	38.9	41.2	43.4
28	43.5	41.1	38.8	36.4	34.1	31.7	29.3	26.9	24.5	22.1	19.6	17.1	14.5	11.9	9.2	6.4	3.6	0.6	-2.4
	-2.4	0.6	3.6	5.4	9.2	11.9	14.5	17.1	19.6	22.1	24.5	26.9	29.3	31.7	34.1	36.4	38.8	41.1	43.5
36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	

GAMMA

PSI

FIRST LINE, ALPHA1, ANGLE TO N-S LINE FROM HORIZONTAL  
 SECOND LINE, ALPHA2, ANGLE TO E-W LINE FROM HORIZONTAL

27	43.6	41.1	38.7	36.2	33.7	31.2	28.7	26.2	23.7	21.1	18.5	15.9	13.1	10.4	7.5	4.6	1.6	-1.2	-4.7
	-4.7	-1.5	1.6	4.6	7.5	10.4	13.1	15.9	18.5	21.1	23.7	26.2	28.7	31.2	33.7	36.2	38.7	41.1	43.6
26	43.9	41.2	38.0	36.0	33.4	30.8	28.2	25.5	22.9	20.2	17.4	14.6	11.8	8.9	5.9	2.8	-.4	-3.7	-7.1
	-7.1	-3.7	-.4	2.8	5.9	8.9	11.8	14.6	17.4	20.2	22.9	25.5	28.2	30.8	33.4	36.0	38.0	41.2	43.9
25	44.2	41.5	38.7	35.9	33.2	30.4	27.7	24.9	22.1	19.3	16.4	13.4	10.4	7.3	4.2	.9	-2.4	-6.0	-9.6
	-9.6	-6.0	-2.4	.9	4.2	7.3	10.4	13.4	16.4	19.3	22.1	24.9	27.7	30.4	33.2	35.9	38.7	41.5	44.2
24	44.8	41.8	38.8	35.9	33.0	30.1	27.2	24.3	21.3	18.4	15.3	12.2	9.0	5.8	2.5	-1.0	-4.6	-8.3	-12.2
	-12.2	-8.3	-4.6	-1.0	2.5	5.8	9.0	12.2	15.3	18.4	21.3	24.3	27.2	30.1	33.0	35.9	38.8	41.8	44.8
23	45.4	42.2	39.1	36.0	33.0	29.9	26.8	23.7	20.6	17.5	14.3	11.0	7.7	4.2	.7	-3.0	-6.8	-10.8	-15.0
	-15.0	-10.8	-6.8	-3.0	.7	4.2	7.7	11.0	14.3	17.5	20.6	23.7	26.8	29.9	33.0	36.0	39.1	42.2	45.4
22	46.3	42.8	39.2	36.2	33.0	29.7	26.5	23.2	19.9	16.6	13.2	9.8	6.2	2.6	-1.1	-5.0	-9.1	-13.4	-17.9
	-17.9	-13.4	-9.1	-5.0	-1.1	2.6	6.2	9.8	13.2	16.6	19.9	23.2	26.5	29.7	33.0	36.2	39.2	42.8	46.3
21	47.3	43.6	40.0	36.5	33.1	29.6	26.2	22.7	19.3	15.7	12.2	8.5	4.8	.9	-3.1	-7.2	-11.5	-16.1	-21.0
	-21.0	-16.1	-11.5	-7.2	-3.1	.9	4.8	8.5	12.2	15.7	19.3	22.7	26.2	29.6	33.1	36.5	40.0	43.6	47.3
20	48.6	44.6	40.7	37.0	33.3	29.6	26.0	22.3	18.6	14.9	11.1	7.3	3.3	-.8	-5.0	-9.5	-14.1	-19.1	-24.4
	-24.4	-19.1	-14.1	-9.5	-5.0	-.8	3.3	7.3	11.1	14.9	18.6	22.3	26.0	29.6	33.3	37.0	40.7	44.6	48.6
GAMMA	19	50.1	45.8	41.6	37.6	33.6	29.7	25.8	22.0	18.0	14.1	10.1	6.0	1.7	-2.6	-7.1	-11.9	-16.9	-22.1
	-22.1	-16.9	-11.9	-7.1	-2.6	1.7	6.0	10.1	14.1	18.0	22.0	25.8	29.7	33.6	37.6	41.6	45.8	50.1	
18	52.1	47.3	42.7	38.4	34.1	29.9	25.8	21.6	17.5	13.3	9.0	4.6	.1	-4.5	-9.4	-14.5	-19.9	-25.8	-32.2
	-32.2	-25.8	-19.9	-14.5	-9.4	-4.5	.1	4.6	9.0	13.3	17.5	21.6	25.8	29.9	34.1	38.4	42.7	47.3	52.1
17	54.5	49.1	44.1	39.4	34.8	30.3	25.8	21.4	17.0	12.5	7.9	3.3	-1.5	-6.5	-11.8	-17.3	-23.2	-29.7	-36.9
	-36.9	-29.7	-23.2	-17.3	-11.8	-6.5	-1.5	3.3	7.9	12.5	17.0	21.4	25.8	30.3	34.8	39.4	44.1	49.1	54.5
16	57.5	51.4	45.8	40.6	35.6	30.8	26.0	21.2	16.5	11.7	6.8	1.8	-3.3	-8.7	-14.4	-20.4	-26.9	-34.1	-42.3
	-42.3	-34.1	-26.9	-20.4	-14.4	-8.7	-3.3	1.8	6.8	11.7	16.5	21.2	26.0	30.8	35.6	40.6	45.8	51.4	57.5
15	61.4	54.3	48.0	42.2	36.7	31.4	26.3	21.2	16.1	10.9	5.7	.3	-5.2	-11.0	-17.2	-23.8	-31.0	-38.9	-48.9
	-48.9	-38.9	-31.0	-23.8	-17.2	-11.0	-5.2	.3	5.7	10.9	16.1	21.2	26.3	31.4	36.7	42.2	48.0	54.3	61.4
14	66.9	58.0	50.7	44.2	38.1	32.3	26.7	21.2	15.7	10.2	4.5	-1.3	-7.3	-13.6	-20.4	-27.7	-35.8	-45.3	-57.4
	-57.4	-45.3	-35.8	-27.7	-20.4	-13.6	-7.3	-1.3	4.5	10.2	15.7	21.2	26.7	32.3	38.1	44.2	50.7	58.0	66.9

PSI

36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54

FIRST LINE, ALPHA1, ANGLE TU N-S LINE FROM HCRIZONTAL  
 SECONU LINE, ALPHAZ, ANGLE TU E-W LINE FROM HCRIZONTAL

13	75.9	63.1	54.2	45.7	39.9	33.5	27.4	21.4	15.4	9.4	3.3	-3.0	-9.5	-16.5	-23.9	-32.1	-41.6	-53.1	-70.4
	-70.4	-53.1	-41.6	-32.1	-23.9	-16.5	-9.5	-3.0	3.3	9.4	15.4	21.4	27.4	33.5	39.9	46.7	54.2	63.1	75.9
12	70.9	59.0	50.0	42.2	35.1	28.3	21.7	15.2	8.6	2.0	8.6	15.2	21.7	28.3	35.1	42.2	50.0	59.0	70.9
	-64.3	-48.7	-37.5	-28.0	-19.7	-12.0	-4.9	2.0	8.6	15.2	21.7	28.3	35.1	42.2	50.0	59.0	70.9		
11	65.9	54.4	45.2	37.1	29.5	22.2	15.1	7.9	0.6	7.9	15.1	22.2	29.5	37.1	45.2	54.4	65.9		
	-58.5	-44.1	-32.9	-23.4	-14.9	-6.9	0.6	7.9	15.1	22.2	29.5	37.1	45.2	54.4	65.9				
10	79.2	60.7	49.3	39.8	31.2	23.0	15.1	7.2	-0.9	7.2	15.1	23.0	31.2	39.8	49.3	60.7	79.2		
	-75.2	-52.8	-35.0	-27.8	-18.1	-9.3	-0.9	7.2	15.1	23.0	31.2	39.8	49.3	60.7	79.2				
9	71.2	55.0	43.4	33.4	24.2	15.3	6.4	-2.6	6.4	15.3	24.2	33.4	43.4	55.0	71.2				
	-60.5	-46.9	-33.3	-22.0	-11.9	-2.6	6.4	15.3	24.2	33.4	43.4	55.0	71.2						
8	63.9	48.5	36.5	25.8	15.7	5.7	-4.4	5.7	15.7	25.8	36.5	48.5	63.9						
	-58.4	-40.4	-26.8	-15.1	-4.4	5.7	-4.4	15.7	25.8	36.5	48.5	63.9							
7	56.3	40.9	28.2	16.4	5.0	-6.7	16.4	5.0	-6.7	16.4	28.2	40.9	56.3						
	-50.4	-33.0	-19.1	-6.7	5.0	16.4	28.2	40.9	56.3										
6	71.2	47.7	31.7	17.7	4.3	-9.4	17.7	4.3	-9.4	17.7	31.7	47.7	71.2						
	-68.3	-41.7	-24.2	-9.4	4.3	17.7	31.7	47.7	71.2										
5	55.6	37.2	19.8	3.5	-13.0	-31.4	3.5	-13.0	-31.4	3.5	19.8	37.2	55.6						
	-55.8	-31.4	-13.0	3.5	19.8	37.2	55.6												
4	46.9	23.3	2.8	-18.0	-42.9	2.8	-18.0	-42.9	2.8	23.3	46.9								
	-42.9	-18.0	2.8	23.3	46.9														
3	71.1	30.0	2.1	-26.2	-69.6	2.1	-26.2	-69.6	2.1	30.0	71.1								
	-69.6	-26.2	2.1	30.0	71.1														
2	46.0	1.4	-44.0	1.4	-44.0														
	-44.0	1.4	46.0	1.4	46.0														
1	.7	.7																	
	.7																		
0	.0	.0																	
	-.0																		

36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54  
 PSI

FIRST LINE, ALPHA1, ANGLE TO N-S LINE FROM HORIZONTAL  
 SECOND LINE, ALPHA2, ANGLE TO E-W LINE FROM HORIZONTAL

55

54 79.5 80.9 82.9 85.5  
 82.7 83.9 85.4 87.8

53 68.8 69.1 69.5 70.1 70.9 71.9 73.1 74.7 76.8 79.9 85.5  
 75.3 76.1 76.9 77.7 78.7 79.6 80.7 81.9 83.3 85.1 87.9

52 62.0 62.0 62.0 62.2 62.4 62.8 63.3 63.9 64.7 65.7 66.9 68.6 70.6 73.4 77.3 85.0  
 70.8 71.5 72.3 73.1 73.9 74.7 75.6 76.5 77.4 78.4 79.5 80.6 81.9 83.4 85.2 88.2

51 56.6 56.4 56.2 56.1 56.1 56.1 56.2 56.4 56.7 57.1 57.7 58.4 59.4 60.5 62.0 64.0 66.4 69.7  
 67.3 68.1 68.8 69.6 70.4 71.2 72.0 72.9 73.8 74.6 75.6 76.5 77.5 78.5 79.6 80.8 82.1 83.5

50 52.1 51.7 51.3 51.0 50.8 50.6 50.4 50.3 50.3 50.4 50.5 50.8 51.2 51.7 52.4 53.4 54.6 56.1  
 64.5 65.3 66.1 66.9 67.7 68.5 69.3 70.1 71.0 71.9 72.8 73.7 74.6 75.5 76.5 77.5 78.5 79.6

49 48.0 47.5 47.0 46.5 46.1 45.7 45.3 45.0 44.8 44.6 44.4 44.4 44.4 44.5 44.7 45.1 45.6 46.3  
 62.1 62.9 63.7 64.5 65.4 66.2 67.1 67.9 68.8 69.7 70.5 71.4 72.3 73.2 74.2 75.1 76.1 77.0

48 44.4 43.7 43.1 42.5 41.9 41.3 40.8 40.3 39.8 39.4 39.0 38.7 38.4 38.2 38.0 38.0 38.0 38.2  
 60.0 60.8 61.7 62.6 63.4 64.3 65.2 66.1 67.0 67.9 68.8 69.7 70.6 71.5 72.4 73.3 74.3 75.2

GAMMA

47 41.1 40.3 39.5 38.8 38.0 37.3 36.6 35.9 35.3 34.6 34.0 33.5 32.9 32.4 32.0 31.6 31.2 31.0  
 58.1 59.0 59.9 60.8 61.8 62.7 63.6 64.5 65.4 66.3 67.3 68.2 69.1 70.1 71.0 71.9 72.9 73.8

46 37.9 37.0 36.2 35.3 34.4 33.6 32.7 31.9 31.0 30.2 29.4 28.6 27.8 27.1 26.3 25.6 24.9 24.3  
 56.5 57.4 58.4 59.3 60.3 61.2 62.2 63.2 64.1 65.1 66.0 67.0 68.0 68.9 69.9 70.8 71.8 72.8

45 35.0 34.0 33.0 32.0 31.0 30.0 29.0 28.0 27.0 26.0 25.0 24.0 23.0 22.0 21.0 20.0 19.0 18.0  
 55.0 56.0 57.0 58.0 59.0 60.0 61.0 62.0 63.0 64.0 65.0 66.0 67.0 68.0 69.0 70.0 71.0 72.0

44 32.2 31.1 30.0 28.9 27.7 26.6 25.5 24.3 23.2 22.0 20.8 19.6 18.4 17.1 15.9 14.6 13.3 11.9  
 53.7 54.7 55.8 56.8 57.5 58.9 60.0 61.0 62.1 63.1 64.2 65.2 66.2 67.3 68.3 69.4 70.4 71.5

43 29.5 28.3 27.1 25.9 24.6 23.3 22.1 20.8 19.4 18.1 16.7 15.3 13.9 12.4 10.9 9.5 7.7 6.0  
 52.5 53.5 54.7 55.8 56.9 58.0 59.1 60.2 61.3 62.4 63.5 64.6 65.7 66.8 67.9 69.0 70.0 71.1

42 27.0 25.7 24.5 23.0 21.6 20.2 18.8 17.3 15.8 14.3 12.7 11.1 9.5 7.8 6.0 4.2 2.2 .2  
 51.4 52.5 53.7 54.9 56.0 57.2 58.3 59.5 60.6 61.8 62.9 64.1 65.2 66.4 67.6 68.7 69.9 71.0

55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72

PSI

FIRST LINE, ALPHA, ANGLE TO N-S LINE FROM HORIZONTAL  
 SECOND LINE, ALPHA, ANGLE TO E-W LINE FROM HORIZONTAL

41	24.5	23.1	21.6	20.1	18.6	17.1	15.5	13.9	12.3	10.6	8.8	7.0	5.2	3.2	1.2	-1.0	-3.3	-5.7
	50.4	51.6	52.9	54.1	55.3	56.5	57.7	58.9	60.1	61.4	62.6	63.8	65.0	66.2	67.4	68.7	69.9	71.1
40	22.1	20.6	19.0	17.4	15.8	14.1	12.4	10.6	8.8	6.9	5.0	2.9	.8	-1.4	-3.7	-6.2	-8.8	-11.7
	49.5	50.6	52.1	53.4	54.7	55.9	57.2	58.5	59.8	61.0	62.3	63.6	64.9	66.2	67.5	68.8	70.1	71.4
39	19.7	18.1	16.4	14.7	12.9	11.1	9.2	7.3	5.3	3.2	1.1	-1.2	-3.5	-6.0	-8.7	-11.5	-14.5	-17.6
	48.8	50.1	51.5	52.8	54.1	55.5	56.8	58.2	59.5	60.9	62.2	63.6	64.9	66.3	67.7	69.1	70.5	72.0
38	17.4	15.7	15.6	12.0	10.1	8.1	6.1	4.0	1.8	-.4	-2.8	-5.3	-7.9	-10.7	-13.7	-16.9	-20.4	-24.3
	48.1	49.5	50.9	52.3	53.7	55.1	56.6	58.0	59.4	60.8	62.2	63.7	65.1	66.6	68.1	69.6	71.2	72.8
37	15.1	13.3	11.3	9.3	7.3	5.2	3.0	.7	-1.7	-4.2	-6.8	-9.5	-12.4	-15.6	-18.9	-22.6	-26.7	-31.2
	47.5	49.0	50.4	51.9	53.4	54.9	56.4	57.9	59.4	60.9	62.4	64.0	65.5	67.1	68.7	70.4	72.1	73.9
36	12.9	10.9	8.8	6.7	4.5	2.2	-.2	-2.6	-5.2	-7.9	-10.8	-13.8	-17.1	-20.6	-24.4	-28.6	-33.4	-38.8
	47.0	48.5	50.1	51.6	53.2	54.8	56.3	57.9	59.5	61.1	62.7	64.4	66.1	67.8	69.5	71.4	73.3	75.3
35	10.6	8.5	6.3	4.0	1.7	-.8	-3.3	-6.0	-8.8	-11.8	-14.9	-18.3	-21.9	-25.9	-30.3	-35.2	-40.8	-47.4
	46.5	48.2	49.8	51.4	53.1	54.7	56.4	58.1	59.8	61.5	63.2	65.0	66.8	68.7	70.6	72.7	74.9	77.3
34	8.4	6.1	3.8	1.3	-1.2	-3.8	-6.6	-9.5	-12.5	-15.8	-19.2	-23.0	-27.0	-31.5	-36.6	-42.4	-49.3	-58.1
	46.2	47.9	49.6	51.3	53.1	54.8	56.6	58.4	60.2	62.0	63.9	65.8	67.8	69.9	72.0	74.4	77.0	80.1
33	6.1	3.7	1.2	-1.4	-4.1	-6.9	-9.9	-13.0	-16.4	-19.9	-23.7	-27.9	-32.5	-37.7	-43.7	-50.8	-60.0	-74.6
	45.9	47.7	49.5	51.3	53.2	55.0	56.9	58.8	60.7	62.7	64.7	66.8	69.0	71.4	73.9	76.7	80.1	85.1
32	3.9	1.3	-1.4	-4.1	-7.1	-10.1	-13.3	-16.7	-20.4	-24.3	-28.5	-33.2	-38.5	-44.6	-52.0	-61.5	-77.7	
	45.7	47.6	49.5	51.4	53.4	55.4	57.4	59.4	61.5	63.6	65.8	68.1	70.6	73.3	76.3	80.0	85.8	
31	1.6	-1.2	-4.0	-7.0	-10.1	-13.4	-16.9	-20.6	-24.6	-28.9	-33.7	-39.1	-45.3	-52.7	-62.5	-80.2		
	45.6	47.6	49.6	51.7	53.7	55.8	58.0	60.1	62.4	64.7	67.2	69.8	72.6	75.8	79.8	86.4		
30	-.8	-3.7	-6.7	-9.9	-13.2	-16.8	-20.6	-24.6	-29.0	-33.9	-39.4	-45.6	-53.2	-63.2	-82.0			
	45.6	47.7	49.8	52.0	54.2	56.4	58.7	61.1	63.5	66.1	68.9	71.9	75.3	79.5	86.9			
29	-3.1	-6.2	-9.5	-12.9	-16.5	-20.3	-24.5	-29.0	-33.9	-39.4	-45.7	-53.4	-63.4	-82.9				
	45.6	47.9	50.2	52.5	54.8	57.2	59.7	62.3	65.0	67.9	71.0	74.6	79.1	87.1				
28	-5.6	-8.9	-12.4	-16.0	-19.9	-24.1	-28.7	-33.6	-39.2	-45.6	-53.2	-63.3	-82.5					
	45.8	48.2	50.6	53.1	55.6	58.2	60.9	63.7	66.7	70.0	73.8	78.5	86.8					

GAMMA

PSI



FIRST LINE, ALPHA1, ANGLE TO N-S LINE FROM HORIZONTAL  
 SECOND LINE, ALPHA2, ANGLE TO E-W LINE FROM HORIZONTAL

27	-8.1	-11.6	-15.4	-19.3	-23.6	-28.1	-33.2	-38.8	-45.2	-52.8	-62.8	-81.1
	46.1	48.7	51.2	53.9	56.6	59.4	62.4	65.5	69.0	72.9	77.7	86.1
26	-10.7	-14.5	-18.5	-22.8	-27.4	-32.5	-38.1	-44.6	-52.2	-62.1	-79.2	
	46.5	49.2	52.0	54.8	57.8	60.9	64.2	67.7	71.8	76.8	85.0	
25	-13.5	-17.5	-21.9	-26.6	-31.6	-37.3	-43.7	-51.3	-61.0	-76.9		
	47.1	50.0	52.9	56.0	59.2	62.7	66.4	70.6	75.7	83.7		
24	-16.4	-20.7	-25.5	-30.6	-36.3	-42.7	-50.2	-59.7	-74.5			
	47.8	50.9	54.1	57.5	61.0	64.9	69.2	74.4	82.2			
23	-19.4	-24.2	-29.3	-35.0	-41.4	-48.9	-58.2	-72.0				
	48.7	52.0	55.5	59.2	63.2	67.7	73.0	80.5				
22	-22.7	-27.9	-33.6	-40.0	-47.4	-56.5	-69.4					
	49.8	53.4	57.3	61.4	66.0	71.4	78.7					
21	-26.2	-32.0	-38.3	-45.7	-54.6	-66.7						
	51.1	55.1	59.4	64.1	69.6	76.8						
20	-30.1	-36.5	-43.8	-52.5	-64.0							
	52.7	57.2	62.0	67.6	74.7							
19	-34.5	-41.7	-50.2	-61.2	-81.6							
	54.7	59.7	65.4	72.5	85.0							
18	-39.4	-47.8	-58.3	-75.1								
	57.2	63.0	70.1	80.8								
17	-45.1	-55.3	-70.2									
	60.4	67.4	77.3									
16	-52.2	-65.7										
	64.6	73.9										
15	-61.5											
	70.5											
14	-78.1											
	81.7											

GAMMA

PSI



FIRST LINE, ALPHA1, ANGLE TO N-S LINE FROM HCRIZCENTAL  
 SECOND LINE, ALPHA2, ANGLE TO E-W LINE FROM HORIZCENTAL

41 -8.3 -11.1 -14.2 -17.6 -21.5 -25.9 -31.1 -37.6 -45.9 -58.2  
 72.4 73.7 74.9 76.3 77.6 79.0 80.4 82.0 83.7 85.8

40 -14.8 -18.1 -21.9 -26.1 -31.0 -36.9 -44.2 -53.9 -70.2  
 72.8 74.2 75.6 77.1 78.6 80.2 82.0 84.0 86.9

39 -21.5 -25.5 -30.1 -35.4 -41.8 -50.0 -61.4  
 73.5 75.0 76.6 78.3 80.1 82.1 84.7

38 -28.6 -33.5 -39.2 -46.1 -55.1 -68.9  
 74.4 76.2 78.0 80.1 82.4 85.6

37 -36.4 -42.4 -49.9 -59.8 -77.5  
 75.7 77.8 80.1 82.8 87.1

36 -45.1 -53.1 -64.0  
 77.5 80.1 83.3

35 -55.8 -67.9  
 80.1 83.8

34 -71.5  
 84.4

GAMMA 33

32

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KANSAS GEOLOGICAL SURVEY COMPUTER PROGRAM  
THE UNIVERSITY OF KANSAS, LAWRENCE

PROGRAM ABSTRACT

Title (If subroutine state in title):

FORTRAN IV CDC 6400 computer program for constructing isometric diagrams.

Date: 29 August 1969

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Name: Address:

Purpose/description: Subroutines to provide a method of displaying a surface in isometric pictorial representation.

Mathematical method: Point translation from  $(x, y, z)$  space to  $(u, v)$  space.

Restrictions, range: No restrictions except disc or other fast-access storage unit capacity.

Computer manufacturer: CDC Model: 6400

Programming language: FORTRAN IV

Memory required: \* K Approximate running time: variable; linear with number of points defining surface.

Special peripheral equipment required: digital plotter

Remarks (special compilers or operating systems, required word lengths, number of successful runs, other machine versions, additional information useful for operation or modification of program)

Run successfully many times.

\* 7K + work array + user general plotter routines (see text)





(continued from inside front cover)

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