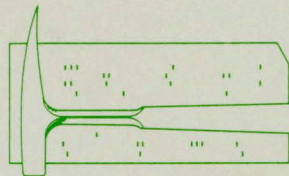


**COMPUTER PROGRAMS FOR
MULTIVARIATE ANALYSIS
IN GEOLOGY**

Edited by

DANIEL F. MERRIAM



COMPUTER CONTRIBUTION 20

State Geological Survey

The University of Kansas, Lawrence

1968

EDITORIAL STAFF

Daniel F. Merriam, Editor

Assistant Editors

John C. Davis Owen T. Spitz

Associate Editors

John R. Dempsey
Richard W. Fetzner
James M. Forgotson, Jr.
John C. Griffiths
John W. Harbaugh

R.G. Hetherington
Sidney N. Hockens
J. Edward Klovans
William C. Krumbein
R.H. Lippert

William C. Pearn
Max G. Pitcher
Floyd W. Preston
Walther Schwarzacher
Peter H.A. Sneath

Editor's Remarks

The following quote is reproduced with permission from the Stanford Research Institute Journal (no. 17 November, 1967, p. 13). We believe it is of considerable interest to all users of the COMPUTER CONTRIBUTION series.

The U.S. market for computer systems is expected to grow from about \$2 billion in 1965 to about \$5.2 billion by 1975, representing nearly 0.5 percent of the total gross national product. With programming, operating, and support costs, it seems reasonable to predict that at least 1 percent of the nation's efforts will be devoted to computer activity by 1975.

Third generation computers will continue to be marketed into the early 1970's; the major advance during this period will be in applications and systems use. The single most dramatic development will be the widespread adoption of communications in conjunction with computers. Dedicated systems (i.e., within a company or organization) for on-line and real-time operations will replace many of the present batch systems. Systems design and implementation will become quite advanced. Time-sharing, on-line systems also will be developed but will continue to be a relatively small factor until 1972.

Fourth generation computers featuring large-scale integrated circuits (LSI) are expected to be available in 1972. Their design will facilitate further expansion of the time-sharing philosophy, utilizing large data bases for the concurrent operation of many dissimilar applications. This will expand the use of computers to a number of applications that previously could not support computers. By 1975, time-sharing should encompass such areas as management information systems, computer-aided instruction, hospital-patient monitoring, and others. Today such time-sharing is being used in the laboratory or experimentally.

As a result of the effect of communications and time-sharing, the terminal unit will become the most important single segment of the computer peripheral market.

Total systems are unlikely to become a reality by 1975. However, many discrete systems will be combined in time-sharing. This certainly will be an important step toward the total system concept. It is doubtful that a total system with all applications integrated will become a practical reality except in a few special cases--at least not in the foreseeable future.

The use of computers in specific industries will remain essentially unchanged, with government and commerce being the big users. Any organization that uses extensive communications in the clerical conduct of its business will expand its data processing needs in the next few years. Banks, department stores, government agencies, widespread manufacturers, and distributors will expand and maintain their present leadership in computer use.

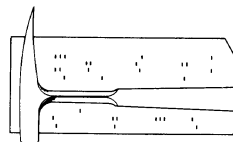
The universities will continue to provide leadership in new applications and innovations of computer use, as well as becoming one of the big users of computers.

An up-to-date list of other COMPUTER CONTRIBUTIONS and related publications may be obtained by writing the Editor, COMPUTER CONTRIBUTION Series, Kansas Geological Survey, The University of Kansas, Lawrence, Kansas 66044.

**COMPUTER PROGRAMS FOR MULTIVARIATE ANALYSIS
IN GEOLOGY**

Edited by

DANIEL F. MERRIAM



1968

CONTENTS

	Page
FORTTRAN IV program for multivariate paleontologic analysis using an IBM System/360 Model 40 computer, by J.A. Wolleben, R.J. Pauken, and J.A. Dearien.	1
R-mode factor analysis program in FORTRAN II for the IBM 1620 computer, by R.J. Sampson	13
Q-mode factor analysis program in FORTRAN IV for small computers, by J.E. Klovan	38
FORTTRAN II program for the calculation of Wilks' Λ using an IBM 1620 computer, by S.V.L.N. Rao	51

FORTRAN IV PROGRAM FOR MULTIVARIATE PALEONTOLOGIC ANALYSIS USING AN IBM SYSTEM/360 MODEL 40 COMPUTER

by

J. A. Wolleben, R. J. Pauken, and J. A. Dearien
University of Missouri

INTRODUCTION

Paleontologists, in attempting to make comparisons between sample sets based on large numbers of variables, are confronted with the problem of working with these variables simultaneously in order to obtain the most meaningful results. If the variables can be quantified then the computer program described in this paper can be used to aid in making paleontologic decisions.

A population described by p variables may be pictured as a cluster of sample points in p -dimensional space. The distribution of these points is specified by the mean vector and covariance matrix of the sample. Equality of sample covariance matrices is a specific characteristic that is of primary concern. R. A. Reyment has used homogeneity and heterogeneity of covariance matrices as an aid in the interpretation of evolutionary changes in ostracodes and physical sorting of fossil samples. The degree of distinctness of several samples can be measured by the "generalized distance" between the multivariate means of the samples. This is referred to as Mahalanobis' D^2 and has been used by Reyment (1960a, 1960b, 1962a, 1962b, 1963), Giles (1960), and Lerman (1965) as an aid in the interpretation of evolutionary changes of different fossil groups. The linear discriminant function also has been used by Reyment (1962b) to classify an unknown sample as belonging to one of several groups.

The computer program described here provides the following:

- (a) sums of squares and cross-products matrices and mean vectors for each sample,
- (b) the necessary values for a homogeneity test of covariance matrices,
- (c) generalized distance (D^2) values and F values for determining the significance of the distances, and
- (d) the constant terms of the linear discriminant function and the discriminant index for the classification of an unknown into one of several populations.

The program differs from previously described programs in several ways. A basic requirement for most multivariate methods including D^2 and discriminant function analysis is that the covariance matrices

be homogeneous. This program computes the necessary values for a homogeneity test of covariance matrices. In addition the program makes generalized distance comparisons and provides discriminant functions for q -sample sets. Previously described programs such as Davis and Sampson (1966) compared only two sample sets at a time. In taxonomic and biostratigraphic analysis the former approach is much more applicable than the latter.

MATHEMATICAL DEVELOPMENT

A more detailed mathematical development of each technique can be found in Anderson (1958). In the following discussion, matrices and vectors are denoted by boldface characters.

The mean vector $\bar{\mathbf{X}}$ is a vector composed of the arithmetic means of two or more different variables in a sample. The covariance matrix \mathbf{S} is derived from the matrix of the sums of squares and cross products \mathbf{A} . The sample covariance matrix is given by

$$\mathbf{S} = \frac{1}{N-1} \mathbf{A}. \quad (1)$$

The test for homogeneity of covariance matrices is a generalization of the Bartlett test for homogeneity of variance in the univariate case and is developed by Anderson (1958). In the multivariate case the homogeneity of covariance is tested by

$$W_1 = V_1 \cdot \frac{n^{\frac{1}{2}pn}}{\prod_{g=1}^q n_g^{\frac{1}{2}pn_g}}, \quad (2)$$

where V_1 is defined by

$$V_1 = \frac{\prod_{g=1}^q |\mathbf{A}_g|^{\frac{1}{2}n_g}}{|\mathbf{A}|^{\frac{1}{2}n}} \quad (3)$$

and $n_g = N_g - 1$, $n = \sum n_g = N - q$, where q is the number of sample sets and p is the number of variables. The significance is found by calculating $-\log_e W_1$, and then using the asymptotic expansion

of $-\rho \log_e W_1$, where ρ is defined as

$$\rho = 1 - \left(\sum \frac{1}{n_g} - \frac{1}{n} \right) \frac{2p^2 + 3p - 1}{6(p+1)(q-1)}, \quad (4)$$

and

$$W_2 = \frac{p(p+1) [(p-1)(p+2) \left(\sum \frac{1}{n_g} - \frac{1}{n} \right) - 6(q-1)(1-\rho^2)]}{48\rho^2}. \quad (5)$$

Thus

$$\Pr \left\{ -2\rho \log_e W_1 \leq z \right\} = \Pr \left\{ \chi_f^2 \leq z \right\} + w_2 \left[\Pr \left\{ \chi_{f+4}^2 \leq z \right\} - \Pr \left\{ \chi_f^2 \leq z \right\} \right] + O(n^{-3}) \quad (6)$$

and the number of degrees of freedom, f , is $\frac{(q-1)p(p+1)}{2}$ (Anderson, 1958). This test takes account of the relative degree of scatter but not orientation heterogeneity.

The generalized statistical distance between populations i and j as defined by Mahalanobis is:

$$D^2 = (\bar{\mathbf{X}}_i - \bar{\mathbf{X}}_j)' \mathbf{S}^{-1} (\bar{\mathbf{X}}_i - \bar{\mathbf{X}}_j), \quad (7)$$

where $\bar{\mathbf{X}}_i$ and $\bar{\mathbf{X}}_j$ are the respective sample mean vec-

tors and $\mathbf{S}^{-1} = \left[\frac{1}{q} (\mathbf{S}_1 + \mathbf{S}_2 + \dots + \mathbf{S}_q) \right]^{-1}$, the pooled inverse covariance matrix of all samples. Significance of the difference between multivariate means is tested by the variance ratio

$$F = \frac{(N_1 N_2) (N_1 + N_2 - p - 1)}{p(N_1 + N_2) (N_1 + N_2 - 2)} D^2 \quad (8)$$

with p and $(N_1 + N_2 - p - 1)$ degrees of freedom.

The linear discriminant function coefficients for three or more samples are found by the equation

$$\lambda'_{ij} = \mathbf{S}^{-1} (\bar{\mathbf{X}}_i - \bar{\mathbf{X}}_j). \quad (9)$$

The discriminant index is found by the equation

$$R_{ij} = -\frac{1}{2} (\bar{\mathbf{X}}_i + \bar{\mathbf{X}}_j)' \mathbf{S}^{-1} (\bar{\mathbf{X}}_i - \bar{\mathbf{X}}_j). \quad (10)$$

From equations 9 and 10 we obtain the discriminant function $\mu_{ij} = \lambda'_{ij} \bar{\mathbf{X}}_i + R_{ij}$, (11)

also $\mu_{ji} = -\mu_{ij}$. If there are equal a priori probabilities, the best set of regions of classification are

$$R_1 : \mu_{12} \geq 0; \mu_{13} \geq 0; \mu_{1m} \geq 0$$

$$R_2 : \mu_{21} \geq 0; \mu_{23} \geq 0; \mu_{2m} \geq 0$$

\vdots

\vdots

$$R_m : \mu_{m1} \geq 0; \mu_{m2} \geq 0; \mu_{mm} \geq 0.$$

This method divides the variable space into m regions of classification; an unknown is placed into one of these regions by applying the discriminant function.

PROGRAM DESCRIPTION

This program computes mean vectors and sum of squares and cross-products matrices for 20 sample sets, using up to 15 variables, and having up to 99 samples in each set. The determinants of each matrix are computed using a pivotal condensation method described by McCormick and Salvadori (1964) and become terms in the W_1 equation for determining heterogeneity of covariance matrices. Sums of squares and cross products are accumulated and used to obtain the pooled variance - covariance matrix of all the samples. The pooled covariance matrix is inverted and the inverted matrix used in the solution of the D^2 equations and the linear discriminant function equations.

Output from the program consists of determinants of each sums of squares and cross-products matrix and the determinant of the pooled sums of squares and cross-products matrix; V_1 , W_1 , ρ , W_2 , and $-\rho \log_e W_1$ values and degrees of freedom for testing homogeneity of covariance matrices; mean vectors of each sample; pooled variance - covariance matrix; inverted variance - covariance matrix; Mahalanobis' generalized distance (D^2) values, F -values, and degrees of freedom for all sample comparisons; constant terms of the linear discriminant functions; and the discriminant indices.

The program was written to run on an IBM System/360 Model 40 computer with 65K bits of core storage, automatic divide, and indirect addressing. Minor alterations make possible the use of this program on an IBM 1620 computer.

Data are read into the program by the following procedure. The total number of sample sets to be considered and the number of variables measured on the sample sets are identified on the first data card. All samples must have the same number of variables.

Card 1. This card contains two two-digit numbers in the first four columns. These must be right justified in columns 2 and 4. The first number (columns 1 and 2) is the number of sample sets to be read-in. The second number is the number of variables

and also the horizontal dimension of the input matrix.

Cards 2 and 3 supply information to the program about each sample. Therefore, each set of sample data cards will be preceded by these two cards each with information about that set.

Card 2. This card contains a two-digit number in the first two columns and is right justified. This number identifies that set as being group 1, 2, 3, or 20.

Card 3. This card also contains a two-digit number in the first two columns that is right justified. This digit, the number of specimens measured for that sample, is the vertical dimension of the input matrix.

The data format, statement 6 in the program listing (6 FORMAT 8F 10.0), may be adjusted by the programmer. If the format is unaltered the data are punched continuously in 10-digit fields, one row of the input matrix at a time from left to right. If, for example, the matrices were formed by measuring six variables the format would read (6 FORMAT 6F 10.0), again each number being placed in a 10-digit field.

All possible comparisons are punched in a triangular output matrix. Rows of the matrix as well

as the specific comparisons are identified as they are punched.

The program has been tested using data published by various authors. The covariance matrix homogeneity test values were obtained from data given by Anderson (1958, p. 256) and correspond with the values obtained by Anderson. D^2 values were obtained from data given by Lerman (1965, p. 427) and correspond with his D^2 values. The discriminant function portion of the program was tested using data published by Reyment (1962b, p. 198, 199) and Miller and Kahn (1962, p. 265, 266, 281).

The length of time required to complete the program depends upon the number of samples, sample sets and variables used. Approximately 2 1/4 minutes are required for compiling and execution of an analysis of 17 sample sets with 13 variables and 20 samples per set.

The program was written by the authors at the University of Missouri as a part of a quantitative paleontology project. Machine time was donated by the University of Missouri Computer Center.

REFERENCES

- Anderson, T. W., 1958, An introduction to multivariate statistical analysis: John Wiley & Sons, New York, 374 p.
- Davis, J. C., and Sampson, R. J., 1966, FORTRAN II program for multivariate discriminant analysis using an IBM 1620 computer: Kansas Geol. Survey Computer Contr. 4, 8 p.
- Giles, E., 1960, Multivariate analysis of Pleistocene and Recent coyotes (Canis latrans) from California: Univ. California Publ. Geol. Sci., v. 36, no. 8, p. 369-390.
- Lerman, A., 1965, Evolution of Exogyra in the Late Cretaceous of the southeastern United States: Jour. Paleontology, v. 39, no. 3, p. 414-435.
- McCormick, J. M., and Salvadori, M. G., 1964, Numerical methods in FORTRAN: Prentice-Hall, Englewood Cliffs, New Jersey, 324 p.
- Miller, R. L., and Kahn, J. S., 1962, Statistical analysis in the geological sciences: John Wiley & Sons, New York, 483 p.
- Reyment, R. A., 1960a, Notes on the study of evolutionary changes in ostracods: 21st Intern. Geol. Congr. Rep., Copenhagen, sec. 6, p. 7-17.
- Reyment, R. A., 1960b, Studies on Nigerian Upper Cretaceous and lower Tertiary Ostracoda, pt. 1: Stockholm Contr. Geol., v. 7, 238 p.
- Reyment, R. A., 1962a, Observations on homogeneity of covariance matrices in paleontologic biometry: Biometrics, v. 18, p. 1-11.
- Reyment, R. A., 1962b, Biometric study of Actinocamax verus s.l. from the Upper Cretaceous of the Russian Platform: Stockholm Contr. Geol., v. 9, p. 147-206.
- Reyment, R. A., 1963, Studies on Nigerian Upper Cretaceous and Lower Tertiary Ostracoda, pt. 2: Stockholm Contr. Geol., v. 10, 286 p.

```

/WATFOR          000,TIME=5
C *****
C   MULTIVARIATE PALEONTOLOGIC ANALYSIS OF UP TO 20 SAMPLE SETS
C   USING UP TO 15 VARIABLES AND 99 SAMPLES PER SET
C   VALUES FOR TEST OF VARIANCE-COVARIANCE HOMOGENIETY, GENERALIZED
C   DISTANCE, AN F-VALUE FOR A TEST OF EQUALITY OF MULTIVARIATE
C   MEANS, AND DISCRIMINANT EQUATIONS ARE COMPUTED
C   COMPUTER= IBM 360-40
C   LANGUAGE= FORTRAN IV
C *****
C   JAMES A. WOLLEBEN, ROBERT J. PAUKEN, AND JOHN A. DEARIEN
C   UNIVERSITY OF MISSOURI GEOLOGY DEPARTMENT 5-17-67
C *****
C   THE FIRST DATA CARD CONTAINS TWO NUMBERS OF TWO DIGITS EACH
C   THESE NUMBERS GO IN THE FIRST FOUR COLUMNS, RIGHT JUSTIFIED
C   THE FIRST NUMBER IS THE NUMBER OF SAMPLES
C   THE SECOND NUMBER IS THE NUMBER OF VARIABLES
C *****
      DIMENSION XA(15,99),XB(15,15),XC(15,15),XVS(20,15),XV(15),R(20)
      DIMENSION VM(15),DMV(15),XVCVI(15),DISC(15),KM(20)
      DIMENSION SMV(15),A(15,15),DS(20),CC(20)
616  READ (5,1) N1,M
      1  FORMAT (I2,I2)
      DO 22 I=1,M
      DO 22 K=1,M
      22  XC(I,K)=0.0
      DF=0.0
      M2=0
      M3=0
      M4=0
      WRITE (6,619)
619  FORMAT (/ ,25X,19HRESULTS OF ANALYSIS,/)
      WRITE (6,55)
      55  FORMAT(2X,69HDETERMINANTS AND SUMS OF SQUARES AND CROSS PRODUCTS O
      1F INPUT MATRICES,/)
      NUB=0
2222 CONTINUE
      JL=NUB+1
C *****
C   TWO TWO-DIGIT CONTROL CARDS GO IN FRONT OF EACH SAMPLE
C   THE FIRST CARD HAS A NUMBER SPECIFYING THE GROUP NAME
C   IN THE FIRST TWO COLUMNS, RIGHT JUSTIFIED
C   THE SECOND CARD HAS THE NUMBER OF SPECIMENS FOR THAT SAMPLE
C   IN THE FIRST TWO COLUMNS, RIGHT JUSTIFIED
C *****
      READ (5,2) N6
      READ (5,2) N5
      2  FORMAT (I2)
      KM(JL)=N6
      DO 3 J=1,N5
      3  READ (5,6) (XA(I,J),I=1,M)
C *****
C   THE FOLLOWING FORMAT SHOULD BE CHANGED TO FIT THE
C   NUMBER OF VARIABLES IN THE INPUT MATRIX
C *****
      6  FORMAT (4F8.0)
      R(JL)=N5
      DF=DF+R(JL)
      SN=N1
      AN=N5

```



```

DO 7 I=1,M
SUM=0.0
DO 8 J=1,N5
8 SUM=SUM+XA(I,J)
7 XV(I)=SUM/AN
DO 511 I=1,M
DO 511 K=1,M
SUM=0.0
DO 9 J=1,N5
9 SUM=SUM+(XA(I,J)-XV(I))*(XA(K,J)-XV(K))
XB(I,K)=SUM
511 CONTINUE
515 WRITE (6,525) JL
525 FORMAT(2X,47HSUMS OF SQUARES AND CROSS PRODUCTS MATRIX GROUP,I2,/)
DO 517 I=1,M
517 WRITE (6,13) (XB(I,K),K=1,M)
GO TO 34
36 CONTINUE
DO 37 K=1,M
DO 37 J=1,M
37 A(K,J)=XC(K,J)
34 M4=M4+1
IF (N1-M4) 61,60,60
60 DO 99 K=1,M
DO 99 J=1,M
99 A(K,J)=XB(K,J)
61 N=M
K=2
L=1
5 DO 10 I=K,N
IF(A(L,L)) 385,386,385
385 RATIO=A(I,L)/A(L,L)
DO 10 J=K,N
10 A(I,J)=A(I,J)-A(L,J)* RATIO
IF(K=N) 15,20,20
15 L=K
K=K+1
GO TO 5
20 DETERM=1
DO 25 L=1,N
25 DETERM=DETERM*A(L,L)
IF (N1-M4) 41,38,38
38 WRITE (6,35) JL,DETERM
35 FORMAT(2X,17HDETERMINANT GROUP,I2,2X,2HIS,E16.8,/)
DS(JL)=DETERM
DO 11 I=1,M
DO 11 K=1,M
XVS(JL,I)=XV(I)
11 XC(I,K)=XC(I,K)+XB(I,K)
NUB=NUB+1
IF (NUB-N1)2222,48,48
48 CONTINUE
GO TO 389
386 WRITE (6,387)
387 FORMAT(2X,49HTHE DETERMINANT OF THIS SAMPLE IS ZERO, JOB ENDED)
GO TO 616
389 DF1=DF-SN
IF (N1-M4) 41,36,41
41 SDET=DETERM
WRITE (6,42) SDET

```

```

42 FORMAT(2X,28HDETERMINANT OF POOLED MATRIX,E16.8,/)
WRITE (6,618)
618 FORMAT(2X,27HVALUES FOR HOMOGENIETY TEST,/)
HT=0.0
DO 43 I=1,N1
CC(I)={(R(I)-1.0)*0.5}*ALOG(ABS(DS(I)))
43 HT=HT+CC(I)
HOT=HT-(0.5*DF1)*ALOG(ABS(SDET))
RP=M
HH=0.0
DO 304 I=1,N1
304 HH=HH+(0.5*RP*(R(I)-1.0))*ALOG(R(I)-1.0)
GG=(0.5*RP*DF1)*ALOG(DF1)-HH+HOT
WRITE (6,305) GG
305 FORMAT(2X,14HLOG W-ONE IS ,E16.8)
SS=0.0
DO 306 I=1,N1
306 SS=SS+(1.0/(R(I)-1.0))
XW=SS-(1.0/DF1)
RO=1.0-XW*((2.0*(RP**2.0))+((3.0*RP)-1.0))/(6.0*(RP+1.0)*(SN-1.0))
WRITE (6,307) RO
307 FORMAT(2X,10HRHO IS ,E16.8)
RR=0.0
DO 308 I=1,N1
308 RR=RR+(1.0/((R(I)-1.0)**2.0))
RW=(RR-(1.0/(DF1*DF1)))*(RP-1.0)*(RP+2.0)
WW=RW-(6.0*(SN-1.0)*(1.0-RO)**2.0)
QW=(WW*RP*(RP+1.0))/(48.0*RO*RO)
WRITE (6,309) QW
309 FORMAT(2X,10HW-TWO IS ,E16.8)
RLW1=RO*GG
WRITE (6,310) RLW1
310 FORMAT(2X,15HRHO LOG W1 IS ,E16.8)
DEG=((SN-1.0)*RP*(RP+1.0))/2.0
WRITE (6,311) DEG
311 FORMAT(2X,20HDEGREES OF FREEDOM ,F5.0,/)
WRITE (6,57)
57 FORMAT(2X,30HMEAN VECTORS OF INPUT MATRICES,/)
DO 18 L=1,N1
WRITE (6,17) L
17 FORMAT(2X,17HMEAN VECTOR GROUP,I2)
18 WRITE (6,13) (XVS(L,I),I=1,M)
13 FORMAT (13F9.3)
DO 28 I=1,M
DO 28 K=1,M
28 XC(I,K)=(XC(I,K))/(DF-SN)
WRITE (6,14)
14 FORMAT (//,2X,24HPOOLED COVARIANCE MATRIX,/)
DO 16 I=1,M
16 WRITE (6,13) (XC(I,K),K=1,M)
DO 26 I=1,M
Y=XC(I,I)
XC(I,I)=1.00
DO 23 J=1,M
23 XC(I,J)=XC(I,J)/Y
DO 26 K=1,M
IF (K-I)24,26,24
24 Y=XC(K,I)
XC(K,I)=0.0
DO 27 J=1,M

```

```

27 XC(K,J)=XC(K,J)-Y*XC(I,J)
26 CONTINUE
WRITE (6,83)
83 FORMAT (//,2X,33HINVERTED POOLED COVARIANCE MATRIX,/)
DO 31 I=1,M
31 WRITE (6,13) (XC(I,J),J=1,M)
N3=N1
69 M3=M3+1
WRITE (6,77) M3
77 FORMAT (//,2X,3HROW,1X,12,1X,16HOF OUTPUT MATRIX,/)
LL=M3
N2=N1-1
N3=N3-1
M2=M2+1
KK=M2
ID1=KM(KK)
DO 68 K=1,N3
LL=LL+1
ID2=KM(LL)
DO 44 I=1,M
44 VM(I)=XVS(LL,I)
DO 51 I=1,M
J=M2
51 DMV(I)=XVS(J,I)-VM(I)
DO 73 I=1,M
J=M2
73 SMV(I)=(VM(I)+XVS(J,I))/2.00
DO 54 J=1,M
SUM =0.0
DO 19 I=1,M
19 SUM=SUM+DMV(I)*XC(I,J)
54 XVCVI(J)=SUM
SUM=0.0
J=M2
X1=R(J)
X2=R(LL)
DOD=(X1+X2-1.0-RP)
WRITE (6,151) ID1,ID2
151 FORMAT (2X,6HGROUP ,12,1X,20HCOMPARED WITH GROUP ,12)
DO 32 J=1,M
32 SUM=SUM+XVCVI(J)*DMV(J)
DSQ=SUM
WRITE (6,617)
617 FORMAT (/)
WRITE (6,56) DSQ
56 FORMAT(2X,14HD-SQUARED IS ,E16.8)
D=SQRT(ABS(DSQ))
DO 59 I=1,M
SUM=0.0
DO 58 J=1,M
58 SUM=SUM+XC(I,J)*DMV(J)
59 DISC(I)=SUM
SUM=0.0
DO 79 I=1,M
79 SUM=SUM+SMV(I)*DISC(I)
XINDX=SUM
EPH=((X1*X2)*(X1+X2-RP-1.0))/((RP*(X1+X2))*(X1+X2-2.0))* DSQ
WRITE (6,97) EPH
97 FORMAT(2X,14HTHE F VALUE IS,E16.8)
WRITE (6,98) RP,DOD

```

```

98 FORMAT(2X,23HF IS DISTRIBUTED WITH ,F5.0,2X,5HAND ,F5.0,2X,18HDE
1Grees OF FREEDOM)
WRITE (6,33)
33 FORMAT(2X,42HTHE DISCRIMINANT FUNCTION COEFFICIENTS ARE)
WRITE (6,13) (DISC(I),I=1,M)
WRITE (6,93) XINDX
93 FORMAT(2X,21HDISCRIMINANT INDEX IS,E16.8)
WRITE (6,617)
68 CONTINUE
IF (N2-M3)49,49,69
49 CONTINUE
WRITE (6,47)
47 FORMAT(2X,17HREAD IN MORE DATA)
GO TO 616
END

```

/DATA

0404 INPUT DATA- OREODONTS- MILLER AND KAHN (1962)

01 SUBDESMATOCHEERUS SP.

11

47.0	99.0	26.0	15.0
42.0	93.0	26.0	16.0
40.0	90.0	22.0	13.0
46.0	100.0	22.0	11.0
46.0	96.0	24.0	16.0
42.0	88.0	26.0	15.0
43.0	89.0	23.0	14.0
44.0	78.0	23.0	13.0
44.0	90.0	25.0	11.0
47.0	99.0	27.0	15.0
47.0	92.0	27.0	13.0

02 MEGOREODON GIGAS LOOMISI

11

78.0	165.0	35.0	18.0
77.0	165.0	37.0	19.0
65.0	148.0	30.0	20.0
74.0	163.0	31.0	15.0
65.0	169.0	31.0	16.0
70.0	176.0	34.0	23.0
69.0	161.0	28.0	13.0
67.0	178.0	31.0	14.0
65.0	174.0	34.0	18.0
64.0	168.0	28.0	13.0
68.0	166.0	32.0	15.0

03 O. OSBORNI

15

42.0	81.0	15.0	8.0
48.0	83.0	18.0	8.6
45.0	87.0	18.0	9.0
48.0	83.0	17.0	8.0
46.0	84.0	16.0	6.1
51.0	87.0	21.0	7.9
46.0	80.0	17.0	7.0
50.0	90.0	18.0	8.1
46.0	85.0	16.0	6.5

48.0	85.0	15.0	7.2
47.0	85.0	17.0	8.0
49.0	83.0	18.0	7.7
43.0	79.0	15.0	7.1
47.0	87.0	19.0	7.5
46.0	87.0	18.0	8.0

04 PSEUDODESMATOCHEERUS
08

60.0	114.0	27.0	20.0
60.0	118.0	31.0	19.0
60.0	111.0	31.0	21.0
58.0	102.0	30.0	20.0
55.0	116.0	28.0	20.0
59.0	117.0	29.0	17.0
59.0	114.0	24.0	17.0
60.0	121.0	25.0	19.0

/END

RESULTS OF ANALYSIS

DETERMINANTS AND SUMS OF SQUARES AND CROSS PRODUCTS OF INPUT MATRICES

SUMS OF SQUARES AND CROSS PRODUCTS MATRIX GROUP 1

58.545	82.272	18.454	-.272
82.272	407.636	30.727	18.363
18.454	30.727	36.545	15.272
-.272	18.363	15.272	31.636

DETERMINANT GROUP 1 IS .12073238E+08

SUMS OF SQUARES AND CROSS PRODUCTS MATRIX GROUP 2

248.181	-29.909	90.272	37.818
-29.909	676.545	64.636	-8.090
90.272	64.636	80.909	58.727
37.818	-8.090	58.727	100.181

DETERMINANT GROUP 2 IS .28057376E+09

SUMS OF SQUARES AND CROSS PRODUCTS MATRIX GROUP 3

80.400	57.200	37.600	4.039
57.200	125.600	39.800	9.820
37.600	39.800	38.400	7.860
4.039	9.820	7.860	8.157

DETERMINANT GROUP 3 IS .78431321E+06

SUMS OF SQUARES AND CROSS PRODUCTS MATRIX GROUP 4

20.875	12.125	.125	-1.875
12.125	230.874	-39.125	-22.125
.125	-39.125	48.875	12.875
-1.875	-22.125	12.875	14.875

DETERMINANT GROUP 4 IS .21030275E+07

DETERMINANT OF POOLED MATRIX .92238759E+10

VALUES FOR HOMOGENIETY TEST

LOG W-ONE IS -.34342310E+02
RHO IS .81371670E+00
W-TWO IS .11569229E+00
RHO LOG W1 IS -.27944911E+02
DEGREES OF FREEDOM 30.

MEAN VECTORS OF INPUT MATRICES

MEAN VECTOR GROUP 1
44.363 92.181 24.636 13.818
MEAN VECTOR GROUP 2
69.272 166.636 31.909 16.727
MEAN VECTOR GROUP 3
46.800 84.400 17.200 7.646
MEAN VECTOR GROUP 4
58.875 114.125 28.125 19.125

POOLED COVARIANCE MATRIX

9.951	2.968	3.572	.968
2.968	35.137	2.342	-.049
3.572	2.342	4.993	2.310
.968	-.049	2.310	3.776

INVERTED POOLED COVARIANCE MATRIX

.139	-.004	-.112	.033
-.004	.029	-.016	.011
-.112	-.016	.384	-.206
.033	.011	-.206	.382

ROW 1 OF OUTPUT MATRIX

GROUP 1 COMPARED WITH GROUP 2

D-SQUARED IS .20265159E+03
THE F VALUE IS .23684904E+03
F IS DISTRIBUTED WITH 4. AND 17. DEGREES OF FREEDOM
THE DISCRIMINANT FUNCTION COEFFICIENTS ARE
-2.428 -2.038 1.837 -1.298
DISCRIMINANT INDEX IS -.36960935E+03

GROUP 1 COMPARED WITH GROUP 3

D-SQUARED IS .21973263E+02
THE F VALUE IS .30503747E+02
F IS DISTRIBUTED WITH 4. AND 21. DEGREES OF FREEDOM
THE DISCRIMINANT FUNCTION COEFFICIENTS ARE
-1.004 .192 1.731 .834
DISCRIMINANT INDEX IS .16335360E+02

GROUP 1 COMPARED WITH GROUP 4

D-SQUARED IS .42713104E+02
THE F VALUE IS .40729523E+02
F IS DISTRIBUTED WITH 4. AND 14. DEGREES OF FREEDOM
THE DISCRIMINANT FUNCTION COEFFICIENTS ARE
-1.709 -.599 1.752 -2.046
DISCRIMINANT INDEX IS -.13758357E+03

ROW 2 OF OUTPUT MATRIX

GROUP 2 COMPARED WITH GROUP 3

D-SQUARED IS .23320833E+03
THE F VALUE IS .32374472E+03
F IS DISTRIBUTED WITH 4. AND 21. DEGREES OF FREEDOM
THE DISCRIMINANT FUNCTION COEFFICIENTS ARE
1.423 2.230 -.105 2.133
DISCRIMINANT INDEX IS .38594469E+03

GROUP 2 COMPARED WITH GROUP 4

D-SQUARED IS .84478001E+02
THE F VALUE IS .80554873E+02
F IS DISTRIBUTED WITH 4. AND 14. DEGREES OF FREEDOM
THE DISCRIMINANT FUNCTION COEFFICIENTS ARE
.719 1.438 -.085 -.748
DISCRIMINANT INDEX IS .23202580E+03

ROW 3 OF OUTPUT MATRIX

GROUP 3 COMPARED WITH GROUP 4

D-SQUARED IS .64892646E+02
THE F VALUE IS .72550782E+02
F IS DISTRIBUTED WITH 4. AND 18. DEGREES OF FREEDOM
THE DISCRIMINANT FUNCTION COEFFICIENTS ARE
-.704 -.791 .020 -2.881
DISCRIMINANT INDEX IS -.15391892E+03

READ IN MORE DATA

KANSAS GEOLOGICAL SURVEY COMPUTER PROGRAM
THE UNIVERSITY OF KANSAS, LAWRENCE

PROGRAM ABSTRACT

Title (If subroutine state in title):

FORTRAN IV program for multivariate paleontologic analysis using an IBM System/360 Model 40 computer

Date: May 17, 1967

Author, organization: J.A. Wolleben, R.J. Pauken, and J.A. Dearien, Dept. of Geology, University of Missouri, Columbia, Missouri

Direct inquiries to: Authors, or

Name: D.F. Merriam Address: Kansas Geological Survey
Lawrence, Kansas 66044

Purpose/description: Computes linear discriminant functions and generalized distances for up to 20 groups, each having up to 15 variables and 99 samples. A test for homogeneity is also made.

Mathematical method: _____

Restrictions, range: 20 groups, with up to 15 variables and 99 samples per group.

Computer manufacturer: IBM Model: System/360 Model 40

Programming language: FORTRAN IV

Memory required: 65 K Approximate running time: 2 1/4 min. for 17 groups with 13 variables.

Special peripheral equipment required: None

Remarks (special compilers or operating systems, required word lengths, number of successful runs, other machine versions, additional information useful for operation or modification of program) _____

The program has been adapted to run on the IBM 1620 with 40 K memory (FORTRAN II) and the GE 625.

R-MODE FACTOR ANALYSIS PROGRAM IN FORTRAN II FOR THE IBM 1620 COMPUTER

by

Robert J. Sampson
Idaho State University

INTRODUCTION

Factor analysis is a well-known multivariate procedure for examining relationships between variables. The purpose of the technique is to reduce a multiplicity of variables to a smaller set of underlying variables, or "factors." Originated in the early 1900's by Spearman (1904) for the analysis of psychological traits, factor analysis has been developed into a powerful psychological tool by Cyril Burt and associates (see Burt, 1941, 1949, 1950). Although originally created by nonstatisticians, a statistical framework for the procedure has been erected by Kendall (1950), Bartlett (1950), Lawley and Maxwell (1963), and Jöreskog (1963). In recent years, factor analysis has played a large role in the development of numerical taxonomy (Sokal and Sneath, 1963). The technique also has been applied in geology to problems of paleontologic taxonomy (Kaesler, 1966; Pitcher, 1966), petrology (Harbaugh and Demirmen, 1964; Imbrie and Purdy, 1962; Imbrie and Van Andel, 1964; Klovan, 1966; Toomey, 1966) and mineral exploration (Harris, 1966). Excellent texts have been written by Fruchter (1954), Harman (1960), and Kendall (1957).

Several computer programs have been written to perform factor analysis including those by Cooley and Lohnes (1962), Imbrie (1963), Manson and Imbrie (1964), Dixon (1964), and IBM (1967). The program listed here is similar to other programs but differs in certain aspects.

This program computes factors in the R-mode. That is, it searches for structure within the variables and the factors express sources of variation affecting observations. This is in contrast to Q-mode analysis, which separates observations into factors that may be regarded as subsets of the original sample. The program is designed for operation on an IBM 1620 computer and may be adapted easily to other small computer systems.

Any number of data points may be processed with this program because data are not stored internally. Other programs store raw data in a core matrix or on a disc, which limits the number of observations to a few hundred. In some applications, this restriction is not severe, but many problems in the earth sciences require analysis of hundreds or thousands of observations. For example, the 100-brine analyses used in the accompanying example represent only a part of 3,016 observations contained in the original data set. The unlimited input feature has

made this program sufficiently desirable so that it has been translated into FORTRAN IV for the GE 625 and the IBM 1130.

Theory and computational details of factor analysis are not described here; those unfamiliar with the procedure are referred to Manson and Imbrie (1964) or IBM (1967). This program operates in R-mode and generates the factor matrix, rotated (varimax) factor matrix, and oblique projection matrix. Up to 30 variables per observation (3 data cards per observation) are read in, and up to 20 of these may be selected for factor analysis. The program will compute and list the following information:

- (1) correlation matrix,
- (2) for each variable, the range, standard deviation, mean, standard error of the mean, variance, and coefficient of variation,
- (3) optionally, the multiple regression of all variables on the first variable,
- (4) eigenvalues and eigenvectors (principal components),
- (5) factor matrix for specified number of factors,
- (6) rotated factor matrix,
- (7) communalities,
- (8) variance at each iteration step, and
- (9) oblique projection matrix.

Machine time for this project was donated by Idaho State University Computer Center on equipment supplied in part by NSF Grant GP-2275. Additional time was donated by the Computation Center at Wichita State University.

OPERATING INSTRUCTIONS

The factor analysis program consists of eight object decks which are called and loaded by the program as they are needed. The message LOAD DATA will appear as each of these enters the machine, but should be ignored after Program 1. Additional information will be requested via the console typewriter as required. Decks should be compiled with subroutines prior to execution. All output is punched unless otherwise noted.

program then checks to see if any variables should be substituted. If so, substitutions are made and the oblique matrix recalculated.

Output

Oblique projection matrix.

The factor analysis program may be modified to perform a variety of calculations that stop short of a complete factor analysis. This may be done by using only part of the factor analysis program set. Possible program combinations include:

Program	Purpose
1, 2	Produces statistics of variables and correlation matrix.
1, 2, 3	Performs multiple regression on the first variable. Program 2 is optional.
1, 2, 4, 5	Performs principal components analysis. Program 2 is optional.

Oblique projection may be omitted by omitting Program 8. Program 3 may be omitted if multiple regression is not desired. Program 2 may be omitted if the correlation matrix is not required as output.

TEST EXAMPLE

The factor analysis program was tested on sample data listed in the Appendix. These data con-

sist of 122 analyses of subsurface brines from the Arbuckle Group (Cambrian-Ordovician) in Kansas. The complete data set contains approximately 7,000 brine analyses obtained from the U.S. Bureau of Mines, Halliburton Company, Dow Chemical Company, and from published sources. The subset used as test data was selected for a study of brine type distributions in the Arbuckle and has 11 variables measured on each sample. The variables, in order, are:

- (1) Calcium, in ppm,
- (2) Magnesium, in ppm,
- (3) Sodium, in ppm,
- (4) Bicarbonate, in ppm,
- (5) Sulphate, in ppm,
- (6) Chloride, in ppm,
- (7) Total dissolved salts, in ppm,
- (8) Specific gravity,
- (9) Temperature, C°,
- (10) Electrical resistivity, in ohms/m²/m, and
- (11) pH.

In the analysis, four principal components accounted for about 70 percent of the variation in the system and were retained for factoring and rotation. The resulting factors and factor loadings are given on the final page of output. These factors correspond closely to those extracted by Betty Miller (personal communication, 1967) from brine data published by Ostroff (1967, p. 411-413), suggesting that they reflect fundamental characteristics of subsurface brines in general. Although no conclusions may be drawn from this preliminary study, it would seem that factor analysis may be useful in the characterization of oil-field waters.

REFERENCES

- Bartlett, M. S., 1950, Tests of significance in factor analysis: *British Jour. Psychology Stat. Sec.*, v. 3, p. 77-85.
- Burt, C., 1941, *Factors of the mind; an introduction to factor analysis in psychology*: The Macmillan Co., New York, 509 p.
- Burt, C., 1949, Alternative methods of factor analysis: *British Jour. Psychology Stat. Sec.*, v. 2, p. 98-121.
- Burt, C., 1950, Group factor analysis: *British Jour. Psychology Stat. Sec.*, v. 3, p. 40-75.
- Cooley, W. W., and Lohnes, P. R., 1962, *Multivariate procedures for the behavioral sciences*: John Wiley & Sons, New York, 211 p.
- Dixon, W. J., ed., 1964, *BMD biomedical computer programs*: Health Ser. Computing Facility, Univ. California at Los Angeles, 620 p.
- Fruchter, B., 1954, *Introduction to factor analysis*: D. Van Nostrand Co., Princeton, New Jersey, 280 p.
- Harbaugh, J. W., and Demirmen, F., 1964, Application of factor analysis to petrologic variations of Americus Limestone (Lower Permian), Kansas and Oklahoma: *Kansas Geol. Survey Sp. Dist. Publ.* 15, 40 p.

- Harmon, H. H., 1960, *Modern factor analysis*: Univ. Chicago Press, Chicago, 471 p.
- Harris, D. V. P., 1966, *Factor analysis, a tool for quantitative studies in mineral exploration*: Pennsylvania State Univ., Mineral Industries, v. 2, p. GG1-GG37.
- Imbrie, J., 1963, *Factor and vector analysis programs for analyzing geologic data*: Office of Naval Research, Geography Branch, ONR Task No. 389-135, Tech. Rpt. No. 6, 83 p.
- Imbrie, J., and Purdy, E. G., 1962, *Classification of modern Bahamian carbonate sediments*, in *Classification of carbonate rocks*: Am. Assoc. Petroleum Geologists Mem. 1, p. 253-272.
- Imbrie, J., and Van Andel, T. H., 1964, *Vector analysis of heavy-mineral data*: Geol. Soc. America Bull., v. 75, no. 11, p. 1131-1155.
- IBM, 1967, *1130 statistical system (1130-CA-06s) user's Manual*: IBM Appl. Prog. H 20-0333-0, Tech. Publ. Dept., White Plains, New York, p. 31-71.
- Jöreskog, K. G., 1963, *Statistical estimation in factor analysis*: Almqvist and Wiksells Boktryckeri AB, Uppsala, 145 p.
- Kaesler, R. L., 1966, *Quantitative re-evaluation of ecology and distribution of Recent Foraminifera and Ostracoda of Todos Santos Bay, Baja California, Mexico*: Univ. Kansas Paleontological Contr. Paper 10, 50 p.
- Kendall, M. G., 1950, *Factor analysis as a statistical technique*: Jour. Roy. Stat. Soc., v. B12, p. 60-73.
- Kendall, M. G., 1957, *A course in multivariate analysis*: Charles Griffin and Company, London, 185 p.
- Klovan, J. E., 1966, *The use of factor analysis in determining depositional environments from grain-size distributions*: Jour. Sed. Pet., v. 36, no. 1, p. 115-125.
- Lawley, D. N., and Maxwell, A. E., 1963, *Factor analysis as a statistical method*: Butterworth and Co., London, 117 p.
- Manson, V., and Imbrie, J., 1964, *FORTTRAN program for factor and vector analysis of geologic data using an IBM 7090 or 7094/1401 computer system*: Kansas Geol. Survey Sp. Dist. Publ. 13, 46 p.
- Ostroff, A. G., 1967, *Comparison of some formation water classification systems*: Am. Assoc. Petroleum Geologists Bull., v. 51, no. 3, p. 404-416.
- Pitcher, M. G., 1966, *A factor analytic scheme for grouping and separating types of fossils*, in *Colloquium on classification procedures*: Kansas Geol. Survey Computer Contr. 7, p. 30-41.
- Sokal, R. R., and Sneath, P. H. A., 1963, *Principles of numerical taxonomy*: W. H. Freeman and Co., San Francisco, 359 p.
- Spearman, C., 1904, *General intelligence, objectively determined and measured*: Am. Jour. Psychology, v. 15, p. 201-293.
- Toomey, D. F., 1966, *Application of factor analysis to a facies study of the Leavenworth Limestone (Pennsylvanian-Virgilian) of Kansas environs*: Kansas Geol. Survey Sp. Dist. Publ. 27, 28 p.

Appendix.

```
C   CORRELATION
C   MULTIPLE REGRESSION
C   FACTOR ANALYSIS
C   PROGRAM 1
C   CORRELATION MATRIX GENERATION
C   ROBERT SAMPSON -- PROGRAMMER
C   4 / 26 / 1967
BEGIN TRACE
COMMON R(210),T(19),N,IPAGE,CONST,AM(20),SD(20),NS
DIMENSION CP(210),SX(20),XMIN(20),XMAX(20),X(20),V(30),K(20)
DO 100 I=1,210
100 CP(I)=0.0
DO 101 I=1,20
SX(I)=0.0
XMIN(I)=.99E 49
101 XMAX(I)=-.99E 49
T(19)=.57414745
NS=0
READ 1000,NI,N,K(1),K(2),K(3),K(4),K(5),K(6),K(7),K(8),K(9),
1K(10),K(11),K(12),K(13),K(14),K(15),K(16),K(17),K(18),K(19),K(20)
READ 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18)
1 READ 1002,V(1),V(2),V(3),V(4),V(5),V(6),V(7),V(8),V(9),V(10)
IF (V(1)-9.0E 48) 2,3,3
2 IF (NI-10) 4,4,5
5 READ 1002,V(11),V(12),V(13),V(14),V(15),V(16),V(17),V(18),
1V(19),V(20)
IF (NI-20) 4,4,14
14 READ 1002,V(21),V(22),V(23),V(24),V(25),V(26),V(27),V(28),
1V(29),V(30)
4 NS=NS+1
DO 110 I=1,N
J=K(I)
110 X(I)=V(J)
DO 102 I=1,N
SX(I)=SX(I)+X(I)
IS=I*(I-1)/2
DO 103 J=1,I
JS=IS+J
CP(JS)=CP(JS)+X(I)*X(J)
103 CONTINUE
IF (XMIN(I)-X(I)) 6,6,7
7 XMIN(I)=X(I)
6 IF (X(I)-XMAX(I)) 102,102,8
8 XMAX(I)=X(I)
102 CONTINUE
GO TO 1
3 AN=NS
IPAGE=1
PUNCH 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
PUNCH 1005,NS
PUNCH 1003
DO 104 I=1,N
AM(I)=SX(I)/AN
II=I*(I+1)/2
```

```

SD(I)=SQRT((CP(II)-(SX(I)**2)/AN)/(AN-1.0))
SE=SD(I)/SQRT(AN)
104 PUNCH 1004,K(I),XMIN(I),XMAX(I),AM(I),SE
    IPAGE=2
    PUNCH 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
    1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
    PUNCH 1006
    DO 107 I=1,N
    VAR=SD(I)**2
    CV=100.0*SD(I)/AM(I)
107 PUNCH 1004,K(I),SD(I),VAR,CV
    AN1=AN-1.0
    DO 105 I=1,N
    IS=I*(I-1)/2
    DO 106 J=1,I
    JS=IS+J
    R(JS)=(CP(JS)-SX(I)*SX(J)/AN)/(SD(I)*SD(J)*AN1)
106 CONTINUE
105 CONTINUE
    A=EXIT(1.0)
1000 FORMAT (22I2)
1001 FORMAT (19A4,I3,1H-)
1002 FORMAT (10F7.2)
1003 FORMAT (8HVARIALE,6X,7HMINIMUM,8X,7HMAXIMUM,24X,8HSTANDARD,/,
    17H NUMBER,8X,5HVALUE,10X,5HVALUE,11X,4HMEAN,6X,13HERROR OF MEAN)
1004 FORMAT (/,I6,4X,4F15.7)
1005 FORMAT (/,29HNUMBER OF SAMPLES EXAMINED = ,I6,/)
1006 FORMAT (/,8HVARIALE,7X,8HSTANDARD,21X,11HCOEFFICIENT,/,
    17H NUMBER,7X,9HDEVIATION,8X,8HVARIANCE,4X,12HOF VARIATION)
    END TRACE
    END

```

```

C      CORRELATION
C      MULTIPLE REGRESSION
C      FACTOR ANALYSIS
C      PROGRAM 2
C      CORRELATION MATRIX OUTPUT
C      ROBERT SAMPSON -- PROGRAMMER
C      4 / 26 / 1967
C      12244 - 12298 - 12580
C      BEGIN TRACE
COMMON R(210),T(19),N,IPAGE,C1,AM(20),SD(20),NS
DIMENSION A(20,20)
DO 100 I=1,N
IS=I*(I-1)/2
DO 101 J=1,I
JS=IS+J
A(I,J)=R(JS)
101 A(J,I)=A(I,J)
100 CONTINUE
    ID=0
    IND=N
    IT=1
    33 IPAGE=IPAGE+1

```

```

PUNCH 1000,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
PUNCH 1002
DO 102 I=1,IND
J=I+ID
GO TO (1,2,3,4,5,6,7,8,9,10,10,10,10,10,10,10,10,10),I
1 PUNCH 1001,J,A(J,IT)
GO TO 102
2 PUNCH 1001,J,A(J,IT),A(J,IT+1)
GO TO 102
3 PUNCH 1001,J,A(J,IT),A(J,IT+1),A(J,IT+2)
GO TO 102
4 PUNCH 1001,J,A(J,IT),A(J,IT+1),A(J,IT+2),A(J,IT+3)
GO TO 102
5 PUNCH 1001,J,A(J,IT),A(J,IT+1),A(J,IT+2),A(J,IT+3),A(J,IT+4)
GO TO 102
6 PUNCH 1001,J,A(J,IT),A(J,IT+1),A(J,IT+2),A(J,IT+3),A(J,IT+4),
1A(J,IT+5)
GO TO 102
7 PUNCH 1001,J,A(J,IT),A(J,IT+1),A(J,IT+2),A(J,IT+3),A(J,IT+4),
1A(J,IT+5),A(J,IT+6)
GO TO 102
8 PUNCH 1001,J,A(J,IT),A(J,IT+1),A(J,IT+2),A(J,IT+3),A(J,IT+4),
1A(J,IT+5),A(J,IT+6),A(J,IT+7)
GO TO 102
9 PUNCH 1001,J,A(J,IT),A(J,IT+1),A(J,IT+2),A(J,IT+3),A(J,IT+4),
1A(J,IT+5),A(J,IT+6),A(J,IT+7),A(J,IT+8)
GO TO 102
10 PUNCH 1001,J,A(J,IT),A(J,IT+1),A(J,IT+2),A(J,IT+3),A(J,IT+4),
1A(J,IT+5),A(J,IT+6),A(J,IT+7),A(J,IT+8),A(J,IT+9)
102 CONTINUE
IF (IND-10) 31,31,32
32 ID=10
IT=11
IND=N-10
GO TO 33
31 R=EXIT(1.0)
1000 FORMAT (19A4,I3,1H-,/)
1001 FORMAT (/ ,I4,10F7.4)
1002 FORMAT (27HCORRELATION COEFFICIENT (R),/)
END TRACE
END

```

```

C CORRELATION
C MULTIPLE REGRESSION
C FACTOR ANALYSIS
C PROGRAM 3
C MULTIPLE REGRESSION
C ROBERT SAMPSON -- PROGRAMMER
C 4 / 26 / 1967
C 09318 - 09732 - 12650
C BEGIN TRACE
COMMON R(210),T(19),N,IPAGE,C1,AM(20),SD(20),NS
DIMENSION A(20,20)

```

```

DO 106 I=1,N
  IS=I*(I-1)/2
  DO 107 J=1,I
    JS=IS+J
    A(I,J)=R(JS)
107 A(J,I)=A(I,J)
106 CONTINUE
  DO 100 I=2,N
    DO 101 J=2,N
      IF (I-J) 1,101,1
      1 F=-A(J,I)/A(I,I)
      A(J,1)=A(J,1)+F*A(I,1)
      DO 102 K=I,N
102 A(J,K)=A(J,K)+F*A(I,K)
101 CONTINUE
100 CONTINUE
  DO 105 I=2,N
105 A(I,1)=A(I,1)/A(I,I)
  RR=0.0
  CONST=AM(1)
  DO 103 I=2,N
    A(I,2)=A(I,1)*SD(1)/SD(I)
    J=(I*I-I)/2+1
    RR=RR+A(I,1)*R(J)
103 CONST=CONST-A(I,2)*AM(I)
  G=SQRT(RR)
  IPAGE=IPAGE+1
  PUNCH 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
  PUNCH 1002,RR,G,CONST
  DO 104 I=2,N
    J=I-1
104 PUNCH 1003,J,A(I,1),A(I,2)
  RR=EXIT(1.0)
1001 FORMAT (19A4,I3,1H-,/)
1002 FORMAT (18HGOODNESS OF FIT = ,F10.6,/,23HMULTIPLE CORRELATION = ,
1F10.6,/,23X,E18.8)
1003 FORMAT (15,2E18.8)
  END TRACE
  END

```

```

C CORRELATION
C MULTIPLE REGRESSION
C FACTOR ANALYSIS
C PROGRAM 4
C FACTOR ANALYSIS -- EIGENVALUES AND EIGENVECTORS
C 04 / 27 / 1967
C 10788 - 11222 - 12620
C ROBERT SAMPSON -- PROGRAMMER
C BEGIN TRACE
COMMON A(210),T(19),N,IPAGE,CONST,R(400)
AN=N
ANORM=0.0

```



```

IA=0
DO 100 I=1,N
DO 101 J=1,N
IA=IA+1
R(IA)=0.0
IF (I-J) 101,1,101
1 R(IA)=1.0
101 CONTINUE
DO 103 J=1,N
IF (I-J) 2,103,2
2 JA=I+(J*J-J)/2
ANORM=ANORM+A(JA)**2
103 CONTINUE
100 CONTINUE
IF (ANORM) 3,3,4
4 ANORM=SQRT(2.0*ANORM)
ANRMX=ANORM*1.0E-06/AN
IND=0
THR=ANORM
5 THR=THR/AN
6 L=1
7 M=L+1
8 MQ=(M*M-M)/2
LQ=(L*L-L)/2
LM=L+MQ
IF (ABS(A(LM))-THR) 10,11,11
11 IND=1
LL=L+LQ
MM=M+MQ
X=(A(LL)-A(MM))/2.0
Y=-A(LM)/SQRT(A(LM)**2+X*X)
IF (X) 13,14,14
13 Y=-Y
14 SINX=Y/SQRT(2.0*(1.0+SQRT(1.0-Y*Y)))
SINX2=SINX*SINX
COSX=SQRT(1.0-SINX2)
COSX2=COSX*COSX
SINCS=SINX*COSX
ILQ=N*(L-1)
IMQ=N*(M-1)
DO 102 I=1,N
IQ=(I*I-I)/2
IF (I-L) 16,17,16
16 IF (I-M) 18,17,20
18 IM=I+MQ
GO TO 19
20 IM=M+IQ
19 IF (I-L) 21,22,22
21 IL=I+LQ
GO TO 23
22 IL=L+IQ
23 X=A(IL)*COSX-A(IM)*SINX
A(IM)=A(IL)*SINX+A(IM)*COSX
A(IL)=X
17 ILR=ILQ+I
IMR=IMQ+I
X=R(ILR)*COSX-R(IMR)*SINX
R(IMR)=R(ILR)*SINX+R(IMR)*COSX
R(ILR)=X
102 CONTINUE

```

```

X=2.0*A(LM)*SINCS
Y=A(LL)*COSX2+A(MM)*SINX2-X
X=A(LL)*SINX2+A(MM)*COSX2+X
A(LM)=(A(LL)-A(MM))*SINCS+A(LM)*(COSX2-SINX2)
A(LL)=Y
A(MM)=X
10 IF (M-N) 25,26,25
25 M=M+1
GO TO 8
26 IF (L-N+1) 27,28,27
27 L=L+1
GO TO 7
28 IF (IND-1) 29,30,29
30 IND=0
GO TO 6
29 IF (THR-ANRMX) 3,3,5
3 X=EXIT(1.0)
END TRACE
END

```

```

C CORRELATION
C MULTIPLE REGRESSION
C FACTOR ANALYSIS
C PROGRAM 5
C FACTOR ANALYSIS -- EIGENVALUES AND EIGENVECTORS CONTINUED AND
C CUMULATIVE PERCENTAGE OF EIGENVALUES
C 04 / 27 / 1967
C 09190 - 09244 - 12990
C ROBERT SAMPSON -- PROGRAMMER
C BEGIN TRACE
COMMON A(210),T(19),N,IPAGE,CONST,R(400),K
DIMENSION D(20)
AN=N
DO 100 I=1,N
IQ=N*(I-1)
LL=(I*I+I)/2
JQ=N*(I-2)
DO 101 J=I,N
JQ=JQ+N
MM=(J*J+J)/2
IF (A(LL)-A(MM)) 1,101,101
1 X=A(LL)
A(LL)=A(MM)
A(MM)=X
DO 102 K=1,N
ILR=IQ+K
IMR=JQ+K
X=R(ILR)
R(ILR)=R(IMR)
102 R(IMR)=X
101 CONTINUE
100 CONTINUE
4 IPAGE=IPAGE+1

```

```

PUNCH 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
PUNCH 1002
CP=0.0
DO 104 I=1,N
J=(I*I+I)/2
CP=CP+A(J)*100.0/AN
PRINT 1003,I,A(J),CP
104 PUNCH 1003,I,A(J),CP
IG=1
16 IQ=0
IPAGE=IPAGE+1
PUNCH 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
PUNCH 1006
DO 105 I=1,N
DO 106 J=1,20
106 D(J)=0.
DO 107 L=1,N
IQ=IQ+1
107 D(L)=R(IQ)
GO TO (11,12),IG
11 PUNCH 1005,I,D(1),D(2),D(3),D(4),D(5),D(6),D(7),D(8),D(9),D(10)
GO TO 105
12 PUNCH 1005,I,D(11),D(12),D(13),D(14),D(15),D(16),D(17),D(18),
1D(19),D(20)
105 CONTINUE
IF (N-11) 13,14,14
14 GO TO (15,13),IG
15 IG=2
GO TO 16
13 L=0
JJ=0
PRINT 1010
ACCEPT 1003,K
DO 110 J=1,K
JJ=JJ+J
SQ=SQRT(A(JJ))
DO 111 I=1,N
L=L+1
111 R(L)=SQ*R(L)
110 CONTINUE
IPAGE=IPAGE+1
PUNCH 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
PUNCH 1007,K
DO 112 I=1,N
DO 113 J=1,20
113 D(J)=0.0
DO 114 J=1,K
L=N*(J-1)+I
114 D(J)=R(L)
PUNCH 1008,I,D(1),D(2),D(3),D(4),D(5),D(6),D(7),D(8),D(9),D(10),
1D(11),D(12),D(13),D(14)
112 CONTINUE
IF (K-1) 20,20,21
20 PRINT 1009,K
STOP 100
21 C=EXIT(1.0)
1001 FORMAT (19A4,I3,1H-)

```

```

1002 FORMAT (/ ,9X,10HEIGENVALUE,6X,7HPERCENT,/)
1003 FORMAT (I4,2F15.7)
1005 FORMAT (/ ,6HVECTOR,I4,9X,6F10.6,/,4F10.6,39X,1H2)
1006 FORMAT (/ ,12HEIGENVECTORS,/)
1007 FORMAT (/ ,15HFACTOR MATRIX (,I4,9H FACTORS),/)
1008 FORMAT (/ ,I4,3X,9F8.4,/,5F8.4,39X,1H2)
1009 FORMAT (4HONLY,I4,33H FACTORS, NO ROTATION CAN BE MADE)
1010 FORMAT (27HNUMBER OF FACTORS TO ROTATE)
      END TRACE
      END

```

```

C      CORRELATION
C      MULTIPLE REGRESSION
C      FACTOR ANALYSIS
C      PROGRAM 6
C      FACTOR ANALYSIS -- VARIMAX ROTATION
C      04 / 28 / 1967
C      ROBERT SAMPSON -- PROGRAMMER
      BEGIN TRACE
      COMMON TV(210),T(19),N,IPAGE,CONST,A(400),K,H(20),NC
      DO 106 I=1,N
      H(I)=0.0
      DO 107 J=1,K
      L=N*(J-1)+I
107 H(I)=H(I)+A(L)**2
      HI=SQRT(H(I))
      DO 108 J=1,K
      L=N*(J-1)+I
108 A(L)=A(L)/HI
106 CONTINUE
      EPS=.00116
      TVLT=0.0
      LL=K-1
      NV=1
      NC=0
      FN=N
      FFN=FN*FN
      CONS=.7071066
1   TV(NV)=0.0
      DO 100 J=1,K
      AA=0.0
      BB=0.0
      LB=N*(J-1)
      DO 101 I=1,N
      L=LB+I
      CC=A(L)*A(L)
      AA=AA+CC
101 BB=BB+CC*CC
100 TV(NV)=TV(NV)+(FN*BB-AA*AA)/FFN
      IF (SENSE SWITCH 1) 30,31
      30 PRINT 1000,NV,TV(NV)
1000 FORMAT (I4,F15.8)
      31 IF (NV-51) 2,3,3

```

```

2 IF (TV(NV)-TVLT-1.0E-07) 4,4,5
4 NC=NC+1
  IF (NC-3) 5,5,3
5 DO 102 J=1,LL
  L1=N*(J-1)
  II=J+1
  DO 103 KI=II,K
  L2=N*(KI-1)
  AA=0.0
  BB=0.0
  CC=0.0
  DD=0.0
  DO 104 I=1,N
  L3=L1+I
  L4=L2+I
  U=(A(L3)+A(L4))*(A(L3)-A(L4))
  TN=A(L3)*A(L4)*2.0
  CC=CC+(U+TN)*(U-TN)
  DD=DD+2.0*U*TN
104 AA=AA+U
  BB=BB+TN
  TN=DD-2.0*AA*BB/FN
  B=CC-(AA*AA-BB*BB)/FN
  IF (TN-B) 7,8,9
  8 IF (TN+B-EPS) 103,10,10
10 COS4T=CONS
  SIN4T=CONS
  GO TO 11
  7 TAN4T=ABS(TN/B)
  IF (TAN4T-EPS) 12,13,13
13 COS4T=1.0/SQRT(1.0+TAN4T*TAN4T)
  SIN4T=TAN4T*COS4T
  GO TO 11
12 IF (B) 14,103,103
14 SINP=CONS
  COSP=CONS
  GO TO 15
  9 CTN4T=ABS(TN/B)
  IF (CTN4T-EPS) 16,17,17
17 SIN4T=1.0/SQRT(1.0+CTN4T*CTN4T)
  COS4T=CTN4T*SIN4T
  GO TO 11
16 COS4T=0.0
  SIN4T=1.0
11 COS2T=SQRT((1.0+COS4T)/2.0)
  SIN2T=SIN4T/(2.0*COS2T)
  COST=SQRT((1.0+COS2T)/2.0)
  SINT=SIN2T/(2.0*COST)
  IF (B) 19,19,20
20 COSP=COST
  SINP=SINT
  GO TO 23
19 COSP=CONS*(COST+SINT)
  SINP=ABS(CONS*(COST-SINT))
23 IF (TN) 24,24,15
24 SINP=-SINP
15 DO 109 I=1,N
  L3=L1+I
  L4=L2+I
  AA=A(L3)*COSP+A(L4)*SINP
  A(L4)=-A(L3)*SINP+A(L4)*COSP

```

```

109 A(L3)=AA
103 CONTINUE
102 CONTINUE
    NV=NV+1
    TVLT=TV(NV-1)
    GO TO 1
  3 NC=NV-1
    C=EXIT(1.0)
    END TRACE
    END

```

```

C    CORRELATION
C    MULTIPLE REGRESSION
C    FACTOR ANALYSIS
C    PROGRAM 7
COMMON TV(210),T(19),N,IPAGE,C1,A(400),K,H(20),NC
DIMENSION D(20),F(20),E(20)
DO 100 I=1,N
DO 101 J=1,K
L=N*(J-1)+I
101 A(L)=A(L)*SQRT(H(I))
100 CONTINUE
DO 103 I=1,N
F(I)=0.0
DO 104 J=1,K
L=N*(J-1)+I
104 F(I)=F(I)+A(L)*A(L)
103 D(I)=H(I)-F(I)
IPAGE=IPAGE+1
PUNCH 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
PUNCH 1002
NV=NC+1
DO 105 I=1,NV
J=I-1
105 PUNCH 1003,J,TV(I)
IPAGE=IPAGE+1
PUNCH 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
PUNCH 1005,K
DO 106 I=1,N
DO 108 J=1,20
108 E(J)=0.0
DO 107 J=1,K
L=N*(J-1)+I
107 E(J)=A(L)
PUNCH 1004,I,E(1),E(2),E(3),E(4),E(5),E(6),E(7),E(8),E(9)
IF (K-10) 106,11,11
  11 PUNCH 1009,E(10),E(11),E(12),E(13),E(14)
106 CONTINUE
IPAGE=IPAGE+1
PUNCH 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
PUNCH 1006

```

```

DO 109 I=1,N
109 PUNCH 1007,I,H(I),F(I),D(I)
DO 110 I=1,K
BIG=0.0
JS=0
DO 111 J=1,N
L=N*(I-1)+J
IF (BIG-ABS(A(L))) 20,111,111
20 BIG=ABS(A(L))
JS=J
111 CONTINUE
H(I)=JS
110 CONTINUE
M=K+1
DO 112 I=M,N
H(I)=0.0
DO 114 L=1,N
C1=L
DO 113 J=1,I
IF (H(J)-C1) 113,114,113
113 CONTINUE
H(I)=C1
GO TO 112
114 CONTINUE
112 CONTINUE
C1=EXIT(1.0)
1001 FORMAT (19A4,I3,1H-)
1002 FORMAT (/ ,9HITERATION,3X,9HVARIANCES,/)
1003 FORMAT (I7,F16.7)
1004 FORMAT (/ ,I4,2X,9F8.4)
1005 FORMAT (/ ,23HROTATED FACTOR MATRIX ( ,I4,9H FACTORS),/)
1006 FORMAT (/ ,22HCHECK ON COMMUNALITIES,/)
1007 FORMAT (I6,3F20.7)
1009 FORMAT (5F8.5,39X,1H2)
END TRACE
END

```

```

C CORRELATION
C MULTIPLE REGRESSION
C FACTOR ANALYSIS
C PROGRAM 8
BEGIN TRACE
COMMON V(14,15),T(19),N,IPAGE,C1,B(400),K,H(20)
IR=0
1 DO 100 I=1,K
LINE=H(I)
DO 101 J=1,K
L=N*(J-1)+LINE
101 V(I,J)=B(L)
100 CONTINUE
NP=K+1
DO 102 I=1,K
DO 103 J=1,K
103 V(J,NP)=0.0
V(I,NP)=1.0

```

```

      DIV=V(I,I)
      DO 104 J=1,NP
104  V(I,J)=V(I,J)/DIV
      DO 105 J=1,K
      IF (I-J) 2,105,2
      2  FAC=V(J,I)
      DO 106 L=1,NP
106  V(J,L)=V(J,L)-V(I,L)*FAC
105  CONTINUE
      DO 107 J=1,K
107  V(J,I)=V(J,NP)
102  CONTINUE
      IPAGE=IPAGE+1
      IR=IR+1
      PUNCH 1001,T(1),T(2),T(3),T(4),T(5),T(6),T(7),T(8),T(9),T(10),
1  T(11),T(12),T(13),T(14),T(15),T(16),T(17),T(18),T(19),IPAGE
      PUNCH 1002,IR
      IS=1
      JS=1
      TB=0.0
      DO 108 I=1,N
      J=H(I)
      DO 109 L=1,14
109  V(L,15)=0.0
      DO 110 M=1,K
      DO 111 MM=1,K
      NN=N*(MM-1)+J
111  V(M,15)=V(M,15)+B(NN)*V(MM,M)
      IF (ABS(V(M,15))-TB) 110,110,4
      4  TB=ABS(V(M,15))
      IS=I
      JS=M
110  CONTINUE
      PUNCH 1003,J,V(1,15),V(2,15),V(3,15),V(4,15),V(5,15),V(6,15),
1  V(7,15),V(8,15),V(9,15)
      IF (K-10) 108,10,10
      10 PUNCH 1004,V(10,15),V(11,15),V(12,15),V(13,15),V(14,15)
108  CONTINUE
      IF (TB-1.00005) 5,5,6
      5  C=EXIT(1.0)
      6  AM=H(JS)
      H(JS)=H(IS)
      H(IS)=AM
      GO TO 1
1001 FORMAT (19A4,I3,1H-)
1002 FORMAT (/,25HOBlique PROJECTION MATRIX,I4,/)
1003 FORMAT (/,I4,3X,9F8.5)
1004 FORMAT (5F8.5,39X,1H2)
      END TRACE
      END

```


1111 1 2 3 4 5 6 7 8 9 10 11

FACTOR ANALYSIS OF ARBUCKLE BRINE DATA.

0.60381E	020.10047E	030.57380E	040.15210E	040.77000E	030.58000E	030.10425E	04
0.68236E	050.20963E	050.10760E	010.10000E	030.24800E	000.63667E	01	
0.81229E	020.10775E	030.30900E	040.67209E	030.15500E	040.30267E	030.24759E	04
0.41303E	050.51472E	050.10444E	010.10000E	030.11200E	000.66111E	01	
0.81245E	020.10675E	030.29789E	040.78714E	030.16500E	040.33667E	030.35208E	04
0.39018E	050.95806E	050.10484E	010.10000E	030.83500E	-010.66167E	01	
0.79251E	020.10672E	030.27200E	040.80500E	030.14300E	040.29350E	030.19033E	04
0.28833E	050.50827E	050.10343E	010.10000E	030.12100E	000.67500E	01	
0.78255E	020.10670E	030.21876E	040.87057E	030.14400E	040.36200E	030.28425E	04
0.35400E	050.66314E	050.10410E	010.10000E	030.11700E	000.70375E	01	
0.80490E	020.90734E	020.33900E	040.10558E	040.10100E	040.48350E	030.21600E	04
0.32326E	050.58141E	050.10415E	010.10000E	030.16200E	000.63000E	01	
0.88138E	020.11186E	030.30100E	040.10223E	040.17500E	040.37800E	030.21350E	04
0.38925E	050.61162E	050.10387E	010.10000E	030.10700E	000.73333E	01	
0.84314E	020.10180E	030.31188E	040.92775E	030.17300E	040.36950E	030.11175E	04
0.43413E	050.64642E	050.10445E	010.10000E	030.10050E	000.76000E	01	
0.85392E	020.96812E	020.31390E	040.63750E	030.25400E	040.44500E	030.74650E	03
0.38800E	050.70645E	050.10480E	010.10000E	030.89000E	-010.64000E	01	
0.14417E	020.23531E	020.20750E	040.57517E	030.12360E	040.32550E	030.87540E	03
0.24600E	050.42237E	050.10298E	010.10000E	030.13750E	000.75000E	01	
0.91129E	020.14364E	030.23710E	040.10595E	040.16300E	040.47950E	030.20550E	04
0.34900E	050.65670E	050.10445E	010.10000E	030.10700E	000.67000E	01	
0.91191E	020.13964E	030.27325E	030.61000E	030.83600E	030.14320E	040.29340E	04
0.18400E	050.38225E	050.10245E	010.10000E	030.25200E	000.70000E	01	
0.92378E	020.12766E	030.30550E	040.79167E	030.16800E	040.41700E	030.20067E	04
0.30433E	050.58963E	050.10393E	010.10000E	030.11400E	000.65000E	01	
0.99021E	020.14777E	030.22803E	040.69150E	030.13300E	040.22067E	030.26613E	04
0.24325E	050.45821E	050.10307E	010.10000E	030.12567E	000.77667E	01	
0.98215E	020.13675E	030.31119E	040.86641E	030.15700E	040.41971E	030.24006E	04
0.30824E	050.51958E	050.98294E	000.10000E	030.11033E	000.65167E	01	
0.10298E	030.14884E	030.34863E	040.10723E	040.19243E	040.48850E	030.22650E	04
0.36163E	050.62264E	050.10431E	010.10000E	030.10100E	000.75000E	01	
0.10600E	030.12690E	030.24550E	040.58000E	030.15300E	040.27000E	030.21175E	04
0.28550E	050.50150E	050.10335E	010.10000E	030.11750E	000.69000E	01	
0.10307E	030.14384E	030.31200E	040.93100E	030.16700E	040.51500E	030.22150E	04
0.30550E	050.57903E	050.10390E	010.10000E	030.98000E	-010.77000E	01	
0.10340E	030.12584E	030.25488E	040.72675E	030.15300E	040.32100E	030.22069E	04
0.28538E	050.48045E	050.10312E	010.10000E	030.11825E	000.66000E	01	
0.10443E	030.12386E	030.24130E	040.70980E	030.13700E	040.65000E	030.16848E	04
0.26347E	050.46540E	050.10310E	010.10000E	030.12100E	000.67750E	01	
0.10445E	030.12286E	030.26000E	040.65100E	030.13550E	040.35700E	030.12933E	04
0.28400E	050.44844E	050.10310E	010.10000E	030.12900E	000.69000E	01	
0.11326E	030.13203E	030.24167E	040.56767E	030.14250E	040.18400E	030.19400E	04
0.28367E	050.45798E	050.10323E	010.10000E	030.12850E	000.69000E	01	
0.11524E	030.13307E	030.22967E	040.57767E	030.15500E	040.36700E	030.22667E	04
0.25533E	050.46978E	050.10327E	010.10000E	030.13000E	000.70000E	01	
0.44350E	020.10832E	030.12774E	040.38867E	030.12000E	040.35717E	030.14572E	04
0.16026E	050.33226E	050.10202E	010.10000E	030.22633E	000.69650E	01	
0.49314E	020.11036E	030.37778E	040.82033E	030.11900E	040.33650E	030.10796E	04
0.29073E	050.52964E	050.10369E	010.10000E	030.89000E	-010.70625E	01	
0.52321E	020.10839E	030.12993E	040.28925E	030.79550E	030.55000E	030.19200E	04
0.19825E	050.23419E	050.10235E	010.10000E	030.21200E	000.69500E	01	
0.57207E	020.11744E	030.10506E	040.37450E	030.68300E	030.49813E	030.15989E	04
0.18819E	050.39682E	050.10211E	010.10000E	030.18786E	000.71671E	01	
0.59229E	020.11446E	030.24734E	040.73473E	030.61900E	030.45471E	030.22045E	04
0.40069E	050.22416E	050.10415E	010.10000E	030.19533E	000.69950E	01	
0.55248E	020.11442E	030.10293E	040.42340E	030.68500E	030.41600E	030.18264E	04
0.12239E	050.24269E	050.10162E	010.10000E	030.23600E	000.73840E	01	
0.55259E	020.11342E	030.11476E	040.51380E	030.83900E	030.33667E	030.22300E	04

0.16860E 050.28767E 050.10204E 010.10000E 030.19300E 000.77500E 01
0.58299E 020.10845E 030.19041E 040.55310E 030.89600E 030.36925E 030.18905E 04
0.19763E 050.25206E 050.10235E 010.10000E 030.22757E 000.71417E 01
0.12528E 030.15968E 030.20608E 040.60713E 030.13259E 040.32786E 030.15054E 04
0.25414E 050.41664E 050.10290E 010.10000E 030.15829E 000.70000E 01
0.12236E 030.15661E 030.22420E 040.69120E 030.11387E 040.57733E 030.21960E 04
0.23032E 050.35888E 050.10264E 010.10000E 030.14967E 000.71000E 01
0.12143E 030.15359E 030.73700E 030.21050E 030.48400E 030.30950E 030.41500E 03
0.76650E 040.14494E 050.10085E 010.10000E 030.33900E 000.72000E 01
0.15422E 020.88039E 020.34010E 040.99489E 030.11200E 040.29860E 030.23711E 04
0.36373E 050.75832E 050.10437E 010.10000E 030.13733E 000.69125E 01
0.12145E 030.18241E 030.14744E 040.53280E 030.21000E 040.25633E 030.26420E 04
0.25248E 050.51659E 050.10316E 010.10000E 030.68000E-010.73333E 01
0.89437E 020.93878E 020.23097E 040.55833E 030.67300E 030.38033E 030.15483E 04
0.34169E 050.53932E 050.10363E 010.10000E 030.24300E 000.68000E 01
0.94397E 020.95964E 020.30510E 040.88314E 030.18500E 040.35050E 030.91657E 03
0.38617E 050.62079E 050.10436E 010.10000E 030.90000E-010.76417E 01
0.90033E 020.86791E 020.21433E 040.71100E 030.14850E 040.24100E 030.20000E 03
0.28900E 050.48753E 050.10347E 010.10000E 030.11000E 000.80000E 01
0.11544E 030.18327E 030.40415E 040.66675E 030.22500E 040.35167E 030.18758E 04
0.36225E 050.66453E 050.10437E 010.90000E 020.10100E 000.69333E 01
0.69203E 020.55788E 020.22923E 040.60275E 030.19500E 040.77400E 030.20550E 04
0.27750E 050.38818E 050.10317E 010.10000E 030.17400E 000.69000E 01
0.51269E 020.83263E 020.31774E 040.80029E 030.23300E 040.29343E 030.11257E 04
0.39286E 050.72951E 050.10464E 010.10000E 030.89167E-010.75000E 01
0.43369E 020.10631E 030.12310E 040.29150E 030.68700E 030.50625E 030.15775E 04
0.13137E 050.23003E 050.10157E 010.10000E 030.23050E 000.71800E 01
0.46402E 020.10133E 030.17356E 040.38260E 030.11193E 040.42600E 030.16876E 04
0.17812E 050.36271E 050.10200E 010.10000E 030.19400E 000.72000E 01
0.50374E 020.10337E 030.12483E 040.24025E 030.58700E 030.50000E 030.14640E 04
0.12400E 050.24363E 050.10160E 010.10000E 030.22967E 000.71667E 01
0.53406E 020.99397E 020.19623E 040.52991E 030.67100E 030.56950E 030.73000E 03
0.18952E 050.23363E 050.10206E 010.10000E 030.24100E 000.70000E 01
0.52417E 020.98388E 020.12867E 040.28233E 030.61700E 030.42700E 030.15367E 04
0.14567E 050.21638E 050.10170E 010.10000E 030.25500E 000.74000E 01
0.49422E 020.98360E 020.15003E 040.38800E 030.67900E 030.68800E 030.21987E 04
0.29212E 050.63117E 050.10330E 010.10000E 030.24000E 000.66500E 01
0.52427E 020.97388E 020.13630E 040.49833E 030.65400E 030.56400E 030.16743E 04
0.22267E 050.41495E 050.10273E 010.10000E 030.25000E 000.75000E 01
0.51438E 020.96378E 020.17623E 040.49133E 030.66900E 030.45600E 030.68720E 03
0.20062E 050.39643E 050.10240E 010.10000E 030.23100E 000.69400E 01
0.52456E 020.94388E 020.13354E 040.41588E 030.63500E 030.22775E 030.27194E 04
0.23399E 050.40863E 050.10306E 010.87000E 020.26650E 000.71143E 01
0.51457E 020.94378E 020.87700E 030.32100E 030.69000E 030.45800E 030.10450E 04
0.12100E 050.22368E 050.10150E 010.10000E 030.23400E 000.75000E 01
0.52465E 020.93388E 020.64500E 030.23600E 030.62800E 030.43300E 030.10035E 04
0.84500E 040.15291E 050.10095E 010.10000E 030.26300E 000.70000E 01
0.57313E 020.10744E 030.13653E 040.49300E 030.91600E 030.37500E 030.17700E 04
0.15700E 050.31713E 050.10200E 010.10000E 030.17500E 000.72500E 01
0.59306E 020.10746E 030.16593E 040.37214E 030.82000E 030.39100E 030.24325E 04
0.14992E 050.27042E 050.10164E 010.10000E 030.18250E 000.71286E 01
0.59339E 020.10446E 030.17033E 040.41733E 030.53900E 030.26050E 030.22200E 04
0.15197E 050.21497E 050.10193E 010.10000E 030.26000E 000.66500E 01
0.55381E 020.10142E 030.39460E 040.66975E 030.70700E 030.14700E 030.18300E 04
0.39080E 050.24031E 050.10477E 010.10000E 030.10700E 000.71000E 01
0.59372E 020.10146E 030.12950E 040.36500E 030.64700E 030.17400E 030.20400E 04
0.12250E 050.22902E 050.10155E 010.10000E 030.23400E 000.75000E 01
0.54404E 020.99407E 020.69250E 030.31150E 030.61500E 030.32900E 030.50800E 03
0.11150E 050.17471E 050.10115E 010.10000E 030.25450E 000.75000E 01
0.57398E 020.99438E 020.21639E 040.10153E 040.80100E 030.42200E 030.31650E 03
0.25318E 050.30237E 050.10218E 010.10000E 030.20900E 000.61833E 01
0.58396E 020.99449E 020.32215E 030.28350E 030.66800E 030.60500E 030.50000E 02

0.12525E	050.20125E	050.10120E	010.10000E	030.25200E	000.69000E	01
0.59405E	020.98460E	020.10070E	040.16733E	030.66700E	030.56200E	030.17450E 03
0.15633E	050.23173E	050.10125E	010.10000E	030.24500E	000.70000E	01
0.54424E	020.97407E	020.86027E	030.35500E	030.67100E	030.31067E	030.18133E 04
0.12133E	050.22500E	050.10157E	010.10000E	030.24100E	000.80000E	01
0.58429E	020.96449E	020.27265E	040.10355E	040.19900E	040.39400E	030.12350E 04
0.29750E	050.52984E	050.10375E	010.10000E	030.11200E	000.72500E	01
0.54464E	020.93407E	020.36229E	040.11342E	040.18600E	040.33700E	030.13434E 04
0.40019E	050.45553E	050.10510E	010.10000E	030.16825E	000.67833E	01
0.56463E	020.93428E	020.81700E	030.21267E	030.69650E	030.65300E	030.91133E 03
0.18100E	050.32128E	050.10220E	010.10000E	030.24700E	000.72000E	01
0.99161E	020.16812E	030.14963E	040.52089E	030.21600E	040.39880E	030.20961E 04
0.19559E	050.37085E	050.10237E	010.87167E	020.24767E	000.71062E	01
0.97298E	020.16108E	030.34252E	040.79256E	030.14300E	040.31471E	030.20022E 04
0.32083E	050.60698E	050.10393E	010.10000E	030.12200E	000.67875E	01
0.99370E	020.15712E	030.21480E	040.48250E	030.11300E	040.30150E	030.20050E 04
0.22200E	050.42704E	050.10290E	010.10000E	030.16000E	000.66000E	01
0.10223E	030.16418E	030.17200E	040.52267E	030.20400E	040.22600E	030.24633E 04
0.25733E	050.63664E	050.10283E	010.10000E	030.92000E	010.73000E	01
0.11127E	030.16136E	030.29200E	040.78979E	030.18162E	040.24993E	030.20029E 04
0.33800E	050.58675E	050.10413E	010.10000E	030.10315E	000.69000E	01
0.10931E	030.15932E	030.29050E	040.72025E	030.50200E	040.22633E	030.20618E 04
0.43050E	050.79855E	050.10490E	010.10000E	030.80500E	010.70000E	01
0.11930E	030.15954E	030.26740E	040.79690E	030.18960E	040.30350E	030.19555E 04
0.30994E	050.55383E	050.10372E	010.10000E	030.10850E	000.73750E	01
0.11837E	030.15652E	030.24160E	040.79000E	030.11413E	040.30967E	030.13868E 04
0.24680E	050.43436E	050.10300E	010.10000E	030.16000E	000.80000E	01
0.11848E	030.15152E	030.27013E	040.72767E	030.16300E	040.27400E	030.25000E 04
0.30524E	050.51592E	050.10367E	010.10000E	030.11550E	000.55000E	01
0.91297E	020.10191E	030.14541E	040.48283E	030.67700E	030.42300E	030.18155E 04
0.19300E	050.23943E	050.10238E	010.10000E	030.18025E	000.72900E	01
0.87563E	020.13201E	030.29075E	040.66888E	030.76000E	030.55750E	030.20983E 04
0.34313E	050.40925E	050.10366E	010.85333E	020.16067E	000.68000E	01
0.69437E	020.12535E	030.20175E	040.58663E	030.83000E	030.35200E	030.14800E 04
0.23025E	050.44365E	050.10260E	010.10000E	030.17833E	000.67571E	01
0.70470E	020.12236E	030.16155E	040.36800E	030.92200E	030.28100E	030.17850E 04
0.17425E	050.29627E	050.10185E	010.10000E	030.18100E	000.68000E	01
0.66472E	020.12231E	030.26900E	040.87800E	030.19300E	040.55400E	030.13080E 04
0.27950E	050.48370E	050.10320E	010.10000E	030.92000E	010.75000E	01
0.71481E	020.12137E	030.24150E	040.58175E	030.16100E	040.52350E	030.16913E 04
0.23150E	050.41237E	050.10282E	010.10000E	030.11700E	000.69500E	01
0.68494E	020.12033E	030.65500E	040.34375E	040.92400E	030.36200E	030.16000E 04
0.26800E	050.50939E	050.10345E	010.10000E	030.16100E	000.60000E	01
0.74443E	020.12440E	030.19907E	040.55186E	030.10300E	040.66033E	030.18176E 04
0.20530E	050.37592E	050.10259E	010.10000E	030.15600E	000.74000E	01
0.74456E	020.12340E	030.30800E	040.18945E	040.11000E	040.54200E	030.25000E 04
0.52350E	050.96456E	050.10630E	010.10000E	030.14500E	000.60000E	01
0.76454E	020.12343E	030.23900E	040.71950E	030.11300E	040.57300E	030.27600E 04
0.25850E	050.47059E	050.10315E	010.10000E	030.13200E	000.75000E	01
0.73481E	020.12139E	030.22913E	040.64029E	030.10700E	040.44475E	030.29460E 04
0.34130E	050.43943E	050.10394E	010.10000E	030.14500E	000.71667E	01
0.72493E	020.12038E	030.21766E	040.57620E	030.97300E	030.47480E	030.22931E 04
0.21620E	050.37076E	050.10253E	010.10000E	030.15500E	000.71750E	01
0.80316E	020.13348E	030.52650E	040.10600E	040.63900E	030.43300E	030.15000E 04
0.45245E	050.22823E	050.10570E	010.10000E	030.23400E	000.68000E	01
0.82324E	020.13251E	030.18871E	040.48200E	030.76700E	030.65550E	030.24150E 04
0.14268E	050.24197E	050.10157E	010.10000E	030.24000E	000.64667E	01
0.83336E	020.13152E	030.14000E	040.46300E	030.82100E	030.33600E	030.29850E 04
0.34200E	050.27379E	050.10385E	010.10000E	030.19900E	000.66000E	01
0.80438E	020.12448E	030.30325E	040.69850E	030.22650E	040.54800E	030.25500E 04
0.33133E	050.65701E	050.10363E	010.10000E	030.10400E	000.68875E	01
0.78479E	020.12146E	030.28145E	040.77362E	030.27430E	050.53867E	030.29336E 04

0.37096E	050.64178E	050.10431E	010.10000E	030.10218E	000.70170E	01
0.79478E	020.12147E	030.22748E	040.58417E	030.11550E	040.52567E	030.24571E 04
0.27108E	050.48959E	050.10313E	010.10000E	030.13112E	000.70500E	01
0.85143E	020.14455E	030.19944E	040.62092E	030.15900E	040.68833E	030.31876E 04
0.31053E	050.52371E	050.10385E	010.10000E	030.11900E	000.67500E	01
0.84391E	020.12754E	030.24225E	040.75025E	030.10287E	040.48617E	030.13804E 04
0.26701E	050.38003E	050.10310E	010.10000E	030.15675E	000.67833E	01
0.84419E	020.12554E	030.32920E	040.13046E	040.15800E	040.12600E	030.15056E 04
0.33560E	050.61317E	050.10414E	010.10000E	030.11300E	000.72500E	01
0.64258E	020.79407E	020.24664E	040.77057E	030.21600E	040.34279E	030.22729E 04
0.24064E	050.32477E	050.10280E	010.10000E	030.61333E	-010.76763E	01
0.65266E	020.78419E	020.14933E	040.50133E	030.72400E	030.31400E	030.38100E 04
0.26441E	050.58873E	050.10330E	010.10000E	030.14600E	000.65500E	01
0.65291E	020.76419E	020.14800E	040.36600E	030.69000E	030.44500E	030.18060E 04
0.13200E	050.24817E	050.10165E	010.10000E	030.26100E	000.75000E	01
0.71162E	020.84497E	020.18811E	040.87531E	030.10700E	040.40260E	030.14046E 04
0.34623E	050.63217E	050.10398E	010.82800E	020.17960E	000.70250E	01
0.66199E	020.83431E	020.32420E	040.10907E	040.88100E	030.46500E	030.13767E 04
0.36108E	050.74880E	050.10413E	010.10000E	030.19300E	000.72500E	01
0.67220E	020.81444E	020.15148E	040.42939E	030.81800E	030.55088E	030.21116E 04
0.20179E	050.31762E	050.10377E	010.10000E	030.18700E	000.74961E	01
0.67233E	020.80444E	020.12250E	040.39225E	030.91800E	030.48300E	030.17525E 04
0.14900E	050.27775E	050.10183E	010.10000E	030.18100E	000.75000E	01
0.69318E	020.73471E	020.15273E	040.39367E	030.78700E	030.60600E	030.20470E 04
0.17683E	050.30755E	050.10215E	010.10000E	030.19800E	000.73750E	01
0.69371E	020.69471E	020.17335E	040.46250E	030.97300E	030.15700E	030.27450E 04
0.20700E	050.31795E	050.10235E	010.10000E	030.17700E	000.70500E	01
0.74076E	020.89538E	020.41995E	040.82025E	030.15100E	040.30500E	030.85750E 03
0.42475E	050.49034E	050.10550E	010.10000E	030.97000E	-010.68250E	01
0.75099E	020.87553E	020.21575E	040.82100E	030.12767E	040.38933E	030.16155E 04
0.23100E	050.38604E	050.10272E	010.95000E	020.16125E	000.70000E	01
0.76093E	020.87567E	020.19500E	040.52475E	030.10400E	040.42500E	030.22650E 04
0.22925E	050.34189E	050.10267E	010.82667E	020.19500E	000.76000E	01
0.74133E	020.85539E	020.20325E	040.71750E	030.15695E	040.41085E	030.20633E 04
0.25864E	050.45871E	050.10255E	010.95182E	020.16509E	000.73600E	01
0.76123E	020.85568E	020.16950E	040.55300E	030.11000E	040.35000E	030.21250E 04
0.19150E	050.35823E	050.10245E	010.85000E	020.19250E	000.75000E	01
0.73166E	020.83525E	020.20233E	040.57200E	030.12120E	040.43783E	030.18000E 04
0.24167E	050.41629E	050.10283E	010.10000E	030.14460E	000.75000E	01
0.77147E	020.83583E	020.28998E	040.72233E	030.10900E	040.24025E	030.26633E 04
0.25888E	050.55420E	050.10313E	010.10000E	030.14400E	000.59375E	01
0.75171E	020.82553E	020.17800E	040.41900E	030.11650E	040.20300E	030.25050E 04
0.20575E	050.36704E	050.10222E	010.10000E	030.17000E	000.68500E	01
0.73180E	020.82525E	020.22335E	040.49500E	030.99400E	030.51400E	030.19000E 04
0.19225E	050.33489E	050.10490E	010.10000E	030.17000E	000.75000E	01
0.74190E	020.81539E	020.21650E	040.60000E	030.14200E	040.26150E	030.26500E 04
0.21200E	050.40414E	050.10280E	010.10000E	030.14450E	000.70000E	01
0.73223E	020.79525E	020.14800E	040.39650E	030.83600E	030.44800E	030.22700E 04
0.15800E	050.30268E	050.10205E	010.10000E	030.19200E	000.75000E	01
0.75316E	020.72554E	020.14433E	040.45700E	030.10500E	040.56500E	030.19600E 04
0.17700E	050.31582E	050.10213E	010.10000E	030.16000E	000.75000E	01
0.73434E	020.64527E	020.19000E	040.44900E	030.11400E	040.43400E	030.27000E 04
0.24475E	050.35919E	050.10367E	010.10000E	030.13325E	000.72000E	01
0.72435E	020.64513E	020.24600E	040.57500E	030.12200E	040.42900E	030.22650E 04
0.26750E	050.48107E	050.10330E	010.10000E	030.12500E	000.70000E	01
0.83039E	020.88674E	020.33160E	040.14090E	040.86300E	030.26600E	030.24429E 04
0.34263E	050.62316E	050.10411E	010.86667E	020.11433E	000.71208E	01
0.79184E	020.80613E	020.18750E	040.68375E	030.12300E	040.49133E	030.34275E 04
0.28718E	050.56991E	050.10391E	010.69333E	020.17400E	000.70455E	01
0.86171E	020.79724E	020.27500E	040.62333E	030.12850E	040.38850E	030.23267E 04
0.32767E	050.40969E	050.10367E	010.10000E	030.14850E	000.72000E	01

9.0E25

FACTOR ANALYSIS OF ARBUCKLE BRINE DATA.

NUMBER OF SAMPLES EXAMINED = 122

VARIABLE NUMBER	MINIMUM VALUE	MAXIMUM VALUE	MEAN	STANDARD ERROR OF MEAN
1	273.2500000	6550.0000000	2255.6043701	90.4923534
2	167.3299999	3437.5000000	666.9003754	33.7884774
3	484.0000000	27430.0000000	1433.3737335	221.3325558
4	126.0000000	1432.0000000	415.6301994	14.3571125
5	50.0000000	3810.0000000	1897.8546906	63.5190010
6	7665.0000000	68236.0000000	26361.5737305	881.7889252
7	14494.0000000	96456.0000000	43556.0898437	1500.3942719
8	0.9829400	1.0760000	1.0310697	0.0011189
9	69.3330002	100.0000000	98.7389221	0.4067703
10	0.0613330	0.3390000	0.1646294	0.0051083
11	5.5000000	8.0000000	7.0629427	0.0386358

FACTOR ANALYSIS OF ARBUCKLE BRINE DATA.

VARIABLE NUMBER	STANDARD DEVIATION	VARIANCE	COEFFICIENT OF VARIATION
1	999.5207214	999041.6718750	0.443128E 02
2	373.2059364	139282.6699219	0.559613E 02
3	2444.6979980	5976548.2500000	0.170556E 03
4	158.5794926	25147.4553223	0.381540E 02
5	701.5903015	492228.9492187	0.369675E 02
6	9739.6771240	4861310.0000000	0.369465E 02
7	16572.3964844	4644324.0000000	0.380484E 02
8	0.0123588	0.0001527	0.119864E 01
9	4.4929244	20.1863694	0.455031E 01
10	0.0564229	0.0031835	0.342727E 02
11	0.4267461	0.1821122	0.604204E 01

	EIGENVALUE	PERCENT
1	4.3333752	39.3943195
2	1.3347967	51.5288348
3	1.1569419	62.0464878
4	1.0617283	71.6985626
5	0.8906040	79.7949629
6	0.7346410	86.4735174
7	0.5183883	91.1861382
8	0.4785199	95.5363188
9	0.2772021	98.0563374
10	0.1253838	99.1961899
11	0.0884105	99.9999208

EIGENVECTORS

VECTOR 1	0.416347	0.359419	0.135812	-0.099053	0.121448	0.434795	0.380415	0.405947	-0.017733	-0.346526
VECTOR 2	-0.276296	-0.295874	0.397028	-0.043072	0.597853	-0.083660	0.245765	-0.050012	-0.317075	-0.282026
VECTOR 3	0.047022	-0.104661	0.077496	-0.619472	-0.327850	-0.050470	0.017060	-0.045686	0.361443	-0.341223
VECTOR 4	-0.043559	-0.078736	0.528828	0.456103	-0.023643	-0.004136	0.023673	-0.032829	0.693628	-0.083665
VECTOR 5	0.053793	0.071215	0.282243	0.406063	-0.440511	0.152104	-0.031989	0.229164	-0.368531	0.109816
VECTOR 6	0.093640	0.081140	0.672125	-0.398922	-0.194215	-0.069604	-0.181628	-0.147734	-0.266477	0.261272
VECTOR 7	-0.160991	-0.674688	-0.024680	-0.145177	-0.078942	0.388515	-0.080104	0.513187	0.047626	0.200113
VECTOR 8	-0.274692	-0.178490	-0.070674	0.095641	-0.514855	-0.068556	0.609541	-0.218256	-0.181625	-0.244813
VECTOR 9	-0.322729	0.301981	0.026962	-0.197121	0.094485	-0.013455	0.513831	0.141158	0.210299	0.628123
VECTOR 10	-0.405224	0.268826	0.022663	-0.025929	-0.085899	-0.497983	-0.198281	0.611682	-0.032117	-0.268065
VECTOR 11	0.602219	-0.322406	-0.000835	0.052715	0.019868	-0.607945	0.280579	0.223879	0.007101	0.176967

EIGENVECTORS

VECTOR 1	-0.188458									
VECTOR 2	0.263114									
VECTOR 3	0.487441									
VECTOR 4	-0.108342					VECTOR 8		-0.310919		
VECTOR 5	0.573486					VECTOR 9		0.182340		
VECTOR 6	-0.370277					VECTOR 10		-0.147248		
VECTOR 7	-0.167110					VECTOR 11		0.020003		

FACTOR MATRIX (4 FACTORS)

1	0.8667	-0.3192	0.0506	-0.0655
2	0.7482	-0.3418	-0.1126	-0.0811
3	0.2827	0.4587	0.0834	0.5449
4	-0.2062	-0.0498	-0.6663	0.4700
5	0.2528	0.6907	-0.3526	-0.0244
6	0.9051	-0.0967	-0.0543	-0.0043
7	0.7919	0.2839	0.0184	0.0244
8	0.8451	-0.0578	-0.0491	-0.0338
9	-0.0369	-0.3663	0.3888	0.7147
10	-0.7214	-0.3258	-0.3670	-0.0862
11	-0.3923	0.3040	0.5243	-0.1116

ITERATION VARIANCES

0	0.2836372
1	0.3825061
2	0.3960123
3	0.4096015
4	0.4203899
5	0.4210678
6	0.4210906
7	0.4210910
8	0.4210910
9	0.4210910
10	0.4210910
11	0.4210910

ROTATED FACTOR MATRIX (4 FACTORS)

					6	0.8823	0.2236	0.0249	-0.0501
1	0.9175	0.0233	0.0994	0.0872	7	0.6404	0.4919	0.1326	-0.1974
2	0.8303	-0.0611	-0.0491	0.0191	8	0.8157	0.2159	0.0445	-0.0839
3	0.0498	0.7553	-0.0722	0.1264	9	-0.0167	0.1703	-0.0705	0.8736
4	-0.1639	0.0852	-0.8214	0.0315	10	-0.5240	-0.5751	-0.4042	0.0027
5	0.0388	0.5409	-0.1412	-0.5933	11	-0.5025	0.0903	0.5205	0.0459

CHECK ON COMMUNALITES

1	0.8599128	0.8599125	0.0000003
2	0.6958980	0.6958977	0.0000002
3	0.5942043	0.5942037	0.0000006
4	0.7098357	0.7098356	0.0000002
5	0.6659581	0.6659576	0.0000005
6	0.8315182	0.8315178	0.0000004
7	0.7086591	0.7086586	0.0000004
8	0.7210081	0.7210078	0.0000003
9	0.7975201	0.7975194	0.0000007
10	0.7686601	0.7686601	0.0000000
11	0.5336627	0.5336625	0.0000002

FACTOR ANALYSIS OF ARBUCKLE BRINE DATA,

OBLIQUE PROJECTION MATRIX 1

1	1.0000	=0.0000	=0.0000	0.0000
3	-0.0000	1.0000	=0.0000	=0.0000
4	-0.0000	0.0000	1.0000	0.0000
9	-0.0000	=0.0000	=0.0000	1.0000
2	0.9440	=0.1174	0.1896	=0.0622
5	0.0092	0.8806	0.1655	=0.8134
6	0.9550	0.3030	0.0756	=0.1992
7	0.6303	0.7330	=0.1160	=0.3907
8	0.8762	0.3055	0.0447	=0.2293
10	-0.4335	=0.8362	0.5004	0.1497
11	-0.6892	0.1978	=0.7447	0.1196

KANSAS GEOLOGICAL SURVEY COMPUTER PROGRAM
THE UNIVERSITY OF KANSAS, LAWRENCE

PROGRAM ABSTRACT

Title (If subroutine state in title):

R-mode factor analysis program in FORTRAN II for the IBM 1620 computer

Date: _____

Author, organization: Robert J. Sampson, Idaho State University, Pocatello, Idaho

Direct inquiries to: Author, or

Name: John C. Davis

Address: Kansas Geological Survey

Lawrence, Kansas 66044

Purpose/description: Completes R-mode factor analysis for 20 variables and performs verimax and oblique projections.

Mathematical method: Principal components solution.

Restrictions, range: Accepts samples having up to 30 variables. Up to 20 may be factored, and up to 14 may be rotated. Any number of samples may be entered.

Computer manufacturer: IBM Model: 1620 Model 1

Programming language: PDQ FORTRAN

Memory required: 20 K Approximate running time: 3 1/2 hours for 20 variables

Special peripheral equipment required: none

Remarks (special compilers or operating systems, required word lengths, number of successful runs, other machine versions, additional information useful for operation or modification of program) _____

Requires PDQ FORTRAN Processor C2 without reread (IBM User's Group Program 2.0.031). FORTRAN IV versions available for IBM 1130 and GE 625 computers.

Q-MODE FACTOR ANALYSIS PROGRAM IN FORTRAN IV FOR SMALL COMPUTERS

by

J. E. Klován

University of Calgary

INTRODUCTION

Q-mode factor analysis is a multivariate quantitative technique that may be used to study and portray the interrelationships between geologic items such as rock samples, fossil collections, etc. The technique has been applied recently to geologic problems by Harbaugh and Demirmen (1964), Imbrie and Van Andel (1964), Manson and Imbrie (1964), and Klován (1966), to name only a few. These authors have presented detailed descriptions of the method and its application.

Although programs for performing Q-mode factor analysis have been published previously (Imbrie, 1963; Manson and Imbrie, 1964), these programs are designed for large computers and require considerable effort to convert to small machines. The program described here is being used currently on an IBM System/360 Model 30 but is adapted easily to other computers. It has been written in a low-level subset of FORTRAN IV which allows its use on practically all IBM System/360 machines, and with modification of input-output statements, on the IBM 1620 as well.

PROGRAM DESCRIPTION

Size Restrictions and Data Format

A maximum of 60 items and 60 properties can be analyzed at one time (expansion of these size restrictions for larger machines is discussed later). The data are read in with items as rows of the data matrix and variables or properties as columns. Statement 52 of the main program controls the input format of data. The first 12 columns of a data card are reserved for identification purposes. Format statement 52 must always begin with 3A4.

A maximum of ten factors can be extracted by this program.

Machine Requirements

The version of the program listed here requires 64K memory with two scratch tapes or equivalent working area on disk. It has been run under the standard IBM DOS system and should be compatible with BOS and OS systems.

Operating Procedure

Two control cards precede the data deck:

Card 1. Columns 1-60. Any alphanumeric information.

Card 2. Columns 1- 2. NV = number of items (rows) in data matrix (maximum of 60).

Columns 3- 6. NS = number of variables (columns) in data matrix (maximum of 60).

Columns 7-11. QUIT = stopping criterion (usually set at 99.0).

The data deck follows the control cards. Because geological data seldom are obtained in a specific format, it may be most convenient to leave the main program in source form, change statement 52 to comply with the format of the data, and recompile with each run. If data need to be transformed by, for example, conversion to logarithms, additional FORTRAN statements may be added to the main program at the appropriate place.

Computational Methods

The main program reads in control cards and data. Means of the row vectors of data matrix X are computed as are square roots of the sums of squares, which are the lengths of the row vectors. A matrix of $\cos\theta$ is next computed according to the equation

$$XX' = S,$$

or in scalar form

$$S_{kl} = \frac{\sum_{i=1}^n X_{ki} X_{li}}{\sqrt{\sum_{i=1}^n X_{ki}^2 \sum_{i=1}^n X_{li}^2}},$$

where n equals the number of variables, and where S_{kl} is the cosine of the angle between row vectors k and l . The results of these computations are listed with appropriate labels. Row vectors then are normalized by dividing each element of each row by the row vector length and are stored on tape for computation of factor scores.

Subroutine PRINCP

The eigenvalues and eigenvectors of the $\cos\theta$ matrix are extracted sequentially using a modified Hotelling iterative procedure. After each eigenvalue is extracted, the cumulative sum of squares

accounted for is compared with the stopping criterion QUIT. Extraction of eigenvalues is terminated when QUIT is achieved, when 10 eigenvalues have been extracted, or when any eigenvalue is less than 0.01. The principal component factor matrix is listed and punched.

Subroutine VARMAX

The principal component factor matrix is rotated according to the standard varimax procedure for all principal factors extracted. Then, the last factor is deleted and remaining ones rotated. This process is continued until only two factors remain.

In the case of two and three factors, the varimax matrix is converted to factor components by squaring each element. This matrix is row normalized, resulting in normalized factor components which can be plotted directly on 3-component diagrams.

Subroutine FACSCO

This subroutine computes factor scores for each of the varimax matrices, according to the equation

$$F = Z A \Lambda^{-1} T ,$$

where F is the varimax factor score matrix, Z is the row normalized data matrix, A is the principal com-

ponent factor matrix, Λ is the diagonal matrix of eigenvalues, and T is the varimax transformation matrix.

The column vectors of F show the relative amount of each variable in each factor. These numbers are pseudostandardized and should be used in a qualitative way only. A value of zero indicates that the factor contains roughly an average amount of that variable, a +1.0 means that the factor contains roughly one standard deviation above the average of that variable.

CONVERSION TO OTHER MACHINES

If a large computer is available, DIMENSION statements in the main program and each subroutine may be changed. All array and matrix sizes are determined by the maximum number of items and the maximum number of factors.

A version of this program, adapted for use on an IBM System/360 Model 40 with a 256K memory, can treat 200 samples at once. It should be emphasized that matrices larger than 90 x 90 cannot be handled under DOS and OS must be used. A version modified for the IBM 1620 can treat 40 samples at a time. This modification entails changing of all input-output statements to 1620-compatible format as well as changing the DIMENSION statements.

REFERENCES

- Harbaugh, J. W., and Demirmen, F., 1964, Application of factor analysis to petrologic variations of Americus Limestone (Lower Permian), Kansas and Oklahoma: Kansas Geol. Survey Sp. Dist. Publ. 15, 40 p.
- Imbrie, J., 1963, Factor and vector analysis programs for analyzing geologic data: Office of Naval Research, Geography Branch, ONR Task No. 389-135, Tech. Rpt. No. 6, 83 p.
- Imbrie, J., and Van Andel, T. H., 1964, Vector analysis of heavy mineral data: Geol. Soc. America Bull., v. 75, no. 11, p. 1131-1155.
- Klovan, J. E., 1966, The use of factor analysis in determining depositional environments from grain-size distributions: Jour. Sed. Pet., v. 36, no. 1, p. 115-125.
- Manson, V., and Imbrie, J., 1964, FORTRAN program for factor and vector analysis of geologic data using an IBM 7090 or 7094/1401 computer system: Kansas Geol. Survey Sp. Dist. Publ. 13, 46 p.

C Q - MODE FACTOR ANALYSIS
 C CUS THETA PROGRAM

C THIS PROGRAM WRITTEN FOR THE IBM 360/30

C BY
 C J.E. KLOVAN
 C DEPARTMENT OF GEOLOGY
 C UNIVERSITY OF CALGARY

C-----
 C CONTROL CARD SET UP

C CARD 1.
 C COLS. 1-60 JOB TITLE
 C CARD 2.
 C COLS. 1-2 (12) NV= NUMBER OF ITEMS (ROWS) MAX OF 60.
 C COLS 3-6 (14) NS= NUMBER OF VARIABLES (COLS) MAX OF 60
 C COLS 7-11 (F5.2) QUIT= STOPPING CRITERION
 C-----

C NOTE.

C DATA MATRIX HAS ITEMS AS ROWS

C FIRST TWELVE COLUMNS OF DATA CARD RESERVED FOR ITEM IDENTIFICATION

C STATEMENT 52 CONTROLS INPUT FORMAT

C DIMENSIONING, READING CONTROL CARD AND INITIALIZATION

C DIMENSION X(60),S(60),XX(60, 60),TITLE(15)
 C DIMENSION NAME(60,3)
 C COMMON X,S,NV,NS,TITLE ,NAME
 C REWIND 4
 C 1 READ(1,59) (TITLE(I), I = 1,15)
 C 59 FORMAT(15A4)
 C WRITE(3,60) (TITLE(I),I = 1,15)
 C 60 FORMAT(1H1,15A4)
 C READ(1,51) NV,NS, QUIT
 C 51 FORMAT(I2,I4,F5.2)
 C VN = NV
 C SN = NS
 C DO 2 I = 1, NV
 C S(I) = 0.
 C DO 2 J = 1, NV
 C 2 XX(I,J) = 0.
 C READ RAW DATA
 C DO 70 I = 1,NV
 C 70 READ(1, 52)(NAME(I,K), K = 1,3),(XX(I,J),J = 1,NS)
 C 52 FURMAT(3A4,10F3.1)

C TRANSFORMS CAN GO HERE

C PUT TRANSPOSED DATA MATRIX ON TAPE 4.

C DO 71 J = 1,NS
 C 71 WRITE(4) (XX(I,J), I = 1,NV)
 C REWIND 4
 C DO 75 I = 1,NV
 C DO 75 J = I,NV
 C 75 XX(I,J) = 0.0

C READING IN DATA AND COMPUTING SUMS AND RAW SUMS OF SQUARES AND PRODUCTS

C DO 3 K = 1, NS
 C READ(4) (X(I), I = 1,NV)

C TRANSFORMATIONS CAN GO HERE

C DO 3 I = 1, NV
 C S(I) = S(I) + X(I)
 C DO 3 J = I, NV
 C XX(I,J) = XX(I,J) + X(I) * X(J)
 C 3 XX(J,I) = XX(I,J)

```

C
C
WRITE(3,51)
WRITE(3,53) NV,NS
53 FORMAT(1H0,21HNUMBER OF SAMPLES = 13,15X,
120HNUMBER OF VARS. N=15,///,37H MEANS AND SUM OF SQUARES
2 //,8X,9H SAMPLE 14X4HMEAN 11X8HVECTOR /,8X,7H NAME 29X9H L
3LENGTH /)
DO 4 I = 1,NV
X(I) = SQRT (XX(I,I))
S(I) = S(I) / SN
4 WRITE(3,55) I, (NAME(I,J), J = 1,3), S(I), X(I)
55 FORMAT(1H ,15,2X,3A4,2F17.4)
C
C
COMPUTING COS THETA MATRIX
11 DO 12 I = 1, NV
DO 12 J = I, NV
XX(I,J) = XX(I,J) / (X(I) * X(J))
12 XX(J,I) = XX(I,J)
C
C
PRINTING COS THETA MATRIX
84 WRITE(3,56)
58 FORMAT(///, ' COS THETA MATRIX ' )
6 DO 10 K= 1, NV, 15
L = K + 14
7 IF(NV - L ) 8,9,9
8 L = L - 1
GO TO 7
9 WRITE(3,56)(J,J = K,L)
56 FORMAT(1H0,7X,12HSAMPLES ,3X,15(15,2X),/ )
DO 10 I = 1, NV
10 WRITE(3,57) I, (NAME(I,JK), JK=1,3), (XX(I,J), J=K,L)
57 FORMAT(1H ,15,2X,3A4,3X,15F7.3 )
C
DO 72 I = 1, NV
72 X(I) = SQRT((X(I)* X(I))/ SN)
REWIND 4
C
C
NORMALIZE DATA AND PUT ON TAPE 5
REWIND 5
DO 73 I= 1,NS
READ(4) (S(J), J=1,NV)
DO 74 J= 1,NV
74 S(J) = S(J)/ X(J)
73 WRITE(5)(S(J),J=1,NV)
REWIND 4
REWIND 5
IF(QUIT)40,40,41
41 CALL PRINCP(XX,QUIT)
40 CALL EXIT
50 FORMAT(1H1)
54 FORMAT(15,F17.4,F14.4)
END

```



```

C
C   GO BACK AND GET NEXT EIGENVALUE
C
114 GO TO 102
201 WRITE(3,301)
301 FORMAT(1H0,35H PRINCIPAL COMPONENT FACTOR MATRIX //)
   WRITE(3,700) ( J, J = 1,NF)
700 FORMAT(1H0,22X,'COMM.',4X,10(15,4X),/ )
   DO 600 L = 1,MAX
600   CUM(L) = 0.0
   DO 601 L = 1,MAX
   DO 601 K = 1,NF
601   COM(L) = COM(L) + F(L,K)*F(L,K)
   DO 305 I = 1,MAX
   WRITE(2,802) I,(NAME(I,JK),JK=1,3),(F(I,J),J=1,NF)
802   FORMAT(15,2X,3A4,10F6.3)
C
C   PUT PRINC. COMP. MATRIX ON 4
C
   WRITE(4)(F(I,J), J=1,NF)
305   WRITE(3,311) I,(NAME(I,JK),JK=1,3),COM(I),(F(I,J),J=1,NF)
311   FORMAT(1H ,15,2X,3A4,11F9.4)
   DO 499 I = 1,NF
499   CUM(I) = 0.
   VAR(I) = 0.
   FN = MAX
   DO 500 I = 1,NF
   DO 500 J = 1,MAX
500   VAR(I) = VAR(I) + F(J,I) * F(J,I)
   DO 505 I = 1,NF
505   VAR(I) =(VAR(I)/FN) * 100.
   CUM(I) = VAR(I)
   DO 501 I = 2,NF
501   CUM(I) = CUM(I -1) + VAR(I)
   WRITE(3,502) (VAR(I), I = 1,NF)
502   FORMAT(1H0,19X,8HVARIANCE,3X,10(F7.3 ,2X))
   WRITE(3,503)(CUM(I), I = 1,NF)
503   FORMAT(1H0,19X,8HCUM. VAR,3X,10(F7.3 ,2X))
   NZ = 1
   DO 850 I=1,NF
850   VAR(I)=(VAR(I) * FN)/100.
C
C   PUT EIGENVALUES ON TAPE 4
   WRITE(4)(VAR(I),I=1,MAX)
C
C   ROTATE NF FACTORS FIRST TIME, THEN DROP OFF THE LAST ONE UNTIL HAVE
C   ONLY TWO LEFT.
C
   ITER =0
800   CALL VARMAX(F,NF,COM,VAR,CUM,ITER)
   ITER = ITER+1
   NF = NF - 1
   IF( NF - 2) 801,800,800
801   RETURN
   END

```

4051


```

SUBROUTINE VARMAX(FF,MAXF,CGM,VAR,CUM,ITER)
VARIMAX MATRIX ROTATION
1001
C
C
C
C
T MAXT = NO. OF SAMPLES, NS = NO. OF VARIABLES, MAXF = NO. OF FACTORS
WILL CONTAIN THE VARIMAX TRANSFORMATION MATRIX
DIMENSION F(60,10),COM(60),VAR(10),CUM(10), DUM(120),TITLE(15)
1,FF(60,10),NAME(60,3)
DIMENSION T(10,10)
COMMON DUM,MAXT,NS,TITLE ,NAME
1 FORMAT(2I4)
2 FORMAT(4X 10F7.4 )
DO 800 N = 1,MAXT
DO 800 M = 1,MAXF
800 F(N,M) = FF(N,M)
DO 801 I=1,MAXF
DO 801 J=1,MAXF
IF(I-J) 803,802,803
802 T(I,J) = 1.0
GO TO 801
803 T(I,J) = 0.0
801 CONTINUE
EPS = 0.06993
150 DO 103 N = 1, MAXT
COM(N) = 0.0
DO 102 M = 1, MAXF
102 COM(N) = CGM(N) + F(N,M) * F(N,M)
COM(N) = SQRT (COM(N) )
DO 103 M = 1, MAXF
103 F(N,M) = F(N,M)/COM(N)
L = MAXF - 1
104 NORCT = 0
DO 123 M = 1, L
K = M + 1
DO 123 MONE = K, MAXF
A = 0.0
B = 0.0
C = 0.0
D = 0.0
DO 105 N = 1, MAXT
U = F(N,M)**2 - F(N,MONE) **2
V = F(N,M) * F(N,MONE)* 2.
A = A + U
B = B + V
C = C + U ** 2 - V ** 2
105 D = D + U * V * 2.0
R = MAXT
QNUM = D - 2.0 * A * B / R
QDEN = C - (A ** 2 - B ** 2) / R
IF(ABS(QNUM) + ABS(QDEN)) 120,120,106
IF(ABS(QNUM) - ABS(QDEN)) 107,114,111
106 R = ABS(QNUM/QDEN)
107 IF(R - EPS) 109,108,108
108 CS4TH = COS(ATAN(R))
SN4TH = SIN(ATAN(R))
GO TO 115
109 IF(QDEN) 110,120,120
110 SNPHI = .70710678
CSPHI = SNPHI
GO TO 121
111 R = ABS(QDEN/QNUM)
IF(R - EPS) 113,112,112
112 SN4TH = 1.0/ SQRT(1.0 + R ** 2)
CS4TH = SN4TH * R
GO TO 115
113 CS4TH = 0.0
SN4TH = 1.0
GO TO 115
114 CS4TH = .70710678
SN4TH = CS4TH
115 R = SQRT((1.0 + CS4TH) * 0.5)
CSTH = SQRT((1.0 + R) * 0.5)
SNTH = SN4TH/(4.0 * CSTH * R)
IF(QDEN) 116,117,117
116 CSPHI = .70710678*(CSTH+SNTH)
SNPHI = .70710678*(CSTH-SNTH)
GO TO 118
117 CSPHI = CSTH
1009
1010
1011
1017
1018
1019
1020
1021
1022
1023
1024
1025
1026
1029
1030
1031
1032
1033
1034
1035
1036
1037
1038
1039
1040
1041
1042
1043
1044
1045
1046
1047
1048
1049
1050
1051
1052
1053
1054
1055
1056
1057
1058
1059
1060
1061
1062
1063
1064

```

```

118   SNPFI = SNTH
119   IF(CNUM) 119,121,121
119   SNPFI = - SNPFI
120   GO TO 121
120   NOROT = NOROT + 1
120   GO TO 123
121   DO 123 N = 1, MAXT
      R = F(N,M) * CSPHI + F(N,MONE) * SNPFI
      F(N,MONE) = F(N,MONE) * CSPHI - F(N,M) * SNPFI
      F(N,M) = R
121   IF(N-MAXF) 804,804,123
121   TP = T(N,M)
121   T(N,M) = TP * CSPHI + T(N,MONE) * SNPFI
121   T(N,MONE) = -TP * SNPFI + T(N,MONE) * CSPHI
123   CONTINUE
124   IF(NOROT - (MAXF * L)/2) 104,124,104
124   DO 125 N = 1, MAXT
124   DO 127 M = 1, MAXF
127   F(N,M) = F(N,M) * CUM(N)
125   CUM(N) = CUM(N) ** 2
124   WRITE(3,60) (TITLE(I), I = 1,15)
124   FORMAT(1H1,15A4)
124   WRITE(3,30)
124   FORMAT(22HOVARIMAX FACTOR MATRIX //)
124   WRITE(3,40) (J,J = 1,MAXF)
124   FORMAT(1H0,22X,'CUMM.',4X,10(I5,4X),/ )
124   DO 126 N = 1, MAXT
126   WRITE(3,20) N, (NAME(N,JK), JK=1,3), CUM(N), (F(N,M), M=1,MAXF)
124   DO 200 I = 1, MAXF
200   VAR(I) = 0.
200   CUM(I) = 0.
200   FN = MAXT
200   DO 201 I = 1, MAXF
200   DO 201 J = 1, MAXT
201   VAR(I) = VAR(I) + F(J,I) * F(J,I)
200   DO 500 I = 1, MAXF
500   VAR(I) = (VAR(I)/ FN) * 100.
200   CUM(I) = VAR(I)
200   DO 202 I = 2, MAXF
202   CUM(I) = CUM(I-1) + VAR(I)
202   WRITE(3,502) (VAR(I), I = 1,MAXF)
502   FORMAT(1H0,19X,8HVARIANCE,3X,10(F7.3,2X))
202   WRITE(3,503) (CUM(I), I = 1,MAXF)
503   FORMAT(1H0,19X,8HCUM. VAR,3X,10(F7.3,2X))
C
C   IF ROTATING 3 OR 2 FACTORS, COMPUTE THE NORMALIZED FACTOR COMPONENTS
C
124   IF(MAXF - 3) 600,600,601
600   WRITE(3,60) (TITLE(I), I = 1,15)
600   WRITE(3,602)
602   FORMAT(1H0,' NORMALIZED VARIMAX FACTOR COMPONENTS ' )
602   WRITE(3,40) (J,J = 1,MAXF)
602   DO 603 N = 1, MAXT
602   DO 603 M = 1,MAXF
602   S = F(N,M)
602   F(N,M) = (F(N,M) * F(N,M))/CUM(N)
605   IF(S) 605,603,603
605   F(N,M) = -F(N,M)
603   CONTINUE
604   DO 604 N = 1,MAXT
604   WRITE(3,20) N, (NAME(N,JK), JK=1,3), CUM(N), (F(N,M), M=1,MAXF)
601   CALL FACSCO (MAXF,T,F,CUM,ITER )
100   RETURN
      END

```

1065
1066
1067
1068
1069
1070
1071

1075
1076
1077

1081

1084

C
C
C
C
C

```

SUBROUTINE FACSCD (M,T,A,X ,ITER)
COMPUTES FACTOR SCORES
M= NO. OF FACTORS , NV = NO. OF SAMPLES , NS = NO. OF VARIABLES
DIMENSION A( 60,10),X( 60),FACTSC(10),VAR(10),T(10,10)
DIMENSION TITLE(15),DUM(120),NAME( 60,3)
COMMON DUM,NV,NS,TITLE,NAME
REWIND 4
REWIND 5
WRITE(3,60) TITLE
60 FORMAT(1H1,15A4)
WRITE(3,51)
51 FORMAT(1H0,' VARIMAX FACTOR SCORE MATRIX ',//)
WRITE(3,52)(J,J=1,M)
52 FORMAT(1H0,25X,'FACTOR',10(15,4X))
WRITE(3,53)
53 FORMAT(1H0, 18X, 'VARIABLE' ,//)
IF(ITER) 6, 6,8
6 DO 5 I=1,NV
5 READ(4) (A(I,J),J=1,M)
READ(4)(VAR(I),I =1,M)
8 DO 40 LL=1,NS
REAL(5) (X(I),I=1,NV)
DO 30 J=1,M
25 FACTSC(J) = 0.
DO 30 I=1,NV
30 FACTSC(J) =(X(I)* A(I,J))+ FACTSC(J)
DO 80 II = 1,M
80 FACTSC(II) =FACTSC(II)/ VAR(II)
DO 70 I=1,M
X(I) = 0.0
DO 70 J=1,M
70 X(I) = X(I) + T(J,I) * FACTSC(J)
40 WRITE (3,62) LL, (X(J), J=1,M)
62 FURMAT(1H ,20X,15,3X,10F9.4)
REWIND 4
REWIND 5
RETURN
ENC
    
```

SAMPLE INPUT

CONTROL CARD 1:

Q MODE TEST PROBLEM AFTER IMBRIE AND VAN ANDEL

CONTROL CARD 2:

100010100.

DATA PUNCHED ACCORDING TO FORMAT : (3A4, 10F3.1)

LOC. 1	0502501500500502001000500500050
LOC. 2	100300170170080080050040010000
LOC. 3	030060100130250150130080050020
LOC. 4	075275160110065140075045030025
LOC. 5	046212140066090190106056050044
LOC. 6	038136120098170170118068050032
LCC. 7	083266159142091111068046022012
LOC. 8	061227146102099154091053038029
LOC. 9	076242152138108118076050026014
LOC.10	039103112126213148119073046021

Q MODE TEST PROBLEM AFTER IMBRIE AND VAN ANDEL

NUMBER OF SAMPLES = 10 NUMBER OF VARS. N= 10

MEANS AND SUM OF SQUARES

	SAMPLE NAME	MEAN	VECTOR LENGTH
1	LCC. 1	10.0000	38.7298
2	LCC. 2	10.0000	41.8091
3	LCC. 3	10.0000	37.7624
4	LCC. 4	10.0000	38.9808
5	LCC. 5	10.0000	36.6093
6	LCC. 6	10.0000	35.1875
7	LCC. 7	10.0000	38.8664
8	LCC. 8	10.0000	36.5871
9	LCC. 9	10.0000	37.5798
10	LCC.10	10.0000	36.0374

CGS THETA MATRIX

SAMPLES	1	2	3	4	5	6	7	8	9	10
1 LCC. 1	1.000	0.874	0.691	0.965	0.989	0.885	0.924	0.971	0.928	0.788
2 LCC. 2	0.874	1.000	0.648	0.970	0.873	0.802	0.990	0.939	0.978	0.753
3 LCC. 3	0.691	0.648	1.000	0.691	0.791	0.948	0.723	0.794	0.776	0.988
4 LCC. 4	0.965	0.970	0.691	1.000	0.960	0.870	0.990	0.986	0.986	0.795
5 LCC. 5	0.989	0.873	0.791	0.960	1.000	0.945	0.931	0.986	0.946	0.870
6 LCC. 6	0.885	0.802	0.948	0.870	0.945	1.000	0.872	0.939	0.908	0.983
7 LCC. 7	0.924	0.990	0.723	0.990	0.931	0.872	1.000	0.978	0.997	0.820
8 LCC. 8	0.971	0.939	0.794	0.986	0.986	0.939	0.978	1.000	0.987	0.879
9 LCC. 9	0.928	0.978	0.776	0.986	0.946	0.908	0.997	0.987	1.000	0.864
10 LCC.10	0.788	0.753	0.988	0.795	0.870	0.983	0.820	0.879	0.864	1.000

Q MODE TEST PROBLEM AFTER IMBRIE AND VAN ANDEL

FACTOR 1 EIGENV = 9.05213642 FOR 90.52 PER CENT
 FACTOR 2 EIGENV = 0.74166113 FOR 97.94 PER CENT
 FACTOR 3 EIGENV = 0.20639962 FOR 100.00 PER CENT

PRINCIPAL COMPONENT FACTOR MATRIX

	COMM.	1	2	3
1 LCC. 1	1.0001	0.9506	-0.1684	0.2610
2 LCC. 2	1.0000	0.9310	-0.2859	-0.2270
3 LCC. 3	0.9999	0.8419	0.5343	-0.0752
4 LCC. 4	1.0000	0.9715	-0.2370	0.0079
5 LCC. 5	1.0001	0.9782	-0.0323	0.2053
6 LCC. 6	1.0000	0.9606	0.2699	0.0665
7 LCC. 7	1.0000	0.9723	-0.1970	-0.1263
8 LCC. 8	1.0001	0.9961	-0.0769	-0.0448
9 LCC. 9	1.0000	0.9866	-0.1182	-0.1129
10 LCC.10	1.0000	0.9159	0.3966	-0.0613
	VARIANCE	90.521	7.417	2.064
	CUM. VAR	90.521	97.938	100.002

Q MODE TEST PROBLEM AFTER IMBRIE AND VAN ANDEL

VARIMAX FACTOR MATRIX

	COMM.	1	2	3
1 LOC. 1	1.0001	0.6607	0.3965	0.6375
2 LOC. 2	1.0000	0.9132	0.3518	0.2055
3 LOC. 3	0.9999	0.3090	0.9333	0.1827
4 LOC. 4	1.0000	0.8180	0.3857	0.4269
5 LOC. 5	1.0001	0.6229	0.5281	0.5772
6 LOC. 6	1.0000	0.4898	0.7755	0.3983
7 LOC. 7	1.0000	0.8494	0.4346	0.2996
8 LOC. 8	1.0000	0.7265	0.5231	0.4456
9 LOC. 9	1.0000	0.8079	0.5042	0.3053
10 LOC.10	1.0000	0.4360	0.8658	0.2455
	VARIANCE	47.548	36.476	15.977
	CUM. VAR	47.548	84.024	100.002

Q MODE TEST PROBLEM AFTER IMBRIE AND VAN ANDEL

NORMALIZED VARIMAX FACTOR COMPONENTS

	COMM.	1	2	3
1 LOC. 1	1.0001	0.4365	0.1572	0.4063
2 LOC. 2	1.0000	0.8340	0.1238	0.0422
3 LOC. 3	0.9999	0.0955	0.8711	0.0334
4 LOC. 4	1.0000	0.6690	0.1487	0.1822
5 LOC. 5	1.0001	0.3880	0.2789	0.3331
6 LOC. 6	1.0000	0.2399	0.6015	0.1586
7 LOC. 7	1.0000	0.7214	0.1889	0.0897
8 LOC. 8	1.0000	0.5278	0.2737	0.1985
9 LOC. 9	1.0000	0.6526	0.2542	0.0932
10 LOC.10	1.0000	0.1901	0.7497	0.0603

Q MODE TEST PROBLEM AFTER IMBRIE AND VAN ANDEL

VARIMAX FACTOR SCORE MATRIX

	FACTOR	1	2	3
VARIABLE				
1		0.8821	0.0346	-0.2956
2		2.4504	-0.4581	0.9455
3		1.1366	0.4271	0.4774
4		1.3324	0.9891	-1.3549
5		-0.1017	2.4238	-0.7589
6		-0.2062	0.9918	2.1590
7		-0.1788	1.0682	0.8027
8		0.0292	0.6698	0.1942
9		-0.2080	0.3984	0.6085
10		-0.2183	0.0938	0.8083

Q MODE TEST PROBLEM AFTER IMBRIE AND VAN ANDEL
 VARIMAX FACTOR MATRIX

		COMM.	1	2
1	LCC. 1	0.9320	0.8554	0.4474
2	LCC. 2	0.9485	0.9117	0.3424
3	LCC. 3	0.9943	0.3401	0.9373
4	LCC. 4	1.0000	0.9139	0.4059
5	LCC. 5	0.9579	0.7941	0.5720
6	LCC. 6	0.9956	0.5956	0.8005
7	LCC. 7	0.9841	0.8901	0.4381
8	LCC. 8	0.9980	0.8355	0.5477
9	LCC. 9	0.9873	0.8533	0.5092
10	LCC.10	0.9962	0.4828	0.8736
	VARIANCE		59.507	38.431
	CUM. VAR		59.507	97.938

Q MODE TEST PROBLEM AFTER IMBRIE AND VAN ANDEL
 NORMALIZED VARIMAX FACTOR COMPONENTS

		COMM.	1	2
1	LCC. 1	0.9320	0.7852	0.2148
2	LCC. 2	0.9485	0.8764	0.1236
3	LCC. 3	0.9943	0.1163	0.8837
4	LCC. 4	1.0000	0.8352	0.1648
5	LCC. 5	0.9579	0.6584	0.3416
6	LCC. 6	0.9956	0.3563	0.6437
7	LCC. 7	0.9841	0.8050	0.1950
8	LCC. 8	0.9980	0.6995	0.3005
9	LCC. 9	0.9873	0.7374	0.2626
10	LCC.10	0.9962	0.2340	0.7660

Q MODE TEST PROBLEM AFTER IMBRIE AND VAN ANDEL
 VARIMAX FACTOR SCORE MATRIX

	FACTOR	1	2
	VARIABLE		
1		-1.0063	1.9130
2		-3.2205	6.3397
3		-2.8025	4.9963
4		-2.6010	4.3957
5		-4.0371	6.1161
6		-3.5680	5.9300
7		-2.5828	4.1243
8		-1.5430	2.4671
9		-1.0399	1.6572
10		-0.5917	0.9920

KANSAS GEOLOGICAL SURVEY COMPUTER PROGRAM
THE UNIVERSITY OF KANSAS, LAWRENCE

PROGRAM ABSTRACT

Title (If subroutine state in title):

Q-mode factor analysis program in FORTRAN IV for small computers

Date: _____

Author, organization: J.E. Klován, Department of Geology, Univ. of Calgary, Calgary, Alberta

Direct inquiries to: Author, or

Name: D.F. Merriam Address: Kansas Geological Survey

Lawrence, Kansas 66044

Purpose/description: Computes Q-mode factor analysis and performs varimax rotation.

Mathematical method: Principal components of $\cos \theta$ similarity matrix.

Restrictions, range: Accepts up to 60 samples having up to 60 variables.

Computer manufacturer: IBM Model: System/360 Model 30

Programming language: FORTRAN IV

Memory required: 64 K Approximate running time: _____

Special peripheral equipment required: _____

Remarks (special compilers or operating systems, required word lengths, number of successful runs, other machine versions, additional information useful for operation or modification of program)

Operates under DOS, BOS, or OS systems. Versions exist for the IBM System/360 Model 40 which will handle up to 200 samples using OS, and for the IBM 1620 (40 K) which will accept up to 40 samples.

FORTRAN II PROGRAM FOR THE CALCULATION OF WILKS' Λ
USING AN IBM 1620 COMPUTER

by

S.V.L.N. Rao

Indian Institute of Technology

Analysis of variance is one of the most widely used statistical techniques in geology. The purpose of most applications has been to estimate the significance of differences between means of populations. This is done by measuring the variability of the attribute under examination; if the variance between groups is greater than the variance within groups, this is considered evidence that the groups are indeed different. There are many schemes for partitioning variance into its sources and for controlling extraneous influences on the attribute being studied. Various models and geologic applications are given in Chapter 9 of Krumbain and Graybill (1965).

These techniques are based on a univariate model. That is, only one attribute or variate may be compared at a time. Most geologic problems are multivariate, however, and the appropriate model should consider sets of observation in which all variances (and covariances) are considered simultaneously. A single multivariate test is more sensitive than a series of tests based on individual variates because correlations between variables are taken into account. A sequence of univariate tests may lead to ambiguous results, as in a case discussed by Miller and Kahn (1962, p. 250). Univariate tests made of several variates measured on two groups of fossil oreodonts found significant differences with some variates but not with others. This conflict did not arise in a multivariate approach.

Wilks' Λ criterion, also known as analysis of dispersion, is a widely applicable multivariate technique. The procedure was developed by Wilks (1932) and is extensively discussed by Rao (1952). Miller and Kahn (1962, p. 254-257) present a table of computational equations which have been rewritten into a more standard terminology in Table 1. Several errors in the original table have been corrected.

Wilks' Λ criterion is calculated as the ratio of determinants of the two matrices,

$$\Lambda = \frac{|SS_W|}{|SS_T|}$$

Λ may be considered a multivariate extension of the F-test of analysis of variance. The test statistic,

$$V = -m \ln \Lambda$$

is distributed as χ^2 with $i(j-1)$ degrees of freedom. In this equation, j is the number of groups, i is the number of variables, and

$$m = (\sum_i n_i - 1) - \frac{i+j}{2}$$

The hypothesis tested is one of equality of multivariate means or

$$H_0: \mu_{i1} = \mu_{i2} = \dots = \mu_{ij}$$

against the alternate

$$H_1: \text{Not all } \mu_{ij} \text{ are equal.}$$

PROGRAM DESCRIPTION

Earlier versions of the program followed the outline given by Miller and Kahn (1962); it has been revised subsequently into the present form. Up to 12 data groups may be used, each containing up to 10 variables and any number of observations. The number of samples need not be equal in each group. Data are not stored, but sums, squares, and cross-products are accumulated. Each card is counted as read in and the total number of observations accumulated as COUNT1. Register COUNT2 totals

Table 1.- Computational forms for sums of squares and products matrices on i observations in j groups. All possible combinations are computed except $j = j'$.

Sums of Squares	Symbol	Computational form
Between Groups	$[SS_B] =$	$(\sum x_{ij} \sum x_{ij} / n_i + \sum x_{i'j'} \sum x_{i'j'} / n_{i'}) - [(\sum x_{ij} + \sum x_{i'j'}) (\sum x_{ij} + \sum x_{i'j'}) / n_i + n_{i'}]$
Within Groups	$[SS_W] =$	$(\sum x_{ij} x_{ij} + \sum x_{i'j'} x_{i'j'}) - (\sum x_{ij} \sum x_{ij} / n_i + \sum x_{i'j'} \sum x_{i'j'} / n_{i'})$
Total	$[SS_T] =$	$(\sum x_{ij} x_{ij} + \sum x_{i'j'} x_{i'j'}) - \frac{(\sum x_{ij} + \sum x_{i'j'}) (\sum x_{ij} + \sum x_{i'j'})}{n_i + n_{i'}}$
	$SS_T = SS_W + SS_B$	

observations in each successive group. As soon as a group is read in, the means and variances are calculated. After all groups have entered the computer, the sums of sums are calculated and the matrices $[SS_W]$ and $[SS_T]$ established, the determinants are obtained using Crout's^{1/} method (Nielson, 1956, p. 181). Then, Λ and V are calculated and printed, with the accompanying degrees of freedom and a set of $\chi^2_{.95}$ values (Krumbein and Graybill, 1965, p. 418).

This program is designed for use on an IBM 1620 Model 2 computer with 40K core storage, automatic divide, and indirect addressing, using a PDQ FORTRAN compiler. Simple modifications should allow the program to be run on other computers of comparable size having FORTRAN compilers.

Only one control card is required to operate the program. This card is the first entered into the computer after the program object decks and sub-routines have been loaded, and contains the following information:

^{1/}Crout's method may not return determinants from certain ill-conditioned matrices. In such cases, the order of variables may be changed and the program rerun, or the $[SS_W]$ and $[SS_T]$ matrices may be punched out and the determinants found by another procedure.

Col. 1- 5 N, an integer indicating the number of groups
Col. 6-10 NVAR, an integer indicating the number of variables.

This card is followed by data for the first group, punched in the format specified by statement 818 (as listed, this is 4F15.0). The data set is terminated by a card containing the number 999, punched in the field of the first variable. The second group follows with a similar termination card, and so on through all N groups.

The program test data listed in Appendix II was taken from an example published by Miller and Kahn (1962, p. 257). Output from this program may be compared with their Tables 12.3 and 12.4. A test statistic of 39.622 was obtained for testing the difference of multivariate means of Merychoidoden culbertsoni and Prodesmatochoerus meeki. Miller and Kahn obtained a value of 39.402. The difference probably is due to the additional significant digits carried by the computer.

ACKNOWLEDGMENTS

I wish to thank Dr. T. C. Bagchi, Head of the Department of Geology and Geophysics, Indian Institute of Technology, for his encouragement of computer studies in the earth sciences. Mr. B. S. R. Rao, Department of Civil Engineering, IIT, contributed to the writing of this program. The program was developed and tested at the IIT Computer Centre through the cooperation of Mr. Asish Maity and A. Roy.

REFERENCES

- Krumbein, W. C., and Graybill, A. F., 1965, An introduction to statistical models in geology: McGraw-Hill Book Co., New York, 475 p.
- Miller, R. L., and Kahn, J. S., 1962, Statistical analysis in the geological sciences: John Wiley & Sons, New York, 483 p.
- Nielsen, K. L., 1956, Methods in numerical analysis: Macmillan Co., New York, 382 p.
- Rao, C. R., 1952, Advanced statistical methods in biometrical research: John Wiley & Sons, New York, 390 p.
- Wilks, S. S., 1932, Certain generalizations in the analysis of variance: Biometrika, v. 24, p. 471-494.

```

C      MULTIVARIATE ANALYSES
C      FORTRAN II VERSION
C      TESTED ON IBM 1620 UNIT WITH 40 CORE MEMORY
C      MAIN PROGRAM OCCUPIES 19034 STORAGE LOCATIONS
C      12 SETS OF DATA EACH WITH 1 - 10 VARIABLES
C      CAN BE PROCESSED. IN EACH SET, THERE IS NO LIMIT
C      TO THE NUMBER OF OBSERVATIONS TO BE INCLUDED.
C      FIRST CARD IN INPUT IS N - NVAR CARD IN I5
C      FORMAT. N = NO. OF SETS AND NVAR = NO. OF VARIABLES
C      DATA FOR EACH SET FOLLOWS WITH A 999. TERMINATION CARD
C      AFTER EACH SET
C
C      PROGRAMMER = S.V.L.N.RAO,ASST.PROFESSOR,
C      IND.INST.OF TECHNOLOGY,KHARAGPUR,INDIA
C
C      DIMENSION X(10),P(12,10),XY(55),SXSX(55),VXY(55),VAR(12,10)
C      DIMENSION      SP(10),W(10,11),A(10,11),S(10,11),DET(2)
C      DIMENSION      PM(12,10)
C
C      SUMS,CROSS PRODUCT SUMS ARE COMPUTED
C
1234 COUNT1 = 0.
      SUM = .00626454
      SMEN = .54454155
      VARR = .00654159
      READ 826,N,NVAR
      DO 47 J = 1,NVAR
47      SP(J) = 0.
826      FORMAT (2I5)
      AN = NVAR
      JJ = (AN*(AN+1.))/2.
      DO 4311 J = 1,JJ
      SXSX ( J ) = 0.
      XY(J ) = 0.
4311      VXY(J ) = 0.
      DO 88 K = 1,N
      NP = 1
      DO 78 J = 1,NVAR
78      P(K,J) = 0.
      COUNT2 = 0.
      68 READ 818,(X(J),J= 1,NVAR)
818      FORMAT(4F15.0)
      IF(X(1) - 999.) 178,198,178
178      DO 40 J = 1,NVAR
      40 P(K,J) = P(K,J) + X(J)
1709      MC = 1
      MB = 0
      NB = NVAR
      GO TO (408,508,608),NP
408      DO 34 J = 1,NB
      JM = J +MB
      XY(MC)= XY(MC) +X(J) *X(JM)
      VXY(MC)= VXY(MC) + X(J) * X(JM)
      34 MC = MC+1
708      MB = MB +1
      NB = NB-1
      GO TO (1409,1509,1609),NP
1409      IF(NB) 408,409,408
409      COUNT1= COUNT1 + 1.
      COUNT2= COUNT2 + 1.
      GO TO 68

```

```

C
C      MEAN, VARIANCE ARE COMPUTED
C
198 DO 108 J = 1,NVAR
    PM(K,J) = P(K,J)/COUNT2
    TTP = P(K,J)**2 / COUNT2
108 VAR(K,J) =(VXY(J) - TTP )/(COUNT2 - 1.)
    NP = 2
    GO TO 1709
508 DO 365 J = 1,NB
    JM = J+MB
    SXSJ(MC) = SXSJ(MC) + PM(K,J) * PM(K,JM) * COUNT2
365 MC= MC+1
    GO TO 708
1509 IF(NB) 508,509,508
509 DO 2 J = 1,NVAR
    2 SP(J) = SP(J) + P(K,J)
    DO 77 J = 1,JJ
    77 VXY( J) = 0.
88 CONTINUE
C
C      WITHIN AND TOTAL VARIANCE MATRICES ARE COMPUTED
C
    NP = 3
    GO TO 1709
608 DO 784 J = 1,NB
    JM = J + MB
    W(J,JM) = XY(MC) - SXSJ(MC)
    W(JM,J) = W(J,JM)
    TNN =(SP(J)*SP(JM))/COUNT1
    S(J,JM) = XY(MC) - TNN
    S(JM,J) = S(J,JM)
784 MC = MC+1
    GO TO 708
1609 IF(NB) 608,698,608
C
C      PUNCHES OUT THE MEAN SUM AND VARIANCE FOR THE SETS
C
698 PUNCH 1113
1113 FORMAT(25X,30H MULTIVARIATE ANALYSES RESULTS,/)
    DO 1123 K = 1,N
    PUNCH 1115,K
1115 FORMAT(37X,7HSET NO=I3)
    PUNCH 1117,SUM,( P(K,J),J = 1,NVAR)
    PUNCH 1117,SMEN,(PM(K,J) , J= 1,NVAR)
1123 PUNCH 1117,VARR,(VAR(K,J),J = 1,NVAR)
    PUNCH 1141
1141 FORMAT(/,30X,22HWITHIN VARIANCE MATRIX,/)
    DO 4412 J = 1,NVAR
4412 PUNCH 1145,(W(I,J) ,I = 1,NVAR)
1145 FORMAT ( 5(2X,E14.8))
    PUNCH 1151
1151 FORMAT(/,30X,22HTOTAL VARIANCE MATRIX,/)
    DO 4414 J = 1,NVAR
4414 PUNCH 1145,(S(I,J) ,I = 1,NVAR)
1117 FORMAT(10X,1A4/5(2X,E14.8) )
C
C      DETERMINANTS ARE COMPUTED BY CROUT-S METHOD
C
    DO 101 IA=1,2
    IF (IA-1) 116,116,118

```

```

116 DO 122 I=1,NVAR
DO 122 J=1,NVAR
122 A(I,J)=S(I,J)
GO TO 202
118 DO 124 I=1,NVAR
DO 124 J=1,NVAR
124 A(I,J)=W(I,J)
202 DO 252 J=1,NVAR
DO 222 I=J,NVAR
IF(J-1)210,210,211
210 GS=0.
GO TO 222
211 M=J-1
GS=0.
DO 221 K=1,M
221 GS=GS+A(I,K)*A(K,J)
222 A(I,J)=A(I,J)-GS
I=J
KA=I+1
IF(KA - NVAR) 357,357,359
357 DO 252 JB = KA,NVAR
IF(I-1)220,220,232
220 GS=0.
GO TO 252
232 KB=I-1
GS=0.
DO 242 NA=1,KB
242 GS=GS+A(I,NA)*A(NA,JB)
252 A(I,JB) = ( A(I,JB) - GS) / A(I,I)
359 DET(IA)=1.
DO 101 I=1,NVAR
101 DET(IA)=DET(IA)*A(I,I)
VIN=DET(2)/DET(1)

```

MULTIVARIATE ANALYSES RESULTS

SET NO= 1

SUM	.66800000E+03	.12710000E+04	.24600000E+03	.92500000E+02
MEAN	.47714285E+02	.90785714E+02	.17571428E+02	.66071428E+01
VAR	.32967692E+01	.44892307E+01	.17637384E+01	.78686846E+00

SET NO= 2

SUM	.47200000E+03	.99900000E+03	.18800000E+03	.53000000E+02
MEAN	.39333333E+02	.83250000E+02	.15666666E+02	.44166666E+01
VAR	.15151545E+02	.13659090E+02	.42424272E+01	.17969727E+00

WITHIN VARIANCE MATRIX

.20952800E+03	.72150000E+02	.31621000E+02	.95623000E+01
.72150000E+02	.20861000E+03	.34718000E+02	-.19280000E+01
.31621000E+02	.34718000E+02	.69595900E+02	.45098000E+01
.95623000E+01	-.19280000E+01	.45098000E+01	.12206000E+02

TOTAL VARIANCE MATRIX

.66338500E+03	.48024000E+03	.13477000E+03	.12818470E+03
.48024000E+03	.57554000E+03	.12746200E+03	.10473100E+03
.13477000E+03	.12746200E+03	.93038500E+02	.31469300E+02
.12818470E+03	.10473100E+03	.31469300E+02	.43209620E+02

TEST VALUE= 39.622

DEG.FREEDOM= 4

X² DISTRIBUTION VALUES

DF**(4) = 9.49	DF(6) = 12.59	DF(8) = 15.01	DF(10) = 18.31
DF (12) = 21.03	DF(14) = 23.68	DF(16) = 26.30	DF(18) = 28.87
DF (20) = 31.41	DF(24) = 36.42	DF(30) = 43.77	DF(40) = 55.76

*Symbol for X²
**Degrees of freedom

C
C
C

TEST STATISTIC COMPUTED

```

TK = N
PP = NVAR
TM = (COUNT1-1.) -((PP+(TK-1.) + 1.)/ TK)
IDEGF=PP * (TK - 1.)
VV= -TM * LOGF(VIN)
PUNCH 1161, VV , IDEGF
1161 FORMAT(/,10X,11HTEST VALUE=F8.3,14X,12HDEG.FREEDOM=I3,/)
PUNCH 832
832 FORMAT(5X,22HX2 DISTRIBUTION VALUES,/)
PUNCH 834
834 FORMAT(5X,12HDF( 4)= 9.49,2X,12HDF( 6)=12.59,2X,
112HDF( 8)=15.01,2X,12HDF(10)=18.31)
PUNCH 837
837 FORMAT(5X,12HDF(12)=21.03,2X,12HDF(14)=23.68,2X,
112HDF(16)=26.30,2X,12HDF(18)=28.87)
PUNCH 839
839 FORMAT(5X,12HDF(20)=31.41,2X,12HDF(24)=36.42,2X,
112HDF(30)=43.77,2X,12HDF(40)=55.76)
PRINT 1712
1712 FORMAT(5X,20HPLEASE PUT NEXT SET.)
GO TO 1234
END

```

INPUT DETAILS

	2	4			
	45.0	91.0	16.0	07.5	N, NVAR card
	46.0	93.0	17.0	06.5	
	48.0	92.0	19.0	05.0	
	46.0	91.0	19.0	06.0	
	45.0	86.0	15.0	06.5	
	51.0	93.0	19.0	07.5	
Data for Set 1	47.0	92.0	16.0	05.0	
	48.0	89.0	18.0	06.5	
	47.0	91.0	17.5	06.0	
	50.0	91.0	17.0	07.2	
	48.0	91.0	19.0	07.6	
	49.0	93.0	17.5	07.0	
	49.0	87.0	17.0	06.5	
	49.0	91.0	19.0	07.7	
	999.				Termination card
	37.0	88.0	17.0	03.9	
	43.0	84.0	19.0	04.2	
	43.0	79.0	14.0	04.0	
	42.0	80.0	17.0	05.2	
	39.0	83.0	12.0	04.5	
Data for Set 2	39.0	87.0	15.0	04.5	
	40.0	86.0	18.0	04.5	
	34.0	77.0	16.0	04.8	
	35.0	82.0	15.0	04.6	
	45.0	88.0	17.0	04.9	
	33.0	80.0	15.0	03.9	
	42.0	85.0	13.0	04.0	
	999.				Termination card

KANSAS GEOLOGICAL SURVEY COMPUTER PROGRAM
THE UNIVERSITY OF KANSAS, LAWRENCE

PROGRAM ABSTRACT

Title (If subroutine state in title):

FORTRAN II program for the calculation of Wilks' Λ using an IBM 1620 computer.

Date: _____

Author, organization: S.V.L.N. Rao, Dept. Geology, Indian Institute of Technology, Kharagpur, India

Direct inquiries to: Author, or

Name: D.F. Merriam

Address: Kansas Geological Survey

Lawrence, Kansas 66044

Purpose/description: Computes Wilks' criterion for testing equality of multivariate means (multivariate analysis of variance or analysis of dispersion).

Mathematical method: Λ is calculated as the ratio of the determinants of two matrices. Determinants are found by Crout's method.

Restrictions, range: Up to 12 data sets may be used, each having up to 10 variables. Any number of samples may be used in the groups.

Computer manufacturer: IBM Model: 1620 Model 2

Programming language: PDQ FORTRAN

Memory required: 40 K Approximate running time: _____

Special peripheral equipment required: None

Remarks (special compilers or operating systems, required word lengths, number of successful runs, other machine versions, additional information useful for operation or modification of program) _____

Requires PDQ FORTRAN Processor C2 (IBM User's Group Program 2.0.031).

COMPUTER CONTRIBUTIONS

Kansas Geological Survey
University of Kansas
Lawrence, Kansas

Computer Contribution

1. Mathematical simulation of marine sedimentation with IBM 7090/7094 computers, by J.W. Harbaugh, 1966	\$1.00
2. A generalized two-dimensional regression procedure, by J.R. Dempsey, 1966	\$0.50
3. FORTRAN IV and MAP program for computation and plotting of trend surfaces for degrees 1 through 6, by Mont O'Leary, R.H. Lippert, and O.T. Spitz, 1966	\$0.75
4. FORTRAN II program for multivariate discriminant analysis using an IBM 1620 computer, by J.C. Davis and R.J. Sampson, 1966	\$0.50
5. FORTRAN IV program using double Fourier series for surface fitting of irregularly spaced data, by W.R. James, 1966	\$0.75
6. FORTRAN IV program for estimation of cladistic relationships using the IBM 7040, by R.L. Bartcher, 1966	\$1.00
7. Computer applications in the earth sciences: Colloquium on classification procedures, edited by D.F. Merriam, 1966	\$1.00
8. Prediction of the performance of a solution gas drive reservoir by Muskat's Equation, by Apolonio Baca, 1967	\$1.00
9. FORTRAN IV program for mathematical simulation of marine sedimentation with IBM 7040 or 7094 computers, by J.W. Harbaugh and W.J. Wahlstedt, 1967	\$1.00
10. Three-dimensional response surface program in FORTRAN II for the IBM 1620 computer, by R.J. Sampson and J.C. Davis, 1967	\$0.75
11. FORTRAN IV program for vector trend analyses of directional data, by W.T. Fox, 1967	\$1.00
12. Computer applications in the earth sciences: Colloquium on trend analysis, edited by D.F. Merriam and N.C. Cocks, 1967.	\$1.00
13. FORTRAN IV computer programs for Markov chain experiments in geology, by W.C. Krumbein, 1967	\$1.00
14. FORTRAN IV programs to determine surface roughness in topography for the CDC 3400 computer, by R.D. Hobson, 1967	\$1.00
15. FORTRAN II program for progressive linear fit of surfaces on a quadratic base using an IBM 1620 computer, by A.J. Cole, C. Jordan, and D.F. Merriam, 1967	\$1.00
16. FORTRAN IV program for the GE 625 to compute the power spectrum of geological surfaces, by J.E. Esler and F.W. Preston, 1967.	\$0.75
17. FORTRAN IV program for Q-mode cluster analysis of nonquantitative data using IBM 7090/7094 computers, by G.F. Bonham-Carter, 1967	\$1.00
18. Computer applications in the earth sciences: Colloquium on time-series analysis, D.F. Merriam, editor, 1967.	\$1.00
19. FORTRAN II time-trend package for the IBM 1620 computer, by J.C. Davis and R.J. Sampson, 1967	\$1.00
20. Computer programs for multivariate analysis in geology, D.F. Merriam, editor, 1968	\$1.00

NOTE: Decks for the programs are available at the following prices for a limited time.

Wolleben, J.A., Pauken, R.J., and Dearien, J.A., FORTRAN IV program for multivariate paleontologic analysis using an IBM System/360 Model 40 computer	\$10.00
Sampson, R.J., R-mode factor analysis program in FORTRAN II for the IBM 1620 computer.	\$15.00
Klovan, J.E., Q-mode factor analysis program in FORTRAN IV for small computers	\$10.00
Rao, S.V.L.N., FORTRAN II program for the calculation of Wilks' Λ using an IBM 1620 computer	\$ 5.00

