

DANIEL F. MERRIAM, Editor

**FORTRAN II TIME-TREND
PACKAGE FOR THE
IBM 1620 COMPUTER**

By

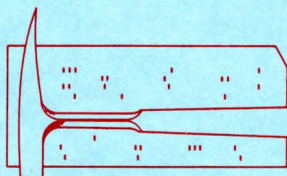
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COMPUTER CONTRIBUTION 19
State Geological Survey
The University of Kansas, Lawrence
1967

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Editor's Remarks

In addition to making computer programs available, the Geological Survey provides information in machineable form. At present two sets of data have been made available (1) a list of all wells drilled into Precambrian rocks in the State, and (2) compendium of helium data.

The Precambrian well data have been available for several years and consist of well location, name, elevation, Precambrian datum, rock type, overlying formation, total depth, and year drilled. Information on more than 2,650 wells has been compiled, and the list is updated yearly.

Now helium data have been released. They consist of well location, geologic formation and lithology, depth of sample zone, wellhead pressure, date of well completion, date sampled and composition.

Copies of the data will be sent post paid, by certified mail according to the following price schedule:

- (1) 32-page printout \$5.00
- (2) returnable magnetic tape copy \$20.00
- (3) duplicate card deck \$25.00

The data are areally concentrated in the southern half of the State, and vertically concentrated in gas-producing zones. There are a few helium only analyses, but the data include all analyses for which helium was specifically analyzed. Thus, data are included from noncommercial gas wells, oil wells, water wells and composite samples.

The Geological Survey's file record and master card decks will be updated whenever information is available.

In making this information available, the Geological Survey is fulfilling yet another service to the State and profession. It is anticipated that in the future other data will be released. The Geological Survey is the only geological organization now known to be distributing data decks as well as computer program decks. An up-to-date list of publications is available on request.

Comments and suggestions concerning the COMPUTER CONTRIBUTION series are welcome and should be addressed to the Editor.

FORTRAN II TIME-TREND PACKAGE FOR THE IBM 1620 COMPUTER

By

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INTRODUCTION

Many types of geologic data are distributed serially, either through time or along a geographic coordinate. Although such data are ordered, it is seldom equally spaced, especially in the time sense. Geologic information that may be uniformly ordered through time (time series) includes that from varved sequences or annual growth of organisms, such as tree rings or bands on certain corals. Most other types of data, such as measurements of a stratigraphic succession, represent a nonuniform time series in which the length of the units are not known. In these instances, distance is used as an approximator of time, and the data sequence is considered as a geographic series. Other types of geographic series have no time connotation; examples include data collected along a traverse or information produced by a linear recorder attached to equipment such as an x-ray diffraction unit or infrared spectrometer.

Serial methods have been applied primarily in three types of investigation. They have been used for the extraction of components, in the examination for periodicity, and to obtain numerical approximations of sequences. Component extraction consists of curve fitting by various methods so that the data are separated into (1) an underlying "trend" and (2) superposed "noise" or error, which is a random component. Filtering of seismographic records to remove random fluctuations is an example of this application. More recently, data from stratigraphic sequences have been smoothed by curve fitting to aid in the detection of long-term trends.

Techniques borrowed from market analysis have been applied widely in the search for periodicity in oscillatory data. Autocorrelation has been used to examine oscillatory sedimentary sequences such as cyclothem in an attempt to objectively test the hypothesis of rhythmic sedimentation. Statistical tests are available for determining the validity of suspected trends in data and are useful in such diverse areas as stratigraphic analysis and prediction of crude-oil reserves.

One of the most recent innovations is the

application of time-series statistics to problems of stratigraphic correlation. Although the data usually do not meet the criteria necessary for valid time series, stratigraphic correlations on the basis of such parameters as coded lithologies or drilling times have been successful. Most of these applications have utilized cross-correlation, cross-association, or related statistics. It is also possible to compare certain types of serial data by reducing the sequences to equations and clustering them on the basis of the similarity of their coefficients.

PROGRAM DESCRIPTIONS

The accompanying series of programs are written in FORTRAN II for use on an IBM 1620 computer having 20K bits core storage. Restrictions in programs for this computer are typical of those inherent in older machines and also in a new generation of instruments such as the PDP-8, IBM 1130 and 1800, SDS Sigma 2, and other small computers. These machines are most generally available to geologists at smaller universities and in oil and mining company field offices. Even on campuses having large data-processing centers, many departments and agencies maintain small computers for their own instructional or routine use. They are usually the only type of computer available in many installations outside the United States. Persons having computers similar in characteristics to the IBM 1620 should find this collection of programs easily adaptable to their use.

Because of computer size restrictions, the different operations cannot be combined into a single large program with options. They are separated, therefore, into a series of independent programs capable of being used separately or in conjunction with one another. A "single" program with options in FORTRAN IV written for the GE 625 also is available. The following five programs constitute the package:

PROGRAM 1 - Equal Spacing and Data Smoothing.

This program will accept unevenly spaced sequential data and convert it to equal spacing.

It also will smooth equally spaced data by Sheppard's equation, Spencer's equation, an n-term sliding trapezoidal approximation, or an n-term sliding average.

PROGRAM 2 - Autocorrelation and Cross-Correlation.

The program will accept one sequence of equally spaced data and perform an autocorrelation, or will accept two data chains and perform cross-correlation. Either forward or backward matching is possible, with chains moving in steps of n.

PROGRAM 3 - Burnaby's Cross-Difference Product.

The cross-difference product (CDP) was proposed by Burnaby (1953) as an alternative to cross-correlation. This program will accept two chains of equally spaced data and compute the CDP for matches moving forward or backward in steps of n.

PROGRAM 4 - Cross Association. This program is an adaptation of a procedure developed by Sackin and Sneath (1965) for the comparison of non-numeric sequences. Unlike other programs in this package, it requires integer data (usually of an arbitrary nature, such as sandstone = 1, shale = 2, limestone = 3, etc.).

All programs require PDQ FORTRAN Processor C2 without reread version 1 modification 0, and PDQ FORTRAN fixed format subroutines without reread version 1 modification 0 (IBM User's Group Program 2.0.031) for operation on the IBM 1620. Minimal machine requirements consist of an IBM 1620 Model 1 central processing unit with 20K bits storage, automatic divide, and indirect addressing. A 1622 card read punch and a 407 accounting machine or similar line printer also are required. Examples of output are included in Appendix.

OPERATING INSTRUCTIONS

Program 1 - Equal Spacing and Smoothing Program.

This program was designed for analysis of stratigraphic sequences, but is not limited to such problems. Data consist of the distances between successive data points (x values) and the value of the variable at the points (y values). For example, x may be the thickness in feet of stratigraphic units, and y a code for a lithology or some sedimentary parameter (Fox, 1964). In the example here, drilling-time logs are used, x is the interval between successive recording points, and y is the time in minutes required to drill the interval.

This program requires two passes. Data are processed on the first pass to produce a new set of data cards containing estimated values of y' at specified equally spaced values of x. Values of y' are computed by a rectangular integration method described by Fox (1964). This intermediate output is entered into the computer and smoothed by one of the specified smoothing equations:

(1) Sheppard's 5-term equation (Whittaker and

Robinson, 1926, Vistelius, 1961).

$$\hat{y}_0 = \frac{1}{35} [17y'_0 + 12 (y'_{+1} + y'_{-1}) - 3 (y'_{+2} + y'_{-2})] \quad (1)$$

(2) Spencer's 21-term equation (Whittaker and Robinson, 1926, Vistelius, 1961).

$$\hat{y}_0 = \frac{1}{350} [60y'_0 + 57 (y'_{+1} + y'_{-1}) + 47 (y'_{+2} + y'_{-2}) + 33 (y'_{+3} + y'_{-3}) + 18 (y'_{+4} + y'_{-4}) + 6 (y'_{+5} + y'_{-5}) - 2 (y'_{+6} + y'_{-6}) - 5 (y'_{+7} + y'_{-6}) - 5 (y'_{+8} + y'_{-8}) - 3 (y'_{+9} + y'_{-9}) - (y'_{+10} + y'_{-10})] \quad (2)$$

(3) Sliding average with specified span.

$$\hat{y}_0 = \frac{y'_{-m} + \dots + y'_{-1} + y'_0 + y'_{+1} + \dots + y'_{+m}}{2m + 1} \quad (3)$$

Span (2m + 1) may be any odd value from 3 to 101. A sliding average weights all points within the span equally in the calculation of \hat{y}_i .

(4) Trapezoidal rule approximation with specified span.

$$\hat{y}_0 = \frac{y'_{-m} + 2y'_{-(m-1)} + \dots + 2y'_{-1} + 2y'_0 + 2y'_{+1} + \dots + 2y'_{+(m-1)} + y'_{+m}}{4m} \quad (4)$$

Output from the second pass consists of a cumulative total of x, smoothed value of \hat{y} , observed value of y', and the deviation at each point. After processing all points, total thickness of raw data, total thickness of equally spaced data, and total thickness of smoothed data are punched. A measure of goodness of fit of smoothed to equally spaced data then is computed by the equation:

$$R^2 = \frac{[n \sum y' - (\sum y')^2] - \sum (y' - \hat{y})^2}{n \sum y'^2 - (\sum y')^2} \quad (5)$$

Expected and observed numbers of runs in the smoothed data sequence are next computed (Miller and Kahn, 1962, p. 331). The expected number of runs in a random sequence of numbers is

$$E_{(r)} = (2n-1)/3, \quad (6)$$

and the expected number of nonruns is

$$E_{(nr)} = (2n-2) - E_{(r)}. \quad (7)$$

Nonrandomness can be tested in a 2 x 2 contingency table of the form

$$\chi^2 = \frac{(O_{(r)} - E_{(r)})^2}{E_{(r)}} + \frac{(O_{(nr)} - E_{(nr)})^2}{E_{(nr)}} \quad (8)$$

with one degree of freedom. $O_{(r)}$ and $O_{(nr)}$ are the number of observed runs and nonruns, respectively. The program prints $E_{(r)}$, $O_{(r)}$, and χ^2 . The standard deviation of smoothed values also is printed.

A series of statistics pertaining to the equally spaced data is next produced. These include $E_{(r)}$, $O_{(r)}$, χ^2 , and the standard deviation of the equal spaced values. The slope (β) of the linear regression of y' on x is computed, accompanied by a t -value and degrees of freedom for testing the hypothesis that the slope is zero. This feature is useful for the detection of linear bias or trend in the data.

After loading the Program 1 object deck and subroutines, the message LOAD DATA will be typed on the console typewriter. The following sequence of cards should then be entered.

CARD 1 - Control card containing the following options code:

- Col. 1- 2 Blank.
- Col. 3 Selection of smoothing equation.
 - 1 = Sheppard's 5-term smoothing equation.
 - 2 = Spencer's 21-term smoothing equation.
 - 3 = Sliding average.
 - 4 = Trapezoidal approximation.

```

C   TIME TREND ANALYSIS -- PROGRAM 1
C   EQUAL SPACING AND SMOOTHING PROGRAM
C   ROBERT SAMPSON -- PROGRAMMER
C   ISU COMPUTER CENTER PROJECT NO. 75
C   BEGIN TRACE
C   DIMENSION SLITH(101)
C   1 DO 100 I=1,101
C   100 SLITH(I)=0.0
C   SX=0.0
C   SY=0.0
C   SXY=0.0
C   SXX=0.0
C   SYY=0.0
C   READ 1000,IEQ,NT,AINT
C   READ 1001
C   TTH=0.0
C   IF (SENSE SWITCH 1) 60,61
C   61 PUNCH 1001
C   PUNCH 1023
C   PUNCH 1013,AINT
C   60 READ 1002,DATT,DATL
C   NTT=0
C   DATTL=DATT

```

Col. 4- 6 Integer specifying the number of terms in smoothing equation. This must be 005 for Sheppard's equation, 021 for Spencer's equation, and an odd number between 003 and 101 if a sliding average or trapezoidal approximation is used.

Col. 7-16 Length of interval between equally spaced data. This number must contain a decimal point.

CARD 2 - This is a title card containing any desired alphanumeric information in col. 1-80.

CARD 3 - This is the first of any number of data cards, each containing one set of x and y values.

Col. 1-10 Values of x . This number must contain a decimal point.

Col. 11-20 Values of y . This number must contain a decimal point.

END CARD - This card is placed at the end of the data deck and contains the number 9.0E 48 punched in col. 1-7.

After completion of punching of intermediate output, the message ENTER EQUAL SPACED DATA will be typed on the console typewriter. The set of intermediate output should be loaded and final output will then be produced. At the completion of calculations, the message STOP 100 will be typed and the machine will pause. A new data set may be entered at this time. If more than one smoothing operation is necessary on a set of data, turn SENSE SWITCH 1 to ON. A new control card should be prepared and inserted in the original data deck and the procedure outlined above repeated. No new intermediate output will be produced, however, because the smoothed data produced on the initial run is used for Pass 2.

```

    DATLL=DATL
    TSTH=AIN T
    SL=0.0
    GO TO 3
2  READ 1002,DATTL,DATLL
   IF (DATTL-9.0E 48) 3,4,3
3  TTHL=TTH+DATTL
   7 IF (TTHL-TSTH) 5,6,6
5  DIF=TTH-TSTH+AIN T
   IF (DIF) 80,81,81
80 SL=SL+(DATTL+DIF)*DATLL
   GO TO 84
81 SL=SL+DATTL*DATLL
84 TTH=TTHL
   DATL=DATLL
   GO TO 2
   6 DIF=TTH-TSTH+AIN T
   IF (DIF) 82,83,83
83 DIF=0.0
82 SL=SL+(DATTL-(TTHL-TSTH)+DIF)*DATLL
   SL=SL/AIN T
   NTT=NTT+1
   IF (SENSE SWITCH 1) 8,9
9  PUNCH 1003,NTT,TSTH,SL
8  SX=SX+TSTH
   SY=SY+SL
   SXY=SXY+TSTH*SL
   SXX=SXX+TSTH*TSTH
   SYY=SYY+SL*SL
   TSTH=TSTH+AIN T
   SL=0.0
   GO TO 7
4  NTM=2
   IF (SENSE SWITCH 1) 90,91
91 PUNCH 1014
90 PRINT 1024
   READ 1015
   PUNCH 1001
   EXECUTE PROCEDURE 5000
   PUNCH 1022,AIN T
   PUNCH 1021
   RCN=0.0
   RCN1=0.0
   AN=NTT
   READ 1004,SLITH(1)
   READ 1004,SLITH(2)
   RCL=SGN(SLITH(2)-SLITH(1))
   MID=NT/2+1
   NTT=0
   SSD=0.0
   SSY=0.0
   SSYY=0.0
   TS=NT/2
   TST=TS*AIN T
15 NTM=NTM+1
   READ 1004,SLITH(NTM)
   IF (SLITH(NTM)-9.0E 48) 10,11,10
10 RC=SGN(SLITH(NTM)-SLITH(NTM-1))
   IF (RC) 12,13,12
12 IF (RC-RCL) 14,13,14
14 RCN=RCN+1.0
   RCL=RC

```

```

13 IF (NT-NTM) 99,16,15
16 GO TO (41,42,43,44),IEQ
41 SLC=17.0*SLITH(3)+12.0*(SLITH(2)+SLITH(4))-3.0*(SLITH(1)+SLITH(5))
   SLC=SLC/35.0
   GO TO 45
42 SLC=60.0*SLITH(11)+57.0*(SLITH(10)+SLITH(12))
   SLC=SLC+47.0*(SLITH(9)+SLITH(13))+33.0*(SLITH(8)+SLITH(14))
   SLC=SLC+18.0*(SLITH(7)+SLITH(15))+6.0*(SLITH(6)+SLITH(16))
   SLC=SLC-2.0*(SLITH(5)+SLITH(17))-5.0*(SLITH(4)+SLITH(18))
   SLC=SLC-5.0*(SLITH(3)+SLITH(19))-3.0*(SLITH(2)+SLITH(20))
   SLC=(SLC-(SLITH(1)+SLITH(21)))/360.0
   GO TO 45
43 ANT=NT
   SUM=0.0
   DO 102 I=1,NT
102 SUM=SUM+SLITH(I)
   SLC=SUM/ANT
   GO TO 45
44 SLC=SLITH(1)+SLITH(NT)
   N=NT-1
   DO 103 I=2,N
103 SLC=SLC+2.0*SLITH(I)
   ANT=N
   SLC=SLC/(2.0*ANT)
45 NTT=NTT+1
   IF (NTT-1) 99,200,201
200 SLCL=SLC
   GO TO 202
201 IF (NTT-2) 99,203,204
203 RCL1=SGN(SLC-SLCL)
   GO TO 200
204 RC1=SGN(SLC-SLCL)
   SLCL=SLC
   IF (RC1) 205,202,205
205 IF (RC1-RCL1) 206,202,206
206 RCN1=RCN1+1.0
   RCL1=RC1
202 TST=TST+AIN
   DIF=SLITH(MID)-SLC
   SSD=SSD+DIF*DIF
   SSY=SSY+SLC
   SSYY=SSYY+SLC*SLC
   PUNCH 1005,NTT,TST,SLC,SLITH(MID),DIF
   DO 101 I=2,NT
101 SLITH(I-1)=SLITH(I)
   NTM=NTM-1
   GO TO 15
11 PUNCH 1014
   AN2=NTT
   SSSXY=SXY-SX*SY/AN
   SSSX=SXX-SX*SX/AN
   SSSY=SY-SY*SY/AN
   B=SSSXY/SSSX
   T=SSSXY/SQRT((SSSY*SSSX-SSSXY*SSSXY)/(AN-2.0))
   ND=AN-2.0
   TSTH=TSTH-AINT
   TST=TST-TS*AIN-AINT
   GF=(SSSY-SSD)/SSSY
   ER=(2.0*AN-1.0)/3.0
   ENR=AN-2.0-ER
   ONR=AN-2.0-RCN
   CHI=((ER-RCN)**2)/ER+((ONR-ENR)**2)/ENR

```

```

ER1=(2.0*AN2-1.0)/3.0
ENR1=AN2-2.0-ER1
ONR1=AN2-2.0-RCN1
CHI1=((ER1-RCN1)**2)/ER1+((ONR1-ENR1)**2)/ENR1
SDL=SQRT(SYY/AN-(SY/AN)**2)
SDSL=SQRT(SSYY/AN2-(SSY/AN2)**2)
PUNCH 1001
PUNCH 1012,TTHL
PUNCH 1006,TSTH
PUNCH 1007,TST
PUNCH 1009,GF
EXECUTE PROCEDURE 5000
PUNCH 1008,ER1,RCN1,CHI1
PUNCH 1016,SDSL
PUNCH 1023
PUNCH 1008,ER,RCN,CHI
PUNCH 1010,SDL
PUNCH 1011,B,T,ND
99 STOP 100
GO TO 1
BEGIN PROCEDURE 5000
GO TO (71,72,73,74),IEQ
71 PUNCH 1017
GO TO 70
72 PUNCH 1018
GO TO 70
73 PUNCH 1019,NT
GO TO 70
74 PUNCH 1020,NT
70 END PROCEDURE 5000
1000 FORMAT (2I3,F10.2)
1001 FORMAT (40H
140H
1002 FORMAT (2F10.2)
1003 FORMAT (I6,2F15.5)
1004 FORMAT (2I4,F15.5)
1005 FORMAT (I6,4F15.5)
1006 FORMAT (/ ,1X,25HTOTAL EQUAL SPACED DATA =,F12.4)
1007 FORMAT (/ ,26HTOTAL SMOOTHED THICKNESS =,F12.4)
1008 FORMAT (19HEXPECTED NO. RUNS =,F10.1,21H OBSERVED NO. RUNS =,
1,F10.1,8H CHI2 =,F10.4)
1009 FORMAT (/ ,17HGOODNESS OF FIT =,F12.4,/)
1010 FORMAT (/ ,20HSTANDARD DEVIATION =,F12.4)
1011 FORMAT (/ ,10HSLOPE(B) =,F12.4,5X,3HT =,F12.4,5H WITH,I5,
119H DEGREES OF FREEDOM)
1012 FORMAT (/ ,9X,17HTOTAL THICKNESS =,F12.3)
1013 FORMAT (/ ,10HINTERVAL =,F12.4,/,/,
134H UNIT CUMULATIVE TOTAL VALUE)
1014 FORMAT (23X,7H9.0E 48)
1015 FORMAT (1X,////////)
1016 FORMAT (/ ,20HSTANDARD DEVIATION =,F12.4,/)
1017 FORMAT (/ ,25H5 TERM SMOOTHING EQUATION)
1018 FORMAT (/ ,26H21 TERM SMOOTHING EQUATION)
1019 FORMAT (/ ,I4,21H TERM SLIDING AVERAGE)
1020 FORMAT (/ ,I4,24H TERM TRAPEZOID EQUATION)
1021 FORMAT (/ ,38H UNIT CUM. TOTAL SMOOTHED VALUE,
16X,5HVALUE,8X,9HDEVIATION)
1022 FORMAT (/ ,10HINTERVAL =,F12.4)
1023 FORMAT (/ ,17HEQUAL SPACED DATA)
1024 FORMAT (23HENTER EQUAL SPACED DATA)
END TRACE
END

```


Program 2 - Autocorrelation and Cross-Correlation.

This program uses as input either equally spaced data (y') or smoothed data (\hat{y}) produced by Program 1. The program accepts two sets of sequential data, called Chain A and Chain B. Chain B is compared to Chain A by computing the correlation coefficient at successive positions of match. Chain B is in effect "moved" past A in steps of specified size and the degree of coincidence of the overlapping parts of the chains computed at each step. The equation for the correlation coefficient is

$$R = \frac{\Sigma AB - \frac{\Sigma A \Sigma B}{n}}{\sqrt{(\Sigma A^2 - \frac{(\Sigma A)^2}{n})(\Sigma B^2 - \frac{(\Sigma B)^2}{n})}} \quad (9)$$

where n = number of overlapping positions. An indeterminate value of R may be produced if all values of A or B (or both) are the same, then

$$(\Sigma A^2 - \frac{(\Sigma A)^2}{n}) = 0 \quad \text{or} \quad (\Sigma B^2 - \frac{(\Sigma B)^2}{n}) = 0 .$$

This situation can arise only near the ends of the chains, where a short sequence of identical numbers can produce indeterminacy. In these situations, an R of .0000, followed by an asterisk (*), will be printed.

Chain B. may be moved either forward or backward past Chain A. Output consists of the sequential number of the match position, the number of terms being compared at that match, the upper and lower limits of the A terms and B terms and the cross-correlation coefficient. A t -value and degrees of freedom are printed for testing the hypothesis that the correlation is equal to zero, using the equation

$$t_{n-2} = R \sqrt{(n-2) / (1-R^2)} \quad (10)$$

This program also will compute autocorrelations of specified steps along a single chain. Under this option, a data sequence is placed in both A and B chain positions automatically. Analysis and out-

put are the same as in cross-correlation with the exception of column headings.

After loading the Program 2 object deck and subroutines, the message LOAD DATA will be typed out. The following sequence of data cards should be entered.

CARD 1 - Control card

- Col. 1-3 Integer specifying length of sliding step.
- Col. 4-5 Blank.
- Col. 6 Selection of match direction.
1 = Both forward and reverse matches.
0 = Forward matches only.
- Col. 9 Selection of correlation type.
1 = Autocorrelation.
0 = Cross-correlation.

CARD 2 - This is a title card containing any desired alphanumeric information in col. 1-80.

CARDS 3 THROUGH 9 - The seven header cards produced by Program 1. If data other than output from Program 1 are used, seven blank cards should be inserted here.

CARD 10 - This is the first data card of Chain A. Up to 350 cards may be included in this set, which must be equal to or longer than Chain B. Data card format is (21X, F15.5), which reads intermediate or final output from Program 1.

END CARD - This card is placed at the end of Chain A data cards and contains the number 9.0E 48 punched in col. 24-31. This card is included automatically in output from Program 1.

CARDS 11 THROUGH 16 - The seven header cards produced by Program 1. If data other than output from Program 1 are used, seven blank cards should be inserted here.

CARD 17 - This is the first data card of Chain B. Up to 350 cards may be included in this set, which must not be longer than Chain A. Card format is (21X, F15.5).

END CARD - A card containing the number 9.0E 48 punched in col. 24-31 should terminate Chain B. This card is produced by Program 1.

Note: Equally spaced or smoothed data produced by Program 1 are in the proper format for input to Program 2. Output from the smoothing pass has extra cards containing statistical measures that must be removed from the end of the data deck before processing on this program. No other changes are necessary.

```
C TIME TREND ANALYSIS -- PROGRAM 2
C CROSS CORRELATION AND AUTO CORRELATION
C ROBERT SAMPSON -- PROGRAMMER
C ISU COMPUTER CENTER PROJECT NO. 75
  BEGIN TRACE
  DIMENSION A(351),B(351)
  1 READ 1000,INC,IR,IOP
  READ 1001
  READ 1002
  N1=0
```

```

N2=0
IRD=0
2 N1=N1+1
  READ 1003,A(N1)
  IF (A(N1)-9.0E 48) 2,3,2
3 IF (IOP) 34,34,30
30 N2=N1
  DO 130 I=1,N2
130 B(I)=A(I)
  GO TO 19
34 READ 1003
  4 N2=N2+1
  READ 1003,B(N2)
  IF (B(N2)-9.0E 48) 4,19,4
19 N1=N1-1
  N2=N2-1
  5 PUNCH 1001
  IF (IRD) 6,6,7
  6 PUNCH 1004
  GO TO 8
  7 PUNCH 1005
  8 PUNCH 1008,INC
  IF (IOP) 31,31,32
31 PUNCH 1009
  GO TO 33
32 PUNCH 1010
33 PUNCH 1006
  NS=0
  NS1=1
  NS2=N2
  N=INC-1
  IF (INC-2) 9,9,10
  9 N=INC+1
10 NE1=NS1+N
  NE2=NS2-N
11 AN=NE1-NS1+1
  NS=NS+1
  SA=0.0
  SB=0.0
  SAB=0.0
  SBB=0.0
  SAA=0.0
  N=NE2-1
  DO 100 I=NS1,NE1
  SA=SA+A(I)
  SAA=SAA+A(I)*A(I)
  N=N+1
  SB=SB+B(N)
  SBB=SBB+B(N)*B(N)
100 SAB=SAB+A(I)*B(N)
  STAR=.14
  R=0.0
  RB=SQRT((SAA-SA*SA/AN)*(SBB-SB*SB/AN))
  IF (RB) 40,41,40
40 STAR=0.0
  R=(SAB-SA*SB/AN)/RB
41 T=9999.9999
  IF (R*R-1.0) 12,13,99
12 T=R*SQRT((AN-2.0)/(1.0-R*R))
13. NDF=AN-2.0
  N=AN

```

```

NE=NE2
NB=NS2
IF (IRD) 16,16,15
15 NE=N2-NS2+1
NB=N2-NE2+1
16 PUNCH 1007,NS,N,NS1,NE1,NE,NB,R,STAR,T,NDF
NE1=NE1+INC
NE2=NE2-INC
IF (N1-NE1) 20,21,21
20 NE1=NE1-INC
NE2=NE2+INC
NS1=NS1+INC
NS2=NS2-INC
IF (NE1-NS1-1) 98,98,11
21 IF (NE1-NS1+1-N2) 11,11,22
22 NS1=NS1+INC
NE2=NE2+INC
GO TO 11
98 IF (IR) 99,99,17
17 IRD=1
IR=0
K=N2/2
N=N2+1
DO 101 I=1,K
C=B(I)
N=N-1
B(I)=B(N)
101 B(N)=C
GO TO 5
99 STOP 100
GO TO 1
1000 FORMAT (3I3)
1001 FORMAT (40H
140H
1002 FORMAT (1X,////////)
1003 FORMAT (21X,F15.5)
1004 FORMAT (/ ,32X,15HFORWARD MATCHES,/)
1005 FORMAT (/ ,32X,15HREVERSE MATCHES,/)
1006 FORMAT (19H POSITION OF TERMS,4X,5HTERMS,7X,5HTERMS,6X,
111HCOEFFICIENT,8X,1HT,8X,4HD.F.,/)
1007 FORMAT (3I8,I4,I8,I4,F15.4,A1,F14.4,I6)
1008 FORMAT (14HSLIDING STEP =,I4)
1009 FORMAT (/ ,19H MATCH NUMBER,6X,1HA,11X,1HB,5X,
117HCROSS-CORRELATION)
1010 FORMAT (/ ,19H MATCH NUMBER,6X,1HA,11X,1HB,5X,
116HAUTO-CORRELATION)
END TRACE
END

```

Program 3 - Burnaby's Cross-Difference Product

Burnaby (1953) proposed the cross-difference product (E) as an alternative to the correlation coefficient for testing the agreement between pairs of time series. The method has the advantage of negating the effect of first-order autocorrelations within the data sequences.

Within two Chains A and B, an overlap of m positions will result in two series A_1, A_2, \dots, A_m and B_1, B_2, \dots, B_m , where subscripts indicate cor-

respondence at that match position. The cross-difference product is defined as

$$E_{m,m+1} = (A_m - B_{m+1})(B_m - A_{m+1}). \quad (11)$$

In the overlapped set of m values in each chain, there are $\frac{m}{2}$ independent values of E. The mean value of E is given by

$$E_{\mu} = \frac{1}{n} (E_{1,2} + E_{3,4} + E_{5,6} + \dots + E_{m-1,m}).$$

(12)

The significance of E_m may be calculated by testing the hypothesis that $E_\mu = 0$, using the following equation

$$t_{m-1} = \frac{E_\mu \sqrt{m}}{S}, \quad (13)$$

where

$$S = \frac{\sum E_{tj}^2 - (\sum E_{tj})^2}{n(n-1)}. \quad (14)$$

The cross-difference product has been used by Burnaby to test the significance of observed agreements between Pleistocene varved sequences

in New York. In these sequences, autocorrelation effects are strong; this method of cross-comparison is especially effective.

Operation instructions for this program are identical to those given for Program 2 with the following exception:

- CARD 1 - This is a control card
- Col. 1-3 Integer giving length of sliding step.
- Col. 4-5 Blank.
- Col. 6 Selection of match direction.
 - 1 = forward and reverse matches.
 - 0 = no reverse matches.

All other cards are identical to those described in Program 2. Note that there is no provision for autocorrelation using the cross-difference product.

```

C    TIME TREND ANALYSIS -- PROGRAM 3
C    CROSS DIFFERENCE PRODUCT
C    ROBERT SAMPSON -- PROGRAMMER
C    ISU COMPUTER CENTER PROJECT NO. 75
    BEGIN TRACE
    DIMENSION A(351),B(351)
1   READ 1000,INC,IR
    READ 1001
    READ 1002
    N1=0
    N2=0
    IRD=0
2   N1=N1+1
    READ 1003,A(N1)
    IF (A(N1) - 9.0E 48) 2,3,2
3   READ 1002
4   N2=N2+1
    READ 1003,B(N2)
    IF (B(N2) - 9.0E 48) 4,5,4
5   N1 = N1 - 1
    N2 = N2 - 1
6   PUNCH 1001
    IF (IRD) 7,7,8
7   PUNCH 1004
    GO TO 9
8   PUNCH 1005
9   PUNCH 1008,INC
    PUNCH 1006
    NS = 0
    NS1 = 1
    NS2 = N2
    N = INC - 1
    IF (INC - 2) 10,10,11
10  N = INC + 1
11  NE1 = NS1 + N
    NE2 = NS2 - N
12  AN = NE1 - NS1 + 1
    NS = NS + 1
    SE = 0.0
    SEE = 0.0
    N = NE2 - 1
    NE = NE1 - 1

```

```

DO 100 I = NS1 , NE
N = N + 1
E = (A(I)-B(N+1))*(B(N)-A(I+1))
SE = SE + E
100 SEE = SEE + E * E
AN = AN - 1.0
EU = SE / AN
T = 9999.9999
IF (EU) 13,14,13
13 T = EU*SQRT(AN)*(AN-1.0)/(AN*SEE-SE*SE)
14 N = AN + 1.0
NDF = N - 2
NE = NE2
NB = NS2
IF (IRD) 15,15,16
16 NE = N2 - NS2 + 1
NB = N2 - NE2 + 1
15 PUNCH 1007,NS,N,NS1,NE1,NE,NB,EU,T,NDF
NE1 = NE1 + INC
NE2 = NE2 - INC
IF (N1 - NE1) 20,21,21
20 NE1 = NE1 - INC
NE2 = NE2 + INC
NS1 = NS1 + INC
NS2 = NS2 - INC
IF (NE1 - NS1 - 1) 98,98,12
21 IF (NE1 - NS1 + 1 - N2) 12,12,22
22 NS1 = NS1 + INC
NE2 = NE2 + INC
GO TO 12
98 IF (IR) 99,99,17
17 IRD = 1
IR = 0
K = N2 / 2
N = N2 + 1
DO 101 I = 1 , K
C = B(I)
N = N - 1
B(I) = B(N)
101 B(N) = C
GO TO 6
99 STOP 100
GO TO 1
1000 FORMAT (2I3)
1001 FORMAT (40H
140H
1002 FORMAT (1X,////////)
1003 FORMAT (21X,F15.5)
1004 FORMAT (/,32X,15HFORWARD MATCHES,/)
1005 FORMAT (/,32X,15HREVERSE MATCHES,/)
1006 FORMAT (/,19H MATCH NUMBER,6X,1HA,11X,1HB,6X,
116HCROSS DIFFERENCE,
2/,19H POSITION OF TERMS,4X,5HTERMS,7X,5HTERMS,8X,7HPRODUCT,
310X,1HT,8X,4HD.F.,/)
1007 FORMAT (3I8,I4,I8,I4,2F15.4,I6)
1008 FORMAT (14HSLIDING STEP =,I4)
END TRACE
END

```

Program 4 - Cross Association

Cross association is a procedure for matching two sequences on the basis of number of identical elements at each match position. The procedure was devised originally by Sackin and Sneath (1965) for the comparison of amino acid chains. ALGOL and FORTRAN IV programs to compute cross associations have been published by Sackin, Sneath, and Merriam (1965). Development of the method and geologic applications are described more fully in that publication.

Unlike other programs in this package, the cross-association program requires integer data. This data usually represents arbitrarily coded states, such as 1 = limestone, 2 = shale, 3 = sandstone, etc. Two data chains are moved past each other in specified steps and the number of matches in the overlap computed. The binomial probability of a match at any position is given by

$$P_r = \frac{\sum_{j=1}^s \sum_{t=1}^r A_{t,j} B_{t,j}}{m n}, \quad (15)$$

where

$A_{t,j}$ = no. of occurrences of t elements

($t = 1, 2, 3, \dots, r$) in the j th class

($j = 1, 2, 3, \dots, s$) of Chain A,

$B_{t,j}$ = no. of occurrences of t elements

($t = 1, 2, 3, \dots, r$) in the j th class

($j = 1, 2, 3, \dots, s$) of Chain B,

s = length of sliding step,

m = length of Chain A, and

n = length of Chain B.

This is equivalent to

$$P_r = \frac{\text{total number of matches summed over all match positions}}{\text{total number of comparisons summed over all match positions}}$$

At each match position, the program computes and prints the sequential number of the match position, number of terms being compared, the limits of the A terms and B terms, percent of matches, standard deviation, and corrected and uncorrected chi-square values for testing the significance of the matches.

The deviation of the number of matches from the expected number of matches at each position (based on the binomial probability, P_r) is given in terms of standard deviations by

$$\sigma = \sqrt{\lambda + \varphi} \left(2 \arcsin \sqrt{\frac{\lambda}{\lambda + \varphi}} - 2 \arcsin \sqrt{P_r} \right), \quad (16)$$

where

λ = no. of matches, and

φ = no. of mismatches.

The arcsin transformation produces variates which are distributed approximately as a standard normal distribution. The derivation and significance of this

transformation is given in Sackin, Sneath, and Merriam (1965).

The significance of a match may be tested by a contingency table against the hypothesis that the number of matches is equal to the number expected from a random distribution. The statistic from the contingency table is distributed as

χ^2 with one degree of freedom

$$\chi^2 = \frac{(O_\lambda - E_\lambda)^2}{E_\lambda} + \frac{(O_\varphi - E_\varphi)^2}{E_\varphi}, \quad (17)$$

where

O_λ = observed number of matches,

O_φ = observed number of mismatches,

E_λ = expected number of matches = $P_r(\lambda + \varphi)$,

and

E_φ = expected number of mismatches

= $(\lambda + \varphi) - P_r(\lambda + \varphi)$.

If E_λ is small, as in match positions near ends of chains, the contingency table test produces a closer approximation of χ^2 if Yate's correction is applied. The test has the form

$$\chi^2 = \frac{(|O_\lambda - E_\lambda| - 1/2)^2}{E_\lambda} + \frac{(|O_\varphi - E_\varphi| - 1/2)^2}{E_\varphi} \quad (18)$$

with one degree of freedom.

After loading the Program 4 object deck and subroutines, the message LOAD DATA will be typed. The following sequence of cards should be entered into the computer:

CARD 1 - Control card

Col. 1- 3 Integer specifying the length of sliding step.

Col. 4- 5 Blank.

Col. 6 Selection of match direction.
1 = forward and reverse matches.
0 = forward matches only.

Col. 7-16 Lower limit of O. If $O \leq$ limit, a marker line is printed on output at the position of occurrence. Number must contain a decimal.

Col. 17-26 Upper limit of O. If $O \geq$ limit, a marker line is printed on output at the position of occurrence. Number must contain a decimal.

CARD 2 - Title card. This card contains any desired alphanumeric information in col. 1-80.

CARD 3 - This is the first data card of Chain A. Up to 350 cards may be included in this set, which must be equal to or longer than Chain B.

Col. 1-10 Values of y . These numbers must contain a decimal point.

END CARD - This card is placed at the end of Chain A and contains the number 9.0E 48 punched in col. 1-10.

CARD 4 - This is the first data card of Chain B. Up to 350 data cards may be included in this set, which must not be longer than Chain A.

Col. 1-10 Values of y . These numbers must contain a decimal point.

END CARD - A card containing the number 9.0E 48 in col. 1-10 should be placed at the end of Chain B.

Operation of this program requires two special functions, DRH and DLH, which respectively drop the fractional and integer parts of a number. These are included in the library of PDQ FORTRAN II, but it may be necessary to add them as subprograms to other compiler systems.

```
C    TIME TREND ANALYSIS -- PROGRAM 4
C    CROSS ASSOCIATION
C    ISU COMPUTER CENTER PROJECT NUMBER 75
C    ROBERT SAMPSON -- PROGRAMMER
    DIMENSION A(351)
    BEGIN TRACE
1   READ 1000,INC,IR,SDL,SDH
    READ 1001
    N1=0
    N2=0
    SUM=0.0
    SUM1=0.0
    IRD=0
2   READ 1003,B
    IF (B-9.0E 48) 4,7,4
4   N1=N1+1
    A(N1)=B
    GO TO 2
7   READ 1003,B
    IF (B-9.0E 48) 5,6,5
5   N2=N2+1
    A(N2)=A(N2)+B/10000.0
    GO TO 7
6   PUNCH 1001
    IF (IRD) 8,8,9
8   PUNCH 1007
    GO TO 10
9   PUNCH 1005
10  PUNCH 1008,INC
    DO 101 NM=1,2
    GO TO (18,13),NM
18  IF (IRD) 13,13,25
13  NS1=1
    NS2=N2
    NE1=NS1+INC-1
    NE2=NS2-INC+1
    NS=0
    SCHI=0.0
14  NS=NS+1
    AMAT=0.0
    N=NE2-1
    TMP=NE1-NS1+1
    DO 102 J=NS1,NE1
    N=N+1
    IF (DRH(A(J))-DLH(A(N))*10000.0) 102,15,102
15  AMAT=AMAT+1.0
102 CONTINUE
    GO TO (16,17),NM
16  SUM=SUM+AMAT
    SUM1=SUM1+TMP
    GO TO 19
```

```

17 R=AMAT/TMP
   E=TMP*PR
   EP=TMP-E
   OP=TMP-AMAT
   CHI=((AMAT-E)**2)/E+((OP-EP)**2)/EP
   CHIY=((ABS(AMAT-E)-.5)**2)/E+((ABS(OP-EP)-.5)**2)/EP
   SCHI=SCHI+CHI
   X=SQRT(R)
   EXECUTE PROCEDURE 5000
   SD=SQRT(TMP)*2.0*(ASX-ASPR)
   IF (SD-SDL) 61,61,60
60 IF (SD-SDH) 19,61,61
61 N=TMP
   R=R*100.0
   NE=NE2
   NB=NS2
   IF (IRD) 30,30,31
31 NE=N2-NS2+1
   NB=N2-NE2+1
30 PUNCH 1004,NS,N,NS1,NE1,NE,NB,R,SD,CHI,CHIY
19 NE1=NE1+INC
   NE2=NE2-INC
   IF (N1-NE1) 20,21,21
20 NE1=NE1-INC
   NE2=NE2+INC
   NS1=NS1+INC
   NS2=NS2-INC
   IF (NE1-NS1) 98,14,14
21 IF (NE1-NS1+1-N2) 14,14,22
22 NS1=NS1+INC
   NE2=NE2+INC
   GO TO 14
98 GO TO (24,23),NM
23 PUNCH 1010,SCHI
   GO TO 101
24 PR=SUM/SUM1
   X=SQRT(PR)
   EXECUTE PROCEDURE 5000
   ASPR=ASX
25 PUNCH 1009,PR
   PUNCH 1006
101 CONTINUE
   IF (IR) 99,99,32
32 IRD=1
   IR=0
   K=N2/2
   N=N2+1
   DO 103 I=1,K
   C=DLH(A(I))
   N=N-1
   A(I)=DRH(A(I))+DLH(A(N))
103 A(N)=DRH(A(N))+C
   GO TO 6
99 STOP 100
   GO TO 1
   BEGIN PROCEDURE 5000
   ASX=1.5707963
   IF (X-1.0) 70,71,71
70 ASX=ATAN(X/SQRT(1.0-X*X))
71 END PROCEDURE 5000
1000 FORMAT (2I3,2F10.2)

```

```

1001 FORMAT (40H
      140H
1003 FORMAT (F10.2)
1004 FORMAT (3I8,I4I8,I4,4F10.4)
1005 FORMAT (/ ,32X,15HREVERSE MATCHES,/)
1006 FORMAT (/ ,50H MATCH NUMBER          A          B          PER CENT,
      129H STANDARD CHI-SQ          CHI-SQ,/,
      259HPOSITION OF TERMS          TERMS          TERMS MATCHS DEVIATION,
      31X,19HUNCORRECTED (YATES),/)
1007 FORMAT (/ ,32X,15HFORWARD MATCHES,/)
1008 FORMAT (14HSLIDING STEP = ,I4,/)
1009 FORMAT (14HPROB(MATCH) = ,F12.8)
1010 FORMAT (/ ,26HSUM CHI-SQ(UNCORRECTED) = ,F15.6)
      END TRACE
      END

```

Discussion

These programs were written for a particular study and reflect the objectives of that work. Reviewers have suggested several simple modifications to the programs that may increase their versatility and make them more useful for other types of problems. The suggested changes include:

(1) Modification of Program 1 to give an alternative method of obtaining equally spaced data, by true point sampling. That is, at specified intervals the actual lithology

encountered is taken as datum for the point. Provision must be made for the situation if the point falls on a boundary.

(2) Modification of Program 1 to give smoothed data formed by the averaging of nonoverlapping intervals. This would be useful for time-series analysis.

(3) Modification of Program 2 to produce autocovariances as well as autocorrelation. Autocovariances may then be used directly for power-spectrum calculations.

REFERENCES

- Burnaby, T. P., 1953, A suggested alternative to the correlation coefficient for testing the significance of agreement between pairs of time series, and its application to geological data: *Nature*, v. 172, no. 4370, p. 210-211.
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- Sackin, M. J., and Sneath, P. H. A., 1965, Amino acid sequences of proteins: a computer study: *Biochem. Jour.*, v. 96, p. 70P-71P.
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- Whittaker, E. T., and Robinson, G., 1926, *The calculus of observations, a treatise of numerical mathematics*, 2nd ed: Blackie and Son, Ltd., 395 p.

APPENDIX

Program Application from Pennsylvanian of Kansas

Drilling-time logs, records of the time necessary to drill 1-, 5-, or 10-foot intervals of rock section, are available for thousands of wells in the Midcontinent region. They are extremely valuable in correlating stratigraphic units from well to well and can be used for this purpose with almost the same reliability as electric and radioactivity logs.

Drilling time is plotted on log strips so depth is the vertical scale (usually plotted at 50 or 100 feet to the inch to correspond to the vertical scale of other logs), and time is the horizontal scale, time increasing to the right. Soft beds drill rapidly, hard beds drill slowly, and intermediate beds drill at in between rates. If drilling time is plotted against depth, and the points connected, a curve results that resembles other types of mechanical logs. This curve, of course, represents bed hardness which to a degree reflects lithology.

Because the original data is in digitized form, it is easily adapted for time-trend analysis. Additional information, beyond that of simple bed to bed correlation, may be gained by subjecting

this raw data to various time-trend analyses. Data illustrating this program package were taken from an unpublished manuscript by D. F. Merriam (personal communication, 1967).

In Merriam's work, portions of the drilling-time logs for five wells in central Kansas were subjected to time-trend analysis. Partial output is listed here. For each well, 100 values at 5-foot intervals were used in the stratigraphic interval which includes the Lansing-Kansas City Groups (Missourian, Upper Pennsylvanian). Correlation of the original data from well to well was obscure because of large variance in drilling time; part of this "noise" can be attributed to recording error.

It was anticipated that the time-trend analysis would (1) aid in eliminating some "noise" and help in the visual correlation of the different beds from well to well, (2) give data on the overall trend of increasing or decreasing carbonate content with stratigraphic position, and (3) emphasize differences (changes in lithology as revealed by drilling time) of certain beds to allow a meaningful and more complete analysis of the changes in the stratigraphic sequence.

The following listings are included to illustrate the form of output from the time-trend package.

Sample input data with control, title, and END card.

```
001005 5.0
PRODUCERS CORP. OF NEVADA, NO. 1 MANEVAL SEC 12, T 13 S, R 2 W WELL NUM. 1 -
5.00 6.00 5.00 8.00 5.00 4.00 5.00 8.00
5.00 5.00 5.00 8.00 5.00 7.00 5.00 7.00
5.00 4.00 5.00 6.00 5.00 5.00 5.00 8.00
5.00 4.00 5.00 7.00 5.00 5.00 5.00 9.00
5.00 5.00 5.00 6.00 5.00 5.00 5.00 8.00
5.00 5.00 5.00 7.00 5.00 5.00 5.00 9.00
5.00 6.00 5.00 5.00 5.00 5.00 5.00 11.00
5.00 5.00 5.00 2.00 5.00 5.00 5.00 7.00
5.00 4.00 5.00 3.00 5.00 3.00 5.00 6.00
5.00 5.00 5.00 8.00 5.00 1.00 5.00 5.00
5.00 4.00 5.00 7.00 5.00 1.00 5.00 7.00
5.00 3.00 5.00 6.00 5.00 5.00 5.00 4.00
5.00 5.00 5.00 7.00 5.00 6.00 5.00 5.00
5.00 6.00 5.00 7.00 5.00 7.00 5.00 5.00
5.00 5.00 5.00 6.00 5.00 6.00 5.00 7.00
5.00 4.00 5.00 4.00 5.00 5.00 5.00 5.00
5.00 8.00 5.00 6.00 5.00 6.00 5.00 5.00
5.00 4.00 5.00 6.00 5.00 5.00 5.00 3.00
5.00 5.00 5.00 4.00 5.00 7.00 5.00 6.00
5.00 6.00 5.00 5.00 5.00 3.00 5.00 4.00
5.00 7.00 5.00 6.00 5.00 6.00 5.00 6.00
5.00 5.00 5.00 5.00 5.00 7.00 5.00 6.00
5.00 9.00 5.00 6.00 5.00 7.00 5.00 6.00
5.00 8.00 5.00 7.00 5.00 6.00 5.00 5.00
5.00 10.00 5.00 6.00 5.00 8.00 5.00 6.00
9.0E 48
```

Pass 1 output giving equally spaced data. Note that data are integral because equal-spacing interval corresponds to distance between original data points.

PRODUCERS CORP. OF NEVADA, NO. 1 MANEVAL SEC 12, T 13 S, R 2 W WELL NUM. 1 -

EQUAL SPACED DATA

INTERVAL = 5.0000

| UNIT | CUMULATIVE TOTAL | VALUE | | | |
|------|------------------|----------|-----|-----------|----------|
| 1 | 5.00000 | 6.00000 | 51 | 255.00000 | 4.00000 |
| 2 | 10.00000 | 5.00000 | 52 | 260.00000 | 7.00000 |
| 3 | 15.00000 | 4.00000 | 53 | 265.00000 | 5.00000 |
| 4 | 20.00000 | 4.00000 | 54 | 270.00000 | 5.00000 |
| 5 | 25.00000 | 5.00000 | 55 | 275.00000 | 5.00000 |
| 6 | 30.00000 | 5.00000 | 56 | 280.00000 | 5.00000 |
| 7 | 35.00000 | 6.00000 | 57 | 285.00000 | 5.00000 |
| 8 | 40.00000 | 5.00000 | 58 | 290.00000 | 5.00000 |
| 9 | 45.00000 | 4.00000 | 59 | 295.00000 | 3.00000 |
| 10 | 50.00000 | 5.00000 | 60 | 300.00000 | 1.00000 |
| 11 | 55.00000 | 4.00000 | 61 | 305.00000 | 1.00000 |
| 12 | 60.00000 | 3.00000 | 62 | 310.00000 | 5.00000 |
| 13 | 65.00000 | 5.00000 | 63 | 315.00000 | 6.00000 |
| 14 | 70.00000 | 6.00000 | 64 | 320.00000 | 7.00000 |
| 15 | 75.00000 | 5.00000 | 65 | 325.00000 | 6.00000 |
| 16 | 80.00000 | 4.00000 | 66 | 330.00000 | 5.00000 |
| 17 | 85.00000 | 8.00000 | 67 | 335.00000 | 6.00000 |
| 18 | 90.00000 | 4.00000 | 68 | 340.00000 | 5.00000 |
| 19 | 95.00000 | 5.00000 | 69 | 345.00000 | 7.00000 |
| 20 | 100.00000 | 6.00000 | 70 | 350.00000 | 3.00000 |
| 21 | 105.00000 | 7.00000 | 71 | 355.00000 | 6.00000 |
| 22 | 110.00000 | 5.00000 | 72 | 360.00000 | 7.00000 |
| 23 | 115.00000 | 9.00000 | 73 | 365.00000 | 7.00000 |
| 24 | 120.00000 | 8.00000 | 74 | 370.00000 | 6.00000 |
| 25 | 125.00000 | 10.00000 | 75 | 375.00000 | 8.00000 |
| 26 | 130.00000 | 8.00000 | 76 | 380.00000 | 8.00000 |
| 27 | 135.00000 | 8.00000 | 77 | 385.00000 | 7.00000 |
| 28 | 140.00000 | 6.00000 | 78 | 390.00000 | 8.00000 |
| 29 | 145.00000 | 7.00000 | 79 | 395.00000 | 9.00000 |
| 30 | 150.00000 | 6.00000 | 80 | 400.00000 | 8.00000 |
| 31 | 155.00000 | 7.00000 | 81 | 405.00000 | 9.00000 |
| 32 | 160.00000 | 5.00000 | 82 | 410.00000 | 11.00000 |
| 33 | 165.00000 | 2.00000 | 83 | 415.00000 | 7.00000 |
| 34 | 170.00000 | 3.00000 | 84 | 420.00000 | 6.00000 |
| 35 | 175.00000 | 8.00000 | 85 | 425.00000 | 5.00000 |
| 36 | 180.00000 | 7.00000 | 86 | 430.00000 | 7.00000 |
| 37 | 185.00000 | 6.00000 | 87 | 435.00000 | 4.00000 |
| 38 | 190.00000 | 7.00000 | 88 | 440.00000 | 5.00000 |
| 39 | 195.00000 | 7.00000 | 89 | 445.00000 | 5.00000 |
| 40 | 200.00000 | 6.00000 | 90 | 450.00000 | 7.00000 |
| 41 | 205.00000 | 4.00000 | 91 | 455.00000 | 5.00000 |
| 42 | 210.00000 | 6.00000 | 92 | 460.00000 | 5.00000 |
| 43 | 215.00000 | 6.00000 | 93 | 465.00000 | 3.00000 |
| 44 | 220.00000 | 4.00000 | 94 | 470.00000 | 6.00000 |
| 45 | 225.00000 | 5.00000 | 95 | 475.00000 | 4.00000 |
| 46 | 230.00000 | 6.00000 | 96 | 480.00000 | 6.00000 |
| 47 | 235.00000 | 5.00000 | 97 | 485.00000 | 6.00000 |
| 48 | 240.00000 | 6.00000 | 98 | 490.00000 | 6.00000 |
| 49 | 245.00000 | 7.00000 | 99 | 495.00000 | 5.00000 |
| 50 | 250.00000 | 6.00000 | 100 | 500.00000 | 6.00000 |

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Pass 2 output giving data smoothed by Sheppard's equation, and associated statistics.

PRODUCERS CORP. OF NEVADA, NO. 1 MANEVAL SEC 12, T 13 S, R 2 W WELL NUM. 1 -

5 TERM SMOOTHING EQUATION

INTERVAL = 5.0000

| UNIT | CUM. TOTAL | SMOOTHED VALUE | VALUE | DEVIATION |
|------|------------|----------------|----------|-----------|
| 1 | 15.00000 | 5.51428 | 5.00000 | -.51428 |
| 2 | 20.00000 | 4.08571 | 4.00000 | -.08571 |
| 3 | 25.00000 | 4.17142 | 4.00000 | -.17142 |
| 4 | 30.00000 | 4.65714 | 5.00000 | .34285 |
| 5 | 35.00000 | 5.42857 | 5.00000 | -.42857 |
| 6 | 40.00000 | 5.57142 | 6.00000 | .42857 |
| 7 | 45.00000 | 5.00000 | 5.00000 | .00000 |
| 8 | 50.00000 | 4.51428 | 4.00000 | -.51428 |
| 9 | 55.00000 | 4.48571 | 5.00000 | .51428 |
| 10 | 60.00000 | 3.91428 | 4.00000 | .08571 |
| 11 | 65.00000 | 3.60000 | 3.00000 | -.60000 |
| 12 | 70.00000 | 4.74285 | 5.00000 | .25714 |
| 13 | 75.00000 | 5.74285 | 6.00000 | .25714 |
| 14 | 80.00000 | 4.74285 | 5.00000 | .25714 |
| 15 | 85.00000 | 5.54285 | 4.00000 | -1.54285 |
| 16 | 90.00000 | 5.77142 | 8.00000 | 2.22857 |
| 17 | 95.00000 | 5.54285 | 4.00000 | -1.54285 |
| 18 | 100.00000 | 4.57142 | 5.00000 | .42857 |
| 19 | 105.00000 | 6.25714 | 6.00000 | -.25714 |
| 20 | 110.00000 | 5.97142 | 7.00000 | 1.02857 |
| 21 | 115.00000 | 6.71428 | 5.00000 | -1.71428 |
| 22 | 120.00000 | 7.37142 | 9.00000 | 1.62857 |
| 23 | 125.00000 | 9.28571 | 8.00000 | -1.28571 |
| 24 | 130.00000 | 8.88571 | 10.00000 | 1.11428 |
| 25 | 135.00000 | 8.85714 | 8.00000 | -.85714 |
| 26 | 140.00000 | 7.22857 | 8.00000 | .77142 |
| 27 | 145.00000 | 6.85714 | 6.00000 | -.85714 |
| 28 | 150.00000 | 6.22857 | 7.00000 | .77142 |
| 29 | 155.00000 | 6.77142 | 6.00000 | -.77142 |
| 30 | 160.00000 | 6.40000 | 7.00000 | .60000 |
| 31 | 165.00000 | 4.74285 | 5.00000 | .25714 |
| 32 | 170.00000 | 2.42857 | 2.00000 | -.42857 |
| 33 | 175.00000 | 3.85714 | 3.00000 | -.85714 |
| 34 | 180.00000 | 6.62857 | 8.00000 | 1.37142 |
| 35 | 185.00000 | 7.34285 | 7.00000 | -.34285 |
| 36 | 190.00000 | 6.42857 | 6.00000 | -.42857 |
| 37 | 195.00000 | 6.74285 | 7.00000 | .25714 |
| 38 | 200.00000 | 7.00000 | 7.00000 | .00000 |
| 39 | 205.00000 | 5.57142 | 6.00000 | .42857 |
| 40 | 210.00000 | 4.94285 | 4.00000 | -.94285 |
| 41 | 215.00000 | 5.48571 | 6.00000 | .51428 |
| 42 | 220.00000 | 5.57142 | 6.00000 | .42857 |
| 43 | 225.00000 | 4.68571 | 4.00000 | -.68571 |
| 44 | 230.00000 | 4.91428 | 5.00000 | .08571 |
| 45 | 235.00000 | 5.48571 | 6.00000 | .51428 |
| 46 | 240.00000 | 5.51428 | 5.00000 | -.51428 |
| 47 | 245.00000 | 6.00000 | 6.00000 | .00000 |
| 48 | 250.00000 | 6.74285 | 7.00000 | .25714 |
| 49 | 255.00000 | 5.57142 | 6.00000 | .42857 |
| 50 | 260.00000 | 5.37142 | 4.00000 | -1.37142 |

| | | | | |
|----|-----------|---------|----------|----------|
| 51 | 265.00000 | 5.54285 | 7.00000 | 1.45714 |
| 52 | 270.00000 | 5.77142 | 5.00000 | -.77142 |
| 53 | 275.00000 | 4.82857 | 5.00000 | .17142 |
| 54 | 280.00000 | 5.00000 | 5.00000 | .00000 |
| 55 | 285.00000 | 5.00000 | 5.00000 | .00000 |
| 56 | 290.00000 | 5.17142 | 5.00000 | -.17142 |
| 57 | 295.00000 | 4.65714 | 5.00000 | .34285 |
| 58 | 300.00000 | 3.00000 | 3.00000 | .00000 |
| 59 | 305.00000 | 1.00000 | 1.00000 | .00000 |
| 60 | 310.00000 | 1.77142 | 1.00000 | -.77142 |
| 61 | 315.00000 | 4.14285 | 5.00000 | .85714 |
| 62 | 320.00000 | 6.42857 | 6.00000 | -.42857 |
| 63 | 325.00000 | 6.65714 | 7.00000 | .34285 |
| 64 | 330.00000 | 6.00000 | 6.00000 | .00000 |
| 65 | 335.00000 | 5.51428 | 5.00000 | -.51428 |
| 66 | 340.00000 | 5.22857 | 6.00000 | .77142 |
| 67 | 345.00000 | 6.20000 | 5.00000 | -1.20000 |
| 68 | 350.00000 | 5.11428 | 7.00000 | 1.88571 |
| 69 | 355.00000 | 4.88571 | 3.00000 | -1.88571 |
| 70 | 360.00000 | 5.14285 | 6.00000 | .85714 |
| 71 | 365.00000 | 7.08571 | 7.00000 | -.08571 |
| 72 | 370.00000 | 6.65714 | 7.00000 | .34285 |
| 73 | 375.00000 | 6.77142 | 6.00000 | -.77142 |
| 74 | 380.00000 | 7.48571 | 8.00000 | .51428 |
| 75 | 385.00000 | 7.82857 | 8.00000 | .17142 |
| 76 | 390.00000 | 7.42857 | 7.00000 | -.42857 |
| 77 | 395.00000 | 8.00000 | 8.00000 | .00000 |
| 78 | 400.00000 | 8.48571 | 9.00000 | .51428 |
| 79 | 405.00000 | 8.42857 | 8.00000 | -.42857 |
| 80 | 410.00000 | 9.51428 | 9.00000 | -.51428 |
| 81 | 415.00000 | 9.62857 | 11.00000 | 1.37142 |
| 82 | 420.00000 | 8.02857 | 7.00000 | -1.02857 |
| 83 | 425.00000 | 5.48571 | 6.00000 | .51428 |
| 84 | 430.00000 | 5.94285 | 5.00000 | -.94285 |
| 85 | 435.00000 | 5.54285 | 7.00000 | 1.45714 |
| 86 | 440.00000 | 5.20000 | 4.00000 | -1.20000 |
| 87 | 445.00000 | 4.31428 | 5.00000 | .68571 |
| 88 | 450.00000 | 5.77142 | 5.00000 | -.77142 |
| 89 | 455.00000 | 5.97142 | 7.00000 | 1.02857 |
| 90 | 460.00000 | 5.85714 | 5.00000 | -.85714 |
| 91 | 465.00000 | 4.05714 | 5.00000 | .94285 |
| 92 | 470.00000 | 4.45714 | 3.00000 | -1.45714 |
| 93 | 475.00000 | 4.37142 | 6.00000 | 1.62857 |
| 94 | 480.00000 | 5.28571 | 4.00000 | -1.28571 |
| 95 | 485.00000 | 5.31428 | 6.00000 | .68571 |
| 96 | 490.00000 | 6.25714 | 6.00000 | -.25714 |
| 97 | 495.00000 | 5.65714 | 6.00000 | .34285 |

9.0F 48

PRODUCERS CORP. OF NEVADA, NO. 1 MANEVAL SEC 12, T 13 S, R 2 W WELL NUM. 1 -
TOTAL THICKNESS = 500.000
TOTAL EQUAL SPACED DATA = 500.0000
TOTAL SMOOTHED THICKNESS = 480.0000
GOODNESS OF FIT = .7697
5 TERM SMOOTHING EQUATION
EXPECTED NO. RUNS = 64.3 OBSERVED NO. RUNS = 44.0 CH12 = 19.9084
STANDARD DEVIATION = 1.5121
EQUAL SPACED DATA
EXPECTED NO. RUNS = 66.3 OBSERVED NO. RUNS = 54.0 CH12 = 7.0966
STANDARD DEVIATION = 1.7182
SLOPE(B) = .0013 T = 1.1269 WITH 98 DEGREES OF FREEDOM

Program 2 cross-correlation between well 1 and well 4, both smoothed by Sheppard's equation. Incomplete listings of both forward and reverse matches are given.

5 TERM SMOOTHING EQUATION FOR WELL 1 VS. 5 TERM SMOOTHING EQUATION FOR WELL 4 -

FORWARD MATCHES

SLIDING STEP = 1

| MATCH POSITION | NUMBER OF TERMS | A TERMS | B TERMS | CROSS-CORRELATION COEFFICIENT | T | D.F. |
|----------------|-----------------|---------|---------|-------------------------------|---------|------|
| 1 | 3 | 1 3 | 100 102 | .8381 | 1.5366 | 1 |
| 2 | 4 | 1 4 | 99 102 | -.9811 | -7.1793 | 2 |
| 3 | 5 | 1 5 | 98 102 | -.5435 | -1.1216 | 3 |
| 4 | 6 | 1 6 | 97 102 | -.0265 | -.0530 | 4 |
| 5 | 7 | 1 7 | 96 102 | .8437 | 3.5155 | 5 |
| 6 | 8 | 1 8 | 95 102 | .6445 | 2.0649 | 6 |
| 7 | 9 | 1 9 | 94 102 | -.3247 | -.9086 | 7 |
| 8 | 10 | 1 10 | 93 102 | -.7290 | -3.0123 | 8 |
| 9 | 11 | 1 11 | 92 102 | -.3777 | -1.2239 | 9 |
| 10 | 12 | 1 12 | 91 102 | .0355 | .1126 | 10 |
| 11 | 13 | 1 13 | 90 102 | .0878 | .2923 | 11 |
| 12 | 14 | 1 14 | 89 102 | -.1400 | -.4900 | 12 |
| 13 | 15 | 1 15 | 88 102 | .0600 | .2168 | 13 |
| 14 | 16 | 1 16 | 87 102 | .2745 | 1.0683 | 14 |
| 15 | 17 | 1 17 | 86 102 | .1937 | .7646 | 15 |
| 16 | 18 | 1 18 | 85 102 | -.0011 | -.0046 | 16 |
| 17 | 19 | 1 19 | 84 102 | .2572 | 1.0978 | 17 |
| 18 | 20 | 1 20 | 83 102 | .4310 | 2.0268 | 18 |
| 19 | 21 | 1 21 | 82 102 | .4786 | 2.3764 | 19 |
| 20 | 22 | 1 22 | 81 102 | .4702 | 2.3827 | 20 |
| 21 | 23 | 1 23 | 80 102 | .4819 | 2.5207 | 21 |
| 22 | 24 | 1 24 | 79 102 | .4806 | 2.5706 | 22 |
| 23 | 25 | 1 25 | 78 102 | .5447 | 3.1153 | 23 |
| 24 | 26 | 1 26 | 77 102 | .6014 | 3.6885 | 24 |
| 25 | 27 | 1 27 | 76 102 | .6458 | 4.2293 | 25 |
| 26 | 28 | 1 28 | 75 102 | .5748 | 3.5823 | 26 |
| 27 | 29 | 1 29 | 74 102 | .5253 | 3.2083 | 27 |
| 28 | 30 | 1 30 | 73 102 | .4733 | 2.8434 | 28 |
| 29 | 31 | 1 31 | 72 102 | .4027 | 2.3696 | 29 |
| 30 | 32 | 1 32 | 71 102 | .2135 | 1.1973 | 30 |
| 31 | 33 | 1 33 | 70 102 | .1529 | .8619 | 31 |
| 32 | 34 | 1 34 | 69 102 | .2244 | 1.3030 | 32 |
| 33 | 35 | 1 35 | 68 102 | .3127 | 1.8914 | 33 |
| 34 | 36 | 1 36 | 67 102 | .3488 | 2.1704 | 34 |
| 35 | 37 | 1 37 | 66 102 | .3293 | 2.0638 | 35 |
| 36 | 38 | 1 38 | 65 102 | .1870 | 1.1425 | 36 |
| 37 | 39 | 1 39 | 64 102 | .0271 | .1650 | 37 |
| 38 | 40 | 1 40 | 63 102 | -.0179 | -.1104 | 38 |
| 39 | 41 | 1 41 | 62 102 | -.0053 | -.0332 | 39 |
| 40 | 42 | 1 42 | 61 102 | -.0745 | -.4728 | 40 |
| 41 | 43 | 1 43 | 60 102 | -.1046 | -.6734 | 41 |
| 42 | 44 | 1 44 | 59 102 | -.0269 | -.1746 | 42 |
| 43 | 45 | 1 45 | 58 102 | .0592 | .3892 | 43 |
| 44 | 46 | 1 46 | 57 102 | -.0437 | -.2905 | 44 |
| 45 | 47 | 1 47 | 56 102 | -.2306 | -1.5902 | 45 |
| 46 | 48 | 1 48 | 55 102 | -.3659 | -2.6669 | 46 |
| 47 | 49 | 1 49 | 54 102 | -.4647 | -3.5980 | 47 |
| 48 | 50 | 1 50 | 53 102 | -.5588 | -4.6693 | 48 |

5 TERM SMOOTHING EQUATION FOR WELL 1 VS. 5 TERM SMOOTHING EQUATION FOR WELL 4 -

REVERSE MATCHES

SLIDING STEP = 1

| MATCH POSITION | NUMBER OF TERMS | A TERMS | B TERMS | CROSS-CORRELATION COEFFICIENT | T | D.F. |
|----------------|-----------------|---------|---------|-------------------------------|---------|------|
| 1 | 3 | 1 3 | 1 3 | .0000* | .0000 | 1 |
| 2 | 4 | 1 4 | 1 4 | .0000* | .0000 | 2 |
| 3 | 5 | 1 5 | 1 5 | .0000* | .0000 | 3 |
| 4 | 6 | 1 6 | 1 6 | .0000* | .0000 | 4 |
| 5 | 7 | 1 7 | 1 7 | .4182 | 1.0297 | 5 |
| 6 | 8 | 1 8 | 1 8 | -.0699 | -.1717 | 6 |
| 7 | 9 | 1 9 | 1 9 | -.2952 | -.8176 | 7 |
| 8 | 10 | 1 10 | 1 10 | -.2017 | -.5826 | 8 |
| 9 | 11 | 1 11 | 1 11 | .1129 | .3411 | 9 |
| 10 | 12 | 1 12 | 1 12 | .4409 | 1.5535 | 10 |
| 11 | 13 | 1 13 | 1 13 | .4352 | 1.6033 | 11 |
| 12 | 14 | 1 14 | 1 14 | .3324 | 1.2209 | 12 |
| 13 | 15 | 1 15 | 1 15 | .0611 | .2210 | 13 |
| 14 | 16 | 1 16 | 1 16 | -.2836 | -1.1069 | 14 |
| 15 | 17 | 1 17 | 1 17 | -.6086 | -2.9707 | 15 |
| 16 | 18 | 1 18 | 1 18 | -.5836 | -2.8748 | 16 |
| 17 | 19 | 1 19 | 1 19 | -.4777 | -2.2425 | 17 |
| 18 | 20 | 1 20 | 1 20 | -.5118 | -2.5275 | 18 |
| 19 | 21 | 1 21 | 1 21 | -.4351 | -2.1066 | 19 |
| 20 | 22 | 1 22 | 1 22 | -.4526 | -2.2702 | 20 |
| 21 | 23 | 1 23 | 1 23 | -.5605 | -3.1015 | 21 |
| 22 | 24 | 1 24 | 1 24 | -.6637 | -4.1626 | 22 |
| 23 | 25 | 1 25 | 1 25 | -.7059 | -4.7807 | 23 |
| 24 | 26 | 1 26 | 1 26 | -.7857 | -6.2235 | 24 |
| 25 | 27 | 1 27 | 1 27 | -.7601 | -5.8503 | 25 |
| 26 | 28 | 1 28 | 1 28 | -.6153 | -3.9802 | 26 |
| 27 | 29 | 1 29 | 1 29 | -.4491 | -2.6119 | 27 |
| 28 | 30 | 1 30 | 1 30 | -.3422 | -1.9273 | 28 |
| 29 | 31 | 1 31 | 1 31 | -.2142 | -1.1809 | 29 |
| 30 | 32 | 1 32 | 1 32 | -.1170 | -.6455 | 30 |
| 31 | 33 | 1 33 | 1 33 | -.1083 | -.6070 | 31 |
| 32 | 34 | 1 34 | 1 34 | -.1639 | -.9404 | 32 |
| 33 | 35 | 1 35 | 1 35 | -.1738 | -1.0142 | 33 |
| 34 | 36 | 1 36 | 1 36 | -.1633 | -.9652 | 34 |
| 35 | 37 | 1 37 | 1 37 | -.2442 | -1.4902 | 35 |
| 36 | 38 | 1 38 | 1 38 | -.3985 | -2.6071 | 36 |
| 37 | 39 | 1 39 | 1 39 | -.4553 | -3.1110 | 37 |
| 38 | 40 | 1 40 | 1 40 | -.3877 | -2.5930 | 38 |
| 39 | 41 | 1 41 | 1 41 | -.3075 | -2.0188 | 39 |
| 40 | 42 | 1 42 | 1 42 | -.1892 | -1.2189 | 40 |
| 41 | 43 | 1 43 | 1 43 | -.0609 | -.3908 | 41 |
| 42 | 44 | 1 44 | 1 44 | .0164 | .1067 | 42 |
| 43 | 45 | 1 45 | 1 45 | .0223 | .1467 | 43 |
| 44 | 46 | 1 46 | 1 46 | .0744 | .4952 | 44 |
| 45 | 47 | 1 47 | 1 47 | .0651 | .4379 | 45 |
| 46 | 48 | 1 48 | 1 48 | -.0139 | -.0946 | 46 |
| 47 | 49 | 1 49 | 1 49 | -.0916 | -.6313 | 47 |
| 48 | 50 | 1 50 | 1 50 | -.1310 | -.9157 | 48 |
| 49 | 51 | 1 51 | 1 51 | -.1775 | -1.2632 | 49 |
| 50 | 52 | 1 52 | 1 52 | -.1741 | -1.2507 | 50 |
| 51 | 53 | 1 53 | 1 53 | -.0764 | -.5472 | 51 |
| 52 | 54 | 1 54 | 1 54 | .0107 | .0772 | 52 |

Program 2 auto-correlation of data from well 1 smoothed by Sheppard's equation. Incomplete examples of both forward and reverse matches are listed.

5 TERM SMOOTHING EQUATION FOR WELL 1

FORWARD MATCHES

SLIDING STEP = 1

| MATCH POSITION | NUMBER OF TERMS | A TERMS | B TERMS | AUTO-CORRELATION COEFFICIENT | T | D.F. |
|----------------|-----------------|---------|---------|------------------------------|---------|------|
| 1 | 3 | 1 3 | 95 97 | -.8102 | -1.3823 | 1 |
| 2 | 4 | 1 4 | 94 97 | -.4726 | -.7585 | 2 |
| 3 | 5 | 1 5 | 93 97 | -.3042 | -.5531 | 3 |
| 4 | 6 | 1 6 | 92 97 | .4023 | .8789 | 4 |
| 5 | 7 | 1 7 | 91 97 | .4430 | 1.1050 | 5 |
| 6 | 8 | 1 8 | 90 97 | .6436 | 2.0602 | 6 |
| 7 | 9 | 1 9 | 89 97 | .0049 | .0130 | 7 |
| 8 | 10 | 1 10 | 88 97 | -.5235 | -1.7379 | 8 |
| 9 | 11 | 1 11 | 87 97 | -.8781 | -5.5064 | 9 |
| 10 | 12 | 1 12 | 86 97 | -.3090 | -1.0274 | 10 |
| 11 | 13 | 1 13 | 85 97 | .3635 | 1.2945 | 11 |
| 12 | 14 | 1 14 | 84 97 | .6106 | 2.6711 | 12 |
| 13 | 15 | 1 15 | 83 97 | .2673 | 1.0005 | 13 |
| 14 | 16 | 1 16 | 82 97 | .3399 | 1.3527 | 14 |
| 15 | 17 | 1 17 | 81 97 | .0825 | .3208 | 15 |
| 16 | 18 | 1 18 | 80 97 | -.1721 | -.6991 | 16 |
| 17 | 19 | 1 19 | 79 97 | -.3515 | -1.5483 | 17 |
| 18 | 20 | 1 20 | 78 97 | -.1448 | -.6211 | 18 |
| 19 | 21 | 1 21 | 77 97 | -.0933 | -.4087 | 19 |
| 20 | 22 | 1 22 | 76 97 | -.0945 | -.4247 | 20 |
| 21 | 23 | 1 23 | 75 97 | -.2006 | -.9385 | 21 |
| 22 | 24 | 1 24 | 74 97 | -.2535 | -1.2296 | 22 |
| 23 | 25 | 1 25 | 73 97 | -.4270 | -2.2647 | 23 |
| 24 | 26 | 1 26 | 72 97 | -.5563 | -3.2798 | 24 |
| 25 | 27 | 1 27 | 71 97 | -.6853 | -4.7055 | 25 |
| 26 | 28 | 1 28 | 70 97 | -.6516 | -4.3802 | 26 |
| 27 | 29 | 1 29 | 69 97 | -.6421 | -4.3532 | 27 |
| 28 | 30 | 1 30 | 68 97 | -.5306 | -3.3132 | 28 |
| 29 | 31 | 1 31 | 67 97 | -.4296 | -2.5620 | 29 |
| 30 | 32 | 1 32 | 66 97 | -.3050 | -1.7544 | 30 |
| 31 | 33 | 1 33 | 65 97 | -.3582 | -2.1363 | 31 |
| 32 | 34 | 1 34 | 64 97 | -.3017 | -1.7906 | 32 |
| 33 | 35 | 1 35 | 63 97 | -.1885 | -1.1026 | 33 |
| 34 | 36 | 1 36 | 62 97 | -.0440 | -.2572 | 34 |
| 35 | 37 | 1 37 | 61 97 | .0647 | .3838 | 35 |
| 36 | 38 | 1 38 | 60 97 | .2607 | 1.6205 | 36 |
| 37 | 39 | 1 39 | 59 97 | .3706 | 2.4273 | 37 |
| 38 | 40 | 1 40 | 58 97 | .4454 | 3.0669 | 38 |
| 39 | 41 | 1 41 | 57 97 | .5148 | 3.7505 | 39 |
| 40 | 42 | 1 42 | 56 97 | .5511 | 4.1774 | 40 |
| 41 | 43 | 1 43 | 55 97 | .4819 | 3.5221 | 41 |
| 42 | 44 | 1 44 | 54 97 | .4160 | 2.9654 | 42 |
| 43 | 45 | 1 45 | 53 97 | .4697 | 3.4896 | 43 |
| 44 | 46 | 1 46 | 52 97 | .4883 | 3.7122 | 44 |
| 45 | 47 | 1 47 | 51 97 | .3903 | 2.8438 | 45 |
| 46 | 48 | 1 48 | 50 97 | .2531 | 1.7743 | 46 |
| 47 | 49 | 1 49 | 49 97 | .2223 | 1.5631 | 47 |
| 48 | 50 | 1 50 | 48 97 | .1712 | 1.2045 | 48 |

5 TERM SMOOTHING EQUATION FOR WELL 1

REVERSE MATCHES

SLIDING STEP = 1

| MATCH POSITION OF TERMS | NUMBER OF TERMS | A TERMS | B TERMS | AUTO-CORRELATION COEFFICIENT | T | D.F. |
|----------------------------|--------------------|------------|------------|---------------------------------|---------|------|
| 1 | 3 | 1 3 | 1 3 | -.4046 | -.4424 | 1 |
| 2 | 4 | 1 4 | 1 4 | .4235 | .6611 | 2 |
| 3 | 5 | 1 5 | 1 5 | .8172 | 2.4562 | 3 |
| 4 | 6 | 1 6 | 1 6 | .1346 | .2717 | 4 |
| 5 | 7 | 1 7 | 1 7 | -.7112 | -2.2623 | 5 |
| 6 | 8 | 1 8 | 1 8 | -.7487 | -2.7670 | 6 |
| 7 | 9 | 1 9 | 1 9 | -.0467 | -.1237 | 7 |
| 8 | 10 | 1 10 | 1 10 | .1217 | .3468 | 8 |
| 9 | 11 | 1 11 | 1 11 | .1230 | .3719 | 9 |
| 10 | 12 | 1 12 | 1 12 | .5427 | 2.0437 | 10 |
| 11 | 13 | 1 13 | 1 13 | .4079 | 1.4820 | 11 |
| 12 | 14 | 1 14 | 1 14 | -.4923 | -1.9596 | 12 |
| 13 | 15 | 1 15 | 1 15 | -.4674 | -1.9063 | 13 |
| 14 | 16 | 1 16 | 1 16 | -.2762 | -1.0756 | 14 |
| 15 | 17 | 1 17 | 1 17 | -.0184 | -.0715 | 15 |
| 16 | 18 | 1 18 | 1 18 | -.0383 | -.1535 | 16 |
| 17 | 19 | 1 19 | 1 19 | .3763 | 1.6747 | 17 |
| 18 | 20 | 1 20 | 1 20 | .2729 | 1.2038 | 18 |
| 19 | 21 | 1 21 | 1 21 | .1066 | .4676 | 19 |
| 20 | 22 | 1 22 | 1 22 | -.2577 | -1.1928 | 20 |
| 21 | 23 | 1 23 | 1 23 | -.2463 | -1.1650 | 21 |
| 22 | 24 | 1 24 | 1 24 | -.3204 | -1.5866 | 22 |
| 23 | 25 | 1 25 | 1 25 | -.3853 | -2.0026 | 23 |
| 24 | 26 | 1 26 | 1 26 | -.4619 | -2.5518 | 24 |
| 25 | 27 | 1 27 | 1 27 | -.3608 | -1.9344 | 25 |
| 26 | 28 | 1 28 | 1 28 | -.3259 | -1.7578 | 26 |
| 27 | 29 | 1 29 | 1 29 | -.3906 | -2.2049 | 27 |
| 28 | 30 | 1 30 | 1 30 | -.5178 | -3.2030 | 28 |
| 29 | 31 | 1 31 | 1 31 | -.5749 | -3.7842 | 29 |
| 30 | 32 | 1 32 | 1 32 | -.5426 | -3.5389 | 30 |
| 31 | 33 | 1 33 | 1 33 | -.4046 | -2.4640 | 31 |
| 32 | 34 | 1 34 | 1 34 | -.2955 | -1.7501 | 32 |
| 33 | 35 | 1 35 | 1 35 | -.2850 | -1.7080 | 33 |
| 34 | 36 | 1 36 | 1 36 | -.3928 | -2.4910 | 34 |
| 35 | 37 | 1 37 | 1 37 | -.3350 | -2.1037 | 35 |
| 36 | 38 | 1 38 | 1 38 | -.2573 | -1.5977 | 36 |
| 37 | 39 | 1 39 | 1 39 | -.1487 | -.9151 | 37 |
| 38 | 40 | 1 40 | 1 40 | -.0681 | -.4210 | 38 |
| 39 | 41 | 1 41 | 1 41 | .1214 | .7642 | 39 |
| 40 | 42 | 1 42 | 1 42 | .1934 | 1.2471 | 40 |
| 41 | 43 | 1 43 | 1 43 | .1855 | 1.2093 | 41 |
| 42 | 44 | 1 44 | 1 44 | .1504 | .9859 | 42 |
| 43 | 45 | 1 45 | 1 45 | .3045 | 2.0969 | 43 |
| 44 | 46 | 1 46 | 1 46 | .3808 | 2.7322 | 44 |
| 45 | 47 | 1 47 | 1 47 | .3921 | 2.8597 | 45 |
| 46 | 48 | 1 48 | 1 48 | .3705 | 2.7060 | 46 |
| 47 | 49 | 1 49 | 1 49 | .4179 | 3.1541 | 47 |
| 48 | 50 | 1 50 | 1 50 | .3218 | 2.3553 | 48 |
| 49 | 51 | 1 51 | 1 51 | .2096 | 1.5007 | 49 |
| 50 | 52 | 1 52 | 1 52 | .1495 | 1.0697 | 50 |
| 51 | 53 | 1 53 | 1 53 | .0399 | .2853 | 51 |
| 52 | 54 | 1 54 | 1 54 | -.1969 | -1.4487 | 52 |

Program 3 output listing of cross difference product between wells 1 and 4, smoothed by Sheppard's equation.
 Incomplete listings of both forward and reverse matches are given.

5 TERM SMOOTHING EQUATION FOR WELL 1 VS. 5 TERM SMOOTHING EQUATION FOR WELL 4 -
 FORWARD MATCHES

SLIDING STEP = 1

| MATCH POSITION | NUMBER OF TERMS | A TERMS | B TERMS | CROSS DIFFERENCE PRODUCT | T | D.F. |
|----------------|-----------------|---------|---------|--------------------------|--------|------|
| 1 | 3 | 1 3 | 94 96 | -2.1575 | -.5421 | 1 |
| 2 | 4 | 1 4 | 93 96 | -2.3172 | -.7244 | 2 |
| 3 | 5 | 1 5 | 92 96 | -1.6853 | -.4264 | 3 |
| 4 | 6 | 1 6 | 91 96 | -.9598 | -.4517 | 4 |
| 5 | 7 | 1 7 | 90 96 | -.2439 | -.1711 | 5 |
| 6 | 8 | 1 8 | 89 96 | -.4537 | -.5778 | 6 |
| 7 | 9 | 1 9 | 88 96 | -.9813 | -.2556 | 7 |
| 8 | 10 | 1 10 | 87 96 | -1.2537 | -.2783 | 8 |
| 9 | 11 | 1 11 | 86 96 | -1.2103 | -.1324 | 9 |
| 10 | 12 | 1 12 | 85 96 | -.9353 | -.0771 | 10 |
| 11 | 13 | 1 13 | 84 96 | -.7753 | -.0852 | 11 |
| 12 | 14 | 1 14 | 83 96 | -.7529 | -.2380 | 12 |
| 13 | 15 | 1 15 | 82 96 | -.5913 | -.4257 | 13 |
| 14 | 16 | 1 16 | 81 96 | -.3945 | -.1348 | 14 |
| 15 | 17 | 1 17 | 80 96 | -.4669 | -.0786 | 15 |
| 16 | 18 | 1 18 | 79 96 | -.6192 | -.1238 | 16 |
| 17 | 19 | 1 19 | 78 96 | -.4268 | -.1302 | 17 |
| 18 | 20 | 1 20 | 77 96 | -.2897 | -.1174 | 18 |
| 19 | 21 | 1 21 | 76 96 | -.3002 | -.1167 | 19 |
| 20 | 22 | 1 22 | 75 96 | -.4129 | -.0980 | 20 |
| 21 | 23 | 1 23 | 74 96 | -.6506 | -.0662 | 21 |
| 22 | 24 | 1 24 | 73 96 | -1.1163 | -.0450 | 22 |
| 23 | 25 | 1 25 | 72 96 | -1.4935 | -.0459 | 23 |
| 24 | 26 | 1 26 | 71 96 | -1.7443 | -.0386 | 24 |
| 25 | 27 | 1 27 | 70 96 | -1.9776 | -.0293 | 25 |
| 26 | 28 | 1 28 | 69 96 | -2.5494 | -.0287 | 26 |
| 27 | 29 | 1 29 | 68 96 | -2.9994 | -.0354 | 27 |
| 28 | 30 | 1 30 | 67 96 | -3.3114 | -.0438 | 28 |
| 29 | 31 | 1 31 | 66 96 | -3.4267 | -.0429 | 29 |
| 30 | 32 | 1 32 | 65 96 | -3.8128 | -.0345 | 30 |
| 31 | 33 | 1 33 | 64 96 | -4.0341 | -.0301 | 31 |
| 32 | 34 | 1 34 | 63 96 | -3.7803 | -.0274 | 32 |
| 33 | 35 | 1 35 | 62 96 | -3.6487 | -.0282 | 33 |
| 34 | 36 | 1 36 | 61 96 | -3.6504 | -.0205 | 34 |
| 35 | 37 | 1 37 | 60 96 | -3.7932 | -.0153 | 35 |
| 36 | 38 | 1 38 | 59 96 | -4.3875 | -.0164 | 36 |
| 37 | 39 | 1 39 | 58 96 | -4.8313 | -.0177 | 37 |
| 38 | 40 | 1 40 | 57 96 | -4.7524 | -.0151 | 38 |
| 39 | 41 | 1 41 | 56 96 | -4.6776 | -.0137 | 39 |
| 40 | 42 | 1 42 | 55 96 | -4.9261 | -.0154 | 40 |
| 41 | 43 | 1 43 | 54 96 | -4.9003 | -.0206 | 41 |
| 42 | 44 | 1 44 | 53 96 | -4.4578 | -.0262 | 42 |
| 43 | 45 | 1 45 | 52 96 | -4.0288 | -.0227 | 43 |
| 44 | 46 | 1 46 | 51 96 | -4.3421 | -.0143 | 44 |
| 45 | 47 | 1 47 | 50 96 | -4.9594 | -.0095 | 45 |
| 46 | 48 | 1 48 | 49 96 | -5.4298 | -.0072 | 46 |
| 47 | 49 | 1 49 | 48 96 | -5.6660 | -.0064 | 47 |
| 48 | 50 | 1 50 | 47 96 | -5.9091 | -.0067 | 48 |

5 TERM SMOOTHING EQUATION FOR WELL 1 VS. 5 TERM SMOOTHING EQUATION FOR WELL 4 -

REVERSE MATCHES

SLIDING STEP = 1

| MATCH POSITION | NUMBER OF TERMS | A TERMS | B TERMS | CROSS DIFFERENCE PRODUCT | T | D.F. |
|----------------|-----------------|---------|---------|--------------------------|---------|------|
| 1 | 3 | 1 3 | 1 3 | -1.8930 | -1.7342 | 1 |
| 2 | 4 | 1 4 | 1 4 | -2.0576 | -1.3372 | 2 |
| 3 | 5 | 1 5 | 1 5 | -3.3175 | -.3526 | 3 |
| 4 | 6 | 1 6 | 1 6 | -4.7175 | -.2995 | 4 |
| 5 | 7 | 1 7 | 1 7 | -5.2386 | -1.5245 | 5 |
| 6 | 8 | 1 8 | 1 8 | -5.5814 | -.9847 | 6 |
| 7 | 9 | 1 9 | 1 9 | -6.0718 | -.2293 | 7 |
| 8 | 10 | 1 10 | 1 10 | -6.1953 | -.1332 | 8 |
| 9 | 11 | 1 11 | 1 11 | -5.9451 | -.1138 | 9 |
| 10 | 12 | 1 12 | 1 12 | -5.7525 | -.1126 | 10 |
| 11 | 13 | 1 13 | 1 13 | -5.8833 | -1.229 | 11 |
| 12 | 14 | 1 14 | 1 14 | -5.7888 | -.1435 | 12 |
| 13 | 15 | 1 15 | 1 15 | -5.5922 | -.2075 | 13 |
| 14 | 16 | 1 16 | 1 16 | -5.7676 | -.2618 | 14 |
| 15 | 17 | 1 17 | 1 17 | -6.0066 | -.1873 | 15 |
| 16 | 18 | 1 18 | 1 18 | -5.6988 | -.1347 | 16 |
| 17 | 19 | 1 19 | 1 19 | -5.6660 | -.1165 | 17 |
| 18 | 20 | 1 20 | 1 20 | -6.0468 | -.0851 | 18 |
| 19 | 21 | 1 21 | 1 21 | -6.3652 | -.0765 | 19 |
| 20 | 22 | 1 22 | 1 22 | -6.7100 | -.0574 | 20 |
| 21 | 23 | 1 23 | 1 23 | -7.7672 | -.0379 | 21 |
| 22 | 24 | 1 24 | 1 24 | -9.1880 | -.0223 | 22 |
| 23 | 25 | 1 25 | 1 25 | -10.4346 | -.0183 | 23 |
| 24 | 26 | 1 26 | 1 26 | -11.3314 | -.0165 | 24 |
| 25 | 27 | 1 27 | 1 27 | -11.8907 | -.0138 | 25 |
| 26 | 28 | 1 28 | 1 28 | -11.9998 | -.0116 | 26 |
| 27 | 29 | 1 29 | 1 29 | -11.8382 | -.0103 | 27 |
| 28 | 30 | 1 30 | 1 30 | -11.6677 | -.0098 | 28 |
| 29 | 31 | 1 31 | 1 31 | -11.5042 | -.0096 | 29 |
| 30 | 32 | 1 32 | 1 32 | -11.2369 | -.0095 | 30 |
| 31 | 33 | 1 33 | 1 33 | -11.0518 | -.0097 | 31 |
| 32 | 34 | 1 34 | 1 34 | -10.9885 | -.0106 | 32 |
| 33 | 35 | 1 35 | 1 35 | -11.2541 | -.0122 | 33 |
| 34 | 36 | 1 36 | 1 36 | -11.0304 | -.0128 | 34 |
| 35 | 37 | 1 37 | 1 37 | -10.7467 | -.0136 | 35 |
| 36 | 38 | 1 38 | 1 38 | -10.6723 | -.0152 | 36 |
| 37 | 39 | 1 39 | 1 39 | -10.4653 | -.0166 | 37 |
| 38 | 40 | 1 40 | 1 40 | -9.8084 | -.0176 | 38 |
| 39 | 41 | 1 41 | 1 41 | -9.4570 | -.0184 | 39 |
| 40 | 42 | 1 42 | 1 42 | -9.4090 | -.0166 | 40 |
| 41 | 43 | 1 43 | 1 43 | -9.4069 | -.0134 | 41 |
| 42 | 44 | 1 44 | 1 44 | -9.3346 | -.0122 | 42 |
| 43 | 45 | 1 45 | 1 45 | -9.3532 | -.0127 | 43 |
| 44 | 46 | 1 46 | 1 46 | -9.0682 | -.0150 | 44 |
| 45 | 47 | 1 47 | 1 47 | -8.5771 | -.0194 | 45 |
| 46 | 48 | 1 48 | 1 48 | -8.2760 | -.0251 | 46 |
| 47 | 49 | 1 49 | 1 49 | -8.3784 | -.0289 | 47 |
| 48 | 50 | 1 50 | 1 50 | -8.4515 | -.0308 | 48 |
| 49 | 51 | 1 51 | 1 51 | -8.2936 | -.0300 | 49 |
| 50 | 52 | 1 52 | 1 52 | -8.1060 | -.0228 | 50 |
| 51 | 53 | 1 53 | 1 53 | -8.0853 | -.0150 | 51 |
| 52 | 54 | 1 54 | 1 54 | -8.2402 | -.0107 | 52 |

Control cards and sample input data for Program 4, from Sackin, Sneath, and Merriam (1965), giving coded lithologies found in two Pennsylvanian wells in Kansas and Oklahoma. Refer to the original article for key to the coded states.

```

001001 -100.0 -100.0
NORTHERN OKLAHOMA -- SOUTHERN KANSAS
 7.  9.  1.  1.  1.  9.  8.  6.  6.  9.  7.  7.
 6.  6.  7.  2.  2.  2.  6.  9.  7.  6.  6.  6.
 5.  8.  6.  9.  6.  1.  9.  2.  6.  8.  7.  8.
 6.  6.  9.  8.  9.  2.  6.  1.  3.  6.  6.  6.
 9.  7.  8.  6.  6.  1.  8.  2.  1.  9.  7.  7.
 6.  1.  2.  8.  9.  2.  7.  9.  2.  6.  6.  6.
 7.  9.  8.  6.  3.  9.  6.  6.  9.0E 48  8.  7.  9.
 6.  7.  6.  9.  2.  6.  9.  9.  7.  6.  6.  .0
 8.  6.  5.  6.  4.  8.  6.  6.  6.  1.  7.  7.0
 3.  2.  2.  3.  6.  7.  8.  8.  1.  6.  6.  6.0
                                           5.0
                                           4.0
                                           6.0
                                           9.0E48

```

Partial output listing for cross-association between two wells. Both forward and reverse matches are given.

NORTHERN OKLAHOMA -- SOUTHERN KANSAS

FORWARD MATCHES

SLIDING STEP = 1

PROB(MATCH) = .18378553

| MATCH POSITION | NUMBER OF TERMS | A TERMS | B TERMS | PER CENT MATCHES | STANDARD DEVIATION | CHI-SQ UNCORRECTED | CHI-SQ (YATES) |
|----------------|-----------------|---------|---------|------------------|--------------------|--------------------|----------------|
| 1 | 1 | 1 1 | 36 36 | .0000 | -.8861 | .2251 | .6665 |
| 2 | 2 | 1 2 | 35 36 | 50.0000 | .9682 | 1.3331 | .0584 |
| 3 | 3 | 1 3 | 34 36 | .0000 | -1.5347 | .6755 | .0058 |
| 4 | 4 | 1 4 | 33 36 | 25.0000 | .3221 | .1169 | .0921 |
| 5 | 5 | 1 5 | 32 36 | 60.0000 | 1.9812 | 5.7741 | 3.3328 |
| 6 | 6 | 1 6 | 31 36 | 16.6666 | -.1103 | .0117 | .1753 |
| 7 | 7 | 1 7 | 30 36 | 14.2857 | -.2934 | .0781 | .0434 |
| 8 | 8 | 1 8 | 29 36 | 12.5000 | -.4621 | .1842 | .0007 |
| 9 | 9 | 1 9 | 28 36 | 33.3333 | 1.0345 | 1.3417 | .5300 |
| 10 | 10 | 1 10 | 27 36 | .0000 | -2.8021 | 2.2516 | 1.1931 |
| 11 | 11 | 1 11 | 26 36 | 45.4545 | 1.9689 | 5.3758 | 3.7223 |
| 12 | 12 | 1 12 | 25 36 | 8.3333 | -1.0407 | .8072 | .2764 |
| 13 | 13 | 1 13 | 24 36 | 30.7692 | 1.0452 | 1.3305 | .6327 |
| 14 | 14 | 1 14 | 23 36 | 7.1428 | -1.2909 | 1.1781 | .5482 |
| 15 | 15 | 1 15 | 22 36 | 46.6666 | 2.3933 | 8.0017 | 6.2270 |
| 16 | 16 | 1 16 | 21 36 | .0000 | -3.5444 | 3.6026 | 2.4816 |
| 17 | 17 | 1 17 | 20 36 | 41.1764 | 2.0915 | 5.8901 | 4.4683 |
| 18 | 18 | 1 18 | 19 36 | .0000 | -3.7594 | 4.0530 | 2.9204 |
| 19 | 19 | 1 19 | 18 36 | 52.6315 | 3.2139 | 14.8605 | 12.6648 |
| 20 | 20 | 1 20 | 17 36 | .0000 | -3.9628 | 4.5033 | 3.3615 |
| 21 | 21 | 1 21 | 16 36 | 38.0952 | 2.0359 | 5.4421 | 4.2071 |
| 22 | 22 | 1 22 | 15 36 | 9.0909 | -1.2830 | 1.2650 | .7216 |

| | | | | | | | | | |
|----|----|---|----|----|----|---------|---------|---------|---------|
| 23 | 23 | 1 | 23 | 14 | 36 | 52.1739 | 3.4922 | 17.5116 | 15.3311 |
| 24 | 24 | 1 | 24 | 13 | 36 | .0000 | -4.3410 | 5.4040 | 4.2483 |
| 25 | 25 | 1 | 25 | 12 | 36 | 28.0000 | 1.1454 | 1.5427 | .9680 |
| 26 | 26 | 1 | 26 | 11 | 36 | 15.3846 | -.4079 | .1553 | .0198 |
| 27 | 27 | 1 | 27 | 10 | 36 | 29.6296 | 1.3773 | 2.2784 | 1.5901 |
| 28 | 28 | 1 | 28 | 9 | 36 | 7.1428 | -1.8256 | 2.3563 | 1.6668 |
| 29 | 29 | 1 | 29 | 8 | 36 | 27.5862 | 1.1839 | 1.6390 | 1.0826 |
| 30 | 30 | 1 | 30 | 7 | 36 | 16.6666 | -.2467 | .0586 | .0000 |
| 31 | 31 | 1 | 31 | 6 | 36 | 29.0322 | 1.4028 | 2.3455 | 1.6891 |
| 32 | 32 | 1 | 32 | 5 | 36 | 9.3750 | -1.4919 | 1.7292 | 1.1811 |
| 33 | 33 | 1 | 33 | 4 | 36 | 24.2424 | .8243 | .7564 | .4160 |
| 34 | 34 | 1 | 34 | 3 | 36 | 11.7647 | -1.0839 | .9914 | .5995 |
| 35 | 35 | 1 | 35 | 2 | 36 | 28.5714 | 1.4303 | 2.4240 | 1.7922 |

NORTHERN OKLAHOMA -- SOUTHERN KANSAS

REVERSE MATCHES

SLIDING STEP = 1

PROB(MATCH) = .18378553

| MATCH POSITION | NUMBER OF TERMS | A TERMS | B TERMS | PER CENT MATCHES | STANDARD DEVIATION | CHI-SQ UNCORRECTED | CHI-SQ (YATES) |
|----------------|-----------------|---------|---------|------------------|--------------------|--------------------|----------------|
| 1 | 1 | 1 | 1 | 100.0000 | 2.2554 | 4.4411 | .6665 |
| 2 | 2 | 1 | 2 | .0000 | -1.2531 | .4503 | .0584 |
| 3 | 3 | 1 | 3 | 33.3333 | .5972 | .4472 | .0058 |
| 4 | 4 | 1 | 4 | .0000 | -1.7722 | .9006 | .0921 |
| 5 | 5 | 1 | 5 | 20.0000 | .0920 | .0087 | .2339 |
| 6 | 6 | 1 | 6 | 16.6666 | -.1103 | .0117 | .1753 |
| 7 | 7 | 1 | 7 | 28.5714 | .6396 | .4848 | .0434 |
| 8 | 8 | 1 | 8 | 37.5000 | 1.2218 | 1.9499 | .8835 |
| 9 | 9 | 1 | 9 | 11.1111 | -.6193 | .3168 | .0175 |
| 10 | 10 | 1 | 10 | 30.0000 | .8638 | .9003 | .2922 |
| 11 | 11 | 1 | 11 | .0000 | -2.9388 | 2.4768 | 1.4031 |
| 12 | 12 | 1 | 12 | 41.6666 | 1.7917 | 4.3384 | 2.9248 |
| 13 | 13 | 1 | 13 | 7.6923 | -1.1683 | .9896 | .4054 |
| 14 | 14 | 1 | 14 | 50.0000 | 2.5618 | 9.3320 | 7.3430 |
| 15 | 15 | 1 | 15 | 13.3333 | -.5365 | .2545 | .0293 |
| 16 | 16 | 1 | 16 | 37.5000 | 1.7280 | 3.8998 | 2.7293 |
| 17 | 17 | 1 | 17 | .0000 | -3.6535 | 3.8278 | 2.7007 |
| 18 | 18 | 1 | 18 | 66.6666 | 4.3466 | 27.9793 | 24.8528 |
| 19 | 19 | 1 | 19 | .0000 | -3.8624 | 4.2781 | 3.1407 |
| 20 | 20 | 1 | 20 | 50.0000 | 3.0620 | 13.3314 | 11.3068 |
| 21 | 21 | 1 | 21 | .0000 | -4.0606 | 4.7285 | 3.5827 |
| 22 | 22 | 1 | 22 | 45.4545 | 2.7844 | 10.7516 | 9.0224 |
| 23 | 23 | 1 | 23 | 8.6956 | -1.3785 | 1.4375 | .8645 |
| 24 | 24 | 1 | 24 | 41.6666 | 2.5339 | 8.6768 | 7.1938 |
| 25 | 25 | 1 | 25 | 4.0000 | -2.4169 | 3.4455 | 2.5536 |
| 26 | 26 | 1 | 26 | 26.9230 | 1.0450 | 1.2654 | .7599 |
| 27 | 27 | 1 | 27 | 14.8148 | -.4983 | .2285 | .0527 |
| 28 | 28 | 1 | 28 | 32.1428 | 1.6905 | 3.5363 | 2.6782 |
| 29 | 29 | 1 | 29 | 10.3448 | -1.2450 | 1.2477 | .7696 |
| 30 | 30 | 1 | 30 | 30.0000 | 1.4962 | 2.7010 | 1.9818 |
| 31 | 31 | 1 | 31 | 12.9032 | -.8422 | .6195 | .3082 |
| 32 | 32 | 1 | 32 | 31.2500 | 1.6986 | 3.5341 | 2.7282 |
| 33 | 33 | 1 | 33 | 12.1212 | -1.0047 | .8613 | .4947 |
| 34 | 34 | 1 | 34 | 32.3529 | 1.8890 | 4.4261 | 3.5436 |
| 35 | 35 | 1 | 35 | 11.4285 | -1.1619 | 1.1269 | .7112 |

KANSAS GEOLOGICAL SURVEY COMPUTER PROGRAM
THE UNIVERSITY OF KANSAS, LAWRENCE

PROGRAM ABSTRACT

Title (If subroutine state in title):

FORTRAN II Time-Trend Package for the IBM 1620 Computer

Computer: IBM 1620

Date: 20 November 1967

Programming language: PDQ FORTRAN II

Author, organization: John C. Davis, Kansas Geological Survey and Robert J. Sampson, Idaho State University, Pocatello

Direct inquiries to: Authors, or

Name: Daniel F. Merriam

Address: Kansas Geological Survey

University of Kansas, Lawrence, Kansas 66044

Purpose/description: Computes cross- and autocorrelations, cross-difference products, or cross associations between chains of numeric data.

Mathematical method: _____

Restrictions, range: Chains containing up to 350 points may be used.

Storage requirements: _____

Equipment specifications: Memory 20K 40K _____ 60K _____ K _____

Automatic divide: Yes No _____ Indirect addressing Yes No _____

Other special features required Requires PDQ FORTRAN II compiler and subroutine set.

Additional remarks (include at author's discretion: fixed/float, relocatability; optional: running time, approximate number of times run successfully, programming hours) Also written in FORTRAN IV for the GE 625 as a single program.

COMPUTER CONTRIBUTIONS

Kansas Geological Survey
University of Kansas
Lawrence, Kansas

Computer Contribution

| | |
|--|--------|
| 1. Mathematical simulation of marine sedimentation with IBM 7090/7094 computers, by J. W. Harbaugh, 1966 | \$1.00 |
| 2. A generalized two-dimensional regression procedure, by J. R. Dempsey, 1966 | \$0.50 |
| 3. FORTRAN IV and MAP program for computation and plotting of trend surfaces for degrees 1 through 6, by Mont O'Leary, R. H. Lippert, and O. T. Spitz, 1966 | \$0.75 |
| 4. FORTRAN II program for multivariate discriminant analysis using an IBM 1620 computer, by J. C. Davis and R. J. Sampson, 1966 | \$0.50 |
| 5. FORTRAN IV program using double Fourier series for surface fitting of irregularly spaced data, by W. R. James, 1966 | \$0.75 |
| 6. FORTRAN IV program for estimation of cladistic relationships using the IBM 7040, by R. L. Bartcher, 1966 | \$1.00 |
| 7. Computer applications in the earth sciences: Colloquium on classification procedures, edited by D. F. Merriam, 1966 | \$1.00 |
| 8. Prediction of the performance of a solution gas drive reservoir by Muskat's Equation, by Apolonio Baca, 1967 | \$1.00 |
| 9. FORTRAN IV program for mathematical simulation of marine sedimentation with IBM 7040 or 7094 computers, by J. W. Harbaugh and W. J. Wahlstedt, 1967 | \$1.00 |
| 10. Three-dimensional response surface program in FORTRAN II for the IBM 1620 computer, by R. J. Sampson and J. C. Davis, 1967 | \$0.75 |
| 11. FORTRAN IV program for vector trend analyses of directional data, by W. T. Fox, 1967. | \$1.00 |
| 12. Computer applications in the earth sciences: Colloquium on trend analysis, edited by D. F. Merriam and N. C. Cocke, 1967. | \$1.00 |
| 13. FORTRAN IV computer programs for Markov chain experiments in geology, by W. C. Krumbein, 1967. | \$1.00 |
| 14. FORTRAN IV programs to determine surface roughness in topography for the CDC 3400 computer, by R. D. Hobson, 1967 | \$1.00 |
| 15. FORTRAN II program for progressive linear fit of surfaces on a quadratic base using an IBM 1620 computer, by A. J. Cole, C. Jordan, and D. F. Merriam, 1967. | \$1.00 |
| 16. FORTRAN IV program for the GE 625 to compute the power spectrum of geological surfaces, by J. E. Esler and F. W. Preston, 1967 | \$0.75 |
| 17. FORTRAN IV program for Q-mode cluster analysis of nonquantitative data using IBM 7090/7094 computers, by G. F. Bonham-Carter, 1967 | \$1.00 |
| 18. Computer applications in the earth sciences: Colloquium on time-series analysis, D. F. Merriam, editor, 1967 | \$1.00 |
| 19. FORTRAN II time-trend package for the IBM 1620 computer, by J. C. Davis and R. J. Sampson, 1967 | \$1.00 |

Recent reprint (available for a limited time)

Re-interpretation of the *Cyrtina septosa* Band data, Lower Carboniferous of Derbyshire, England, by computer analysis, by H.E. Sadler and D.F. Merriam (reprinted from Sedimentology, v. 8, no. 1, p. 55-61). no charge

