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JUNE 14-16, 2016 | SHERATON TYSONS CORNER | TYSONS, VA





Inaccuracy of End Points of CO₂-Brine Relative Permeability Curves

Adverse Effect of Low Capillary Pressure during Testing and Proposed Solution (New Core Holder to Boost Capillary Pressure)

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Overview

- Importance of CO₂-brine relative permeability
- Status of CO₂-brine relative permeability data
- Evidence of CO₂-brine relative permeability inaccuracy
- Conventional test set up
- Numerical simulation of conventional test setup
- Reasons for CO₂-brine relative permeability uncertainties
- Effect on simulation of CO₂ storage projects
- Proposed new core holder







Importance of CO₂-Brine Relative Permeability

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\Box CO₂-brine relative permeability affects:

- Numerical simulations
- Flow and movement of CO₂ and brine
- Well injectivity index
- Number of injection wells
- Residual trapping of CO₂





Status of existing CO₂-Brine Drainage and Imbibition Relative Permeability Curves

- •Available data very limited
- •Data associated with uncertainty
- •Max CO₂ saturations low (less than 0.5, normally close to 0.9); especially, in high permeability core samples
- •Max CO_2 relative permeability abnormally low ($k_{rCO2max} < 0.4$, normally close to 1); especially, in high permeability samples



CARBON CAPTURE, UTILIZATION & STORAGE CONFERENCE Low endpoint attributed to Conventional Test setup (especially high permeability core samples)

- •CO₂ viscosity relative to brine very low
- •Length of test core is short
- •Differential pressure is low in high permeability sample ; therefore, produce low capillary pressure
 - customary core flood setup not suitable



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Wiltgen et al.(2003)

Why CO₂-Brine Relative Permeability Curves Are Flawed Effect of permeability

In high permeability test cores:

•Low differential pressure across test core at 100% CO₂ flooding

•Average capillary pressure in test core at 100% CO₂ flood less than differential pressure and low

•Max CO₂ saturation low because of low imposed capillary pressure

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•Max relative permeability to CO₂ also low



Evidence that CO₂-Brine Relative Permeability Curves are Flawed

Correlation between Swir and RQI



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Numerical Simulation of Conventional Test Setup for CO₂-Brine Relative Permeability



GasSat



At 100% CO₂ flow: kr_{CO2} of 26%, Swir of 41%





Results from Simulation of Conventional Test Setup Dependency of end points to test condition

\Box At 100% CO₂ flooding:

Increase in rate of CO₂ increases its end points

- •Increase in viscosity increases CO₂ end points
- •Increase in permeability decreases CO₂ end points



Measured and Real CO₂-Brine Relative Permeability High Permeability Sample



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CARBON CAPTURE, UTILIZATION & STORAGE CONFERENCE Why CO₂-Brine Relative Permeability Curves Are Flawed Effect of permeability

- In low permeability test core:
- High differential pressure
- High capillary pressure
- •low Sw and high S_{CO2}
- In High permeability test core:
- Low differential pressure
- Low capillary pressure
- •High Sw and Low S_{CO2}

st core: 0.1 0.01 0.01 0.01 0.001 0.001 0.01 0

10000

Delta P, psi

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Adverse Effect on Numerical Simulation of CO₂ Injection in Deep Saline Formations

In reality S_{CO2} at top reaches 90% when: In simulation it would not exceed 60%
 Formation horizontal perm is good
 Max drainage S_{CO2} inaccurate in

- •Vertical perm is poor
- •Large CO₂ plume is formed
- Plume thickness is 100 ft or more
 Pc at top of plume is >30 psi

- •Max drainage S_{CO2} inaccurate in simulation grids
- Residual trapping of CO₂ inaccurate in simulation cells because residual saturation depends on initial saturation

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Proposed New Core Holder Solves Uncertainty Problems High k Ceramic



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Numerical Simulation of New Core Holder



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Results - Numerical Simulation of New Core Holder

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•Correct endpoints were produced

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•End point not influenced by viscosity

•End points not affected by rate of flow

•End points not influenced by permeability of test core sample





Participants





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 Thanks are extended to KGS for their support and Julie Tollefson at KGS for her review of this work



Acknowledgements & Disclaimer

Acknowledgements

• The work supported by the U.S. Department of Energy (DOE) National Energy Technology Laboratory (NETL) under Grant DE-FE0002056 and DE-FE0006821, W.L. Watney and Jason Rush, Joint PIs. Project is managed and administered by the Kansas Geological Survey/KUCR at the University of Kansas and funded by DOE/NETL and cost-sharing partners.

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Thank you!

