

# Feasibility of CO<sub>2</sub> Sequestration in Deep Saline Reservoirs in the Midwestern USA

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*National Energy Technology Laboratory*

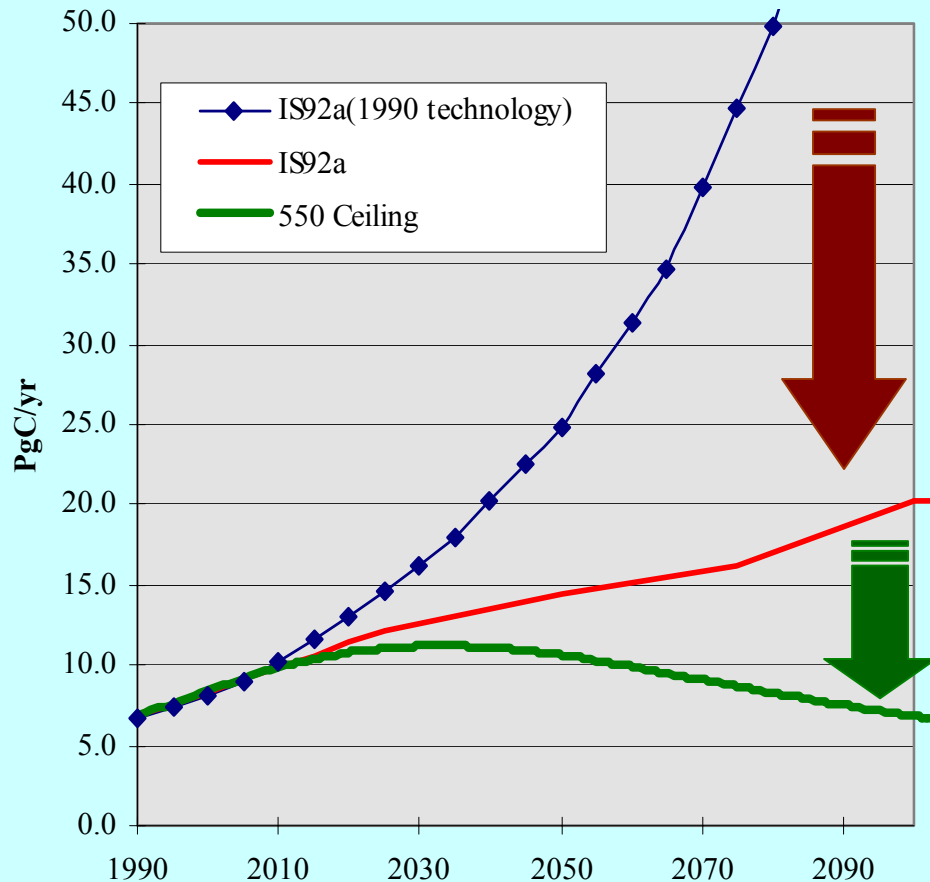
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# Presentation Outline

- ◆ Carbon Mitigation Background (from Edmonds et al.)
- ◆ Regional Setting and Capacity
- ◆ Site-Specific Reservoir Simulations
- ◆ Geochemical Aspects
- ◆ Regional Seismic Aspects
- ◆ Engineering and Economic Aspects

# Energy Technologies Currently in the Pipeline Are Not Enough for CO<sub>2</sub> Stabilization



Based on Work by Edmonds et al. at Battelle/PNNL

**Battelle**

**This gap could be filled by fully developed:**

**Solar**

**Nuclear**

**Efficient Fossil Electric**

**Advanced Transportation**

**End Use Efficiency**

**But stabilization**

**requires**

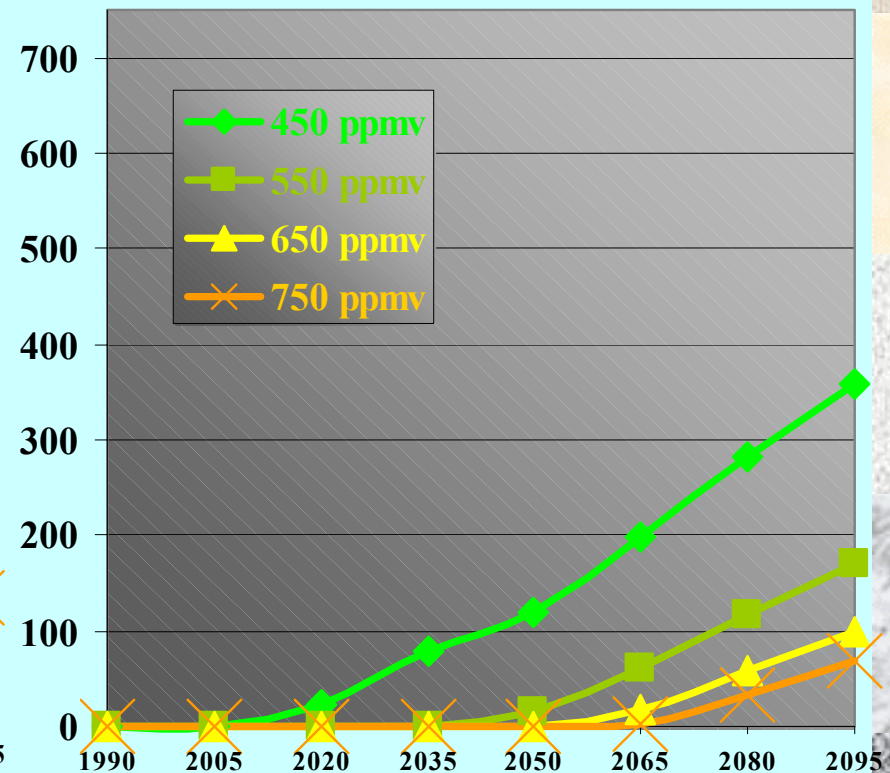
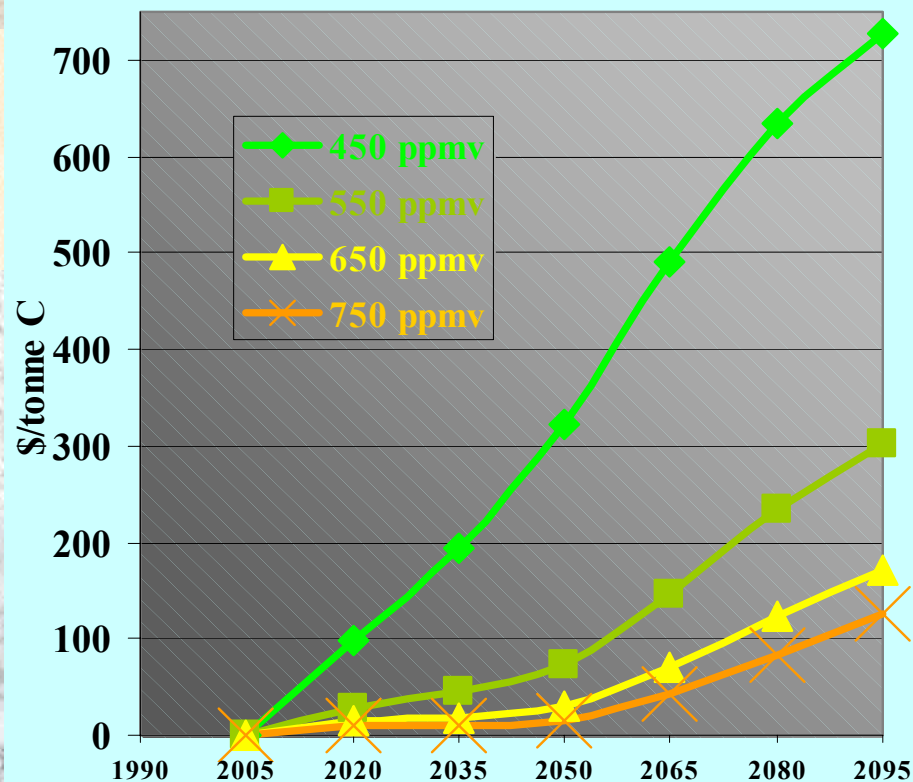
**additional**

**Carbon S&T!**

# Modeling Carbon Sequestration

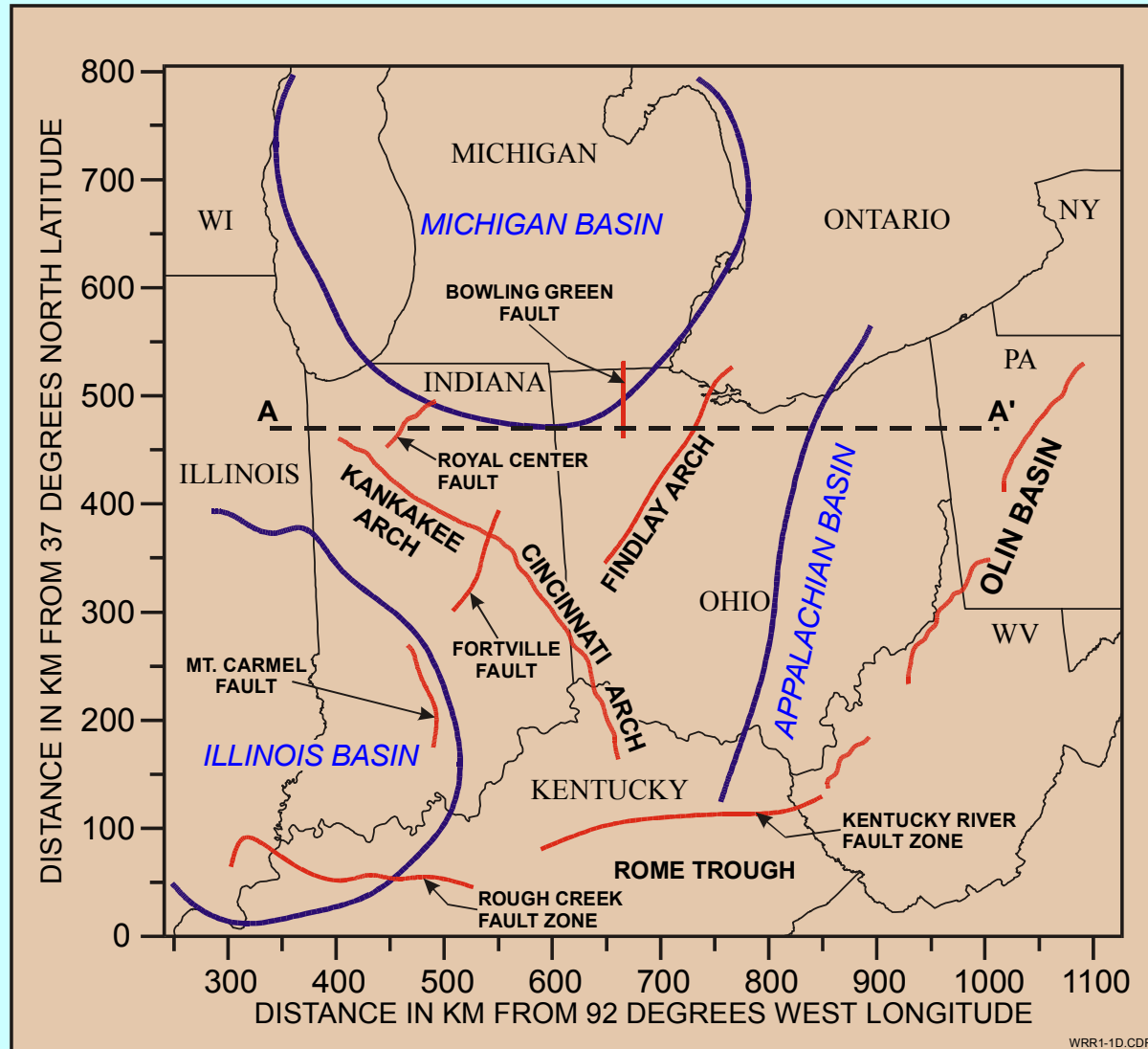
## Value of Carbon Permit Prices 2005 to 2095 (CBF)

Energy Technologies Only      With Capture & Sequestration

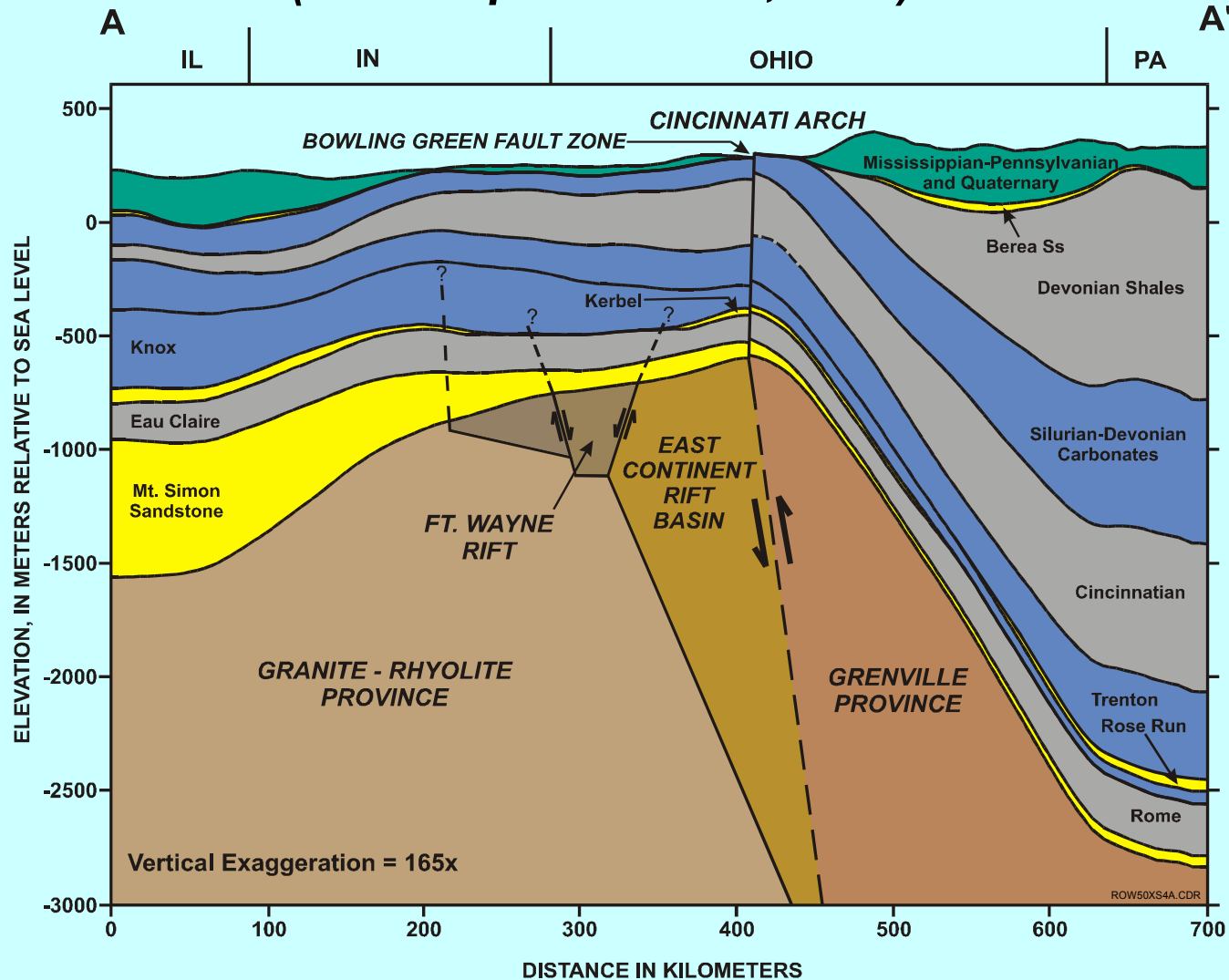


Based on Work by Edmonds et al. at Battelle/PNNL

# Geographic And Geologic Features in Midwestern USA



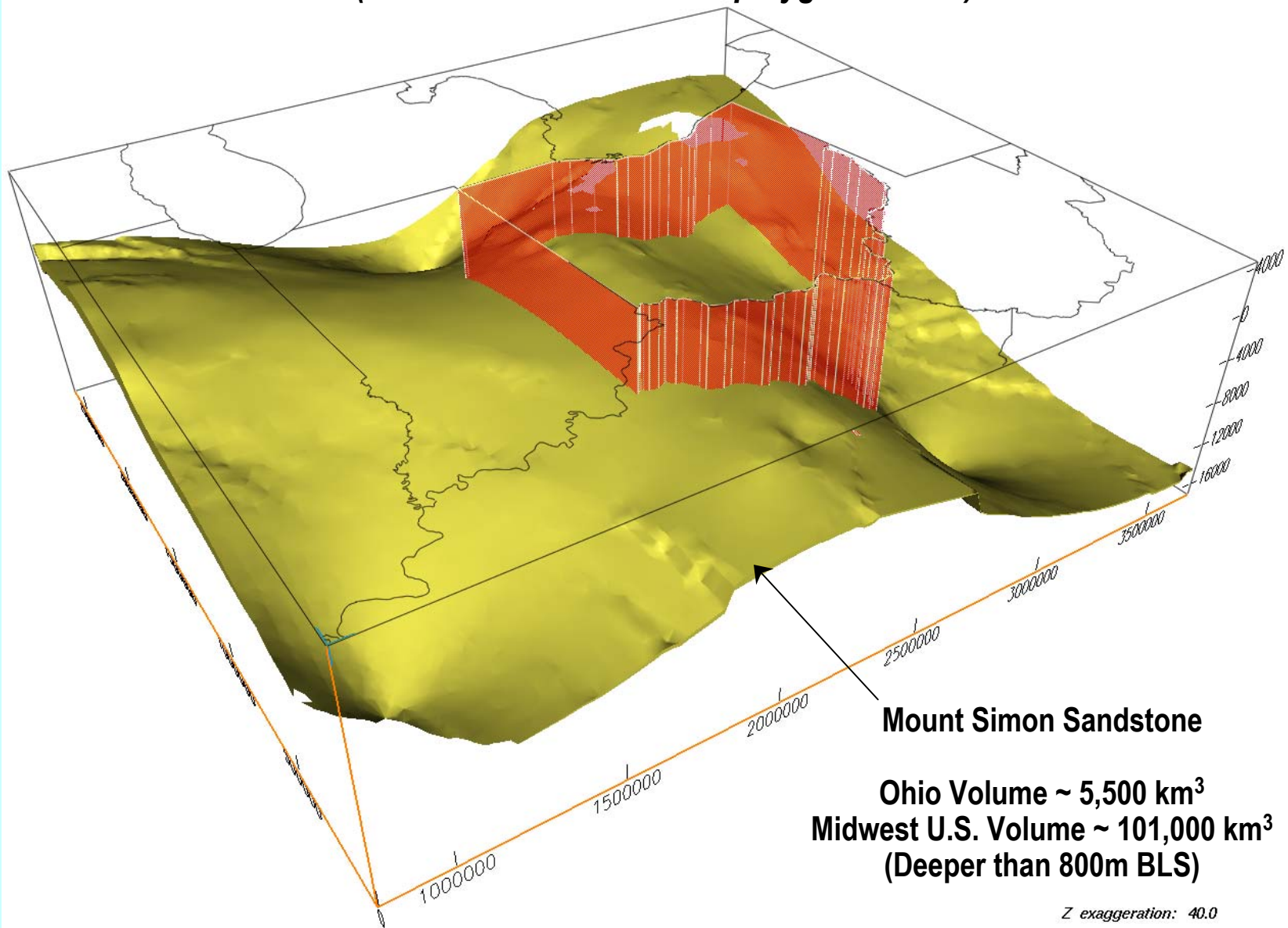
# East-West Geologic Cross-Section Through Midwestern U.S. Showing Major Sedimentary Units (after Gupta and Bair, 1997)





# 3D Block Diagram of Mount Simon Sandstone

*(Ohio is outlined with red polygon curtain)*



**Mount Simon Sandstone**

**Ohio Volume ~ 5,500 km<sup>3</sup>  
Midwest U.S. Volume ~ 101,000 km<sup>3</sup>  
(Deeper than 800m BLS)**

*Z exaggeration: 40.0*

X,Y, and Z ScaleBar units = Feet

# Regional CO<sub>2</sub> Storage Capacity Calculation for Mt. Simon and Rose Run Sandstones

Storage Capacity = Vp x Storage Efficiency x density of CO<sub>2</sub>  
(Joule II Report)

- ◆ Vp = Bulk aquifer volume x Net:Gross x Porosity
- ◆ Bulk aquifer volume from regional geologic data
- ◆ Net:Gross = 50 to 95%
- ◆ Porosity = 5 to 15%
- ◆ Storage efficiency = 6%
- ◆ Density of CO<sub>2</sub> = 700 kg/m<sup>3</sup>



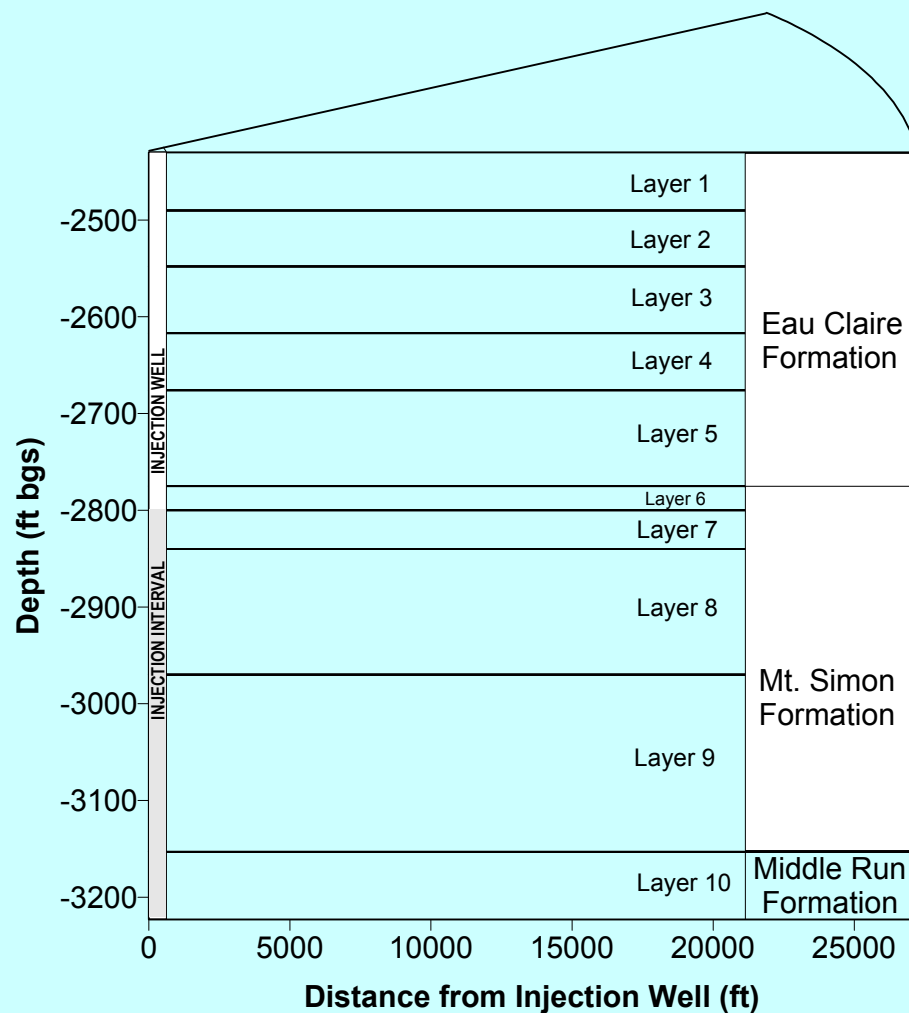
# Estimated Regional CO<sub>2</sub> Storage Capacity

- ◆ Based on Joule II equation for continuous reservoirs:
  - Mt. Simon Sst. (Ohio) 6 – 34 Gt
  - Mt. Simon Sst. (Midwest) 115 – 655 Gt
  - Rose Run (Ohio) 1.5 – 8.6
  - Rose Run (Midwest) 8.5 - 48
- ◆ Bergman and Winter Estimate (U.S.) 5 - 500 Gt
- ◆ Power Plant Emissions (Ohio) ~150 Mt/Yr
- ◆ Conclusion: There is enormous potential capacity on a regional scale
- ◆ Note: Rose Run is a source of oil/gas

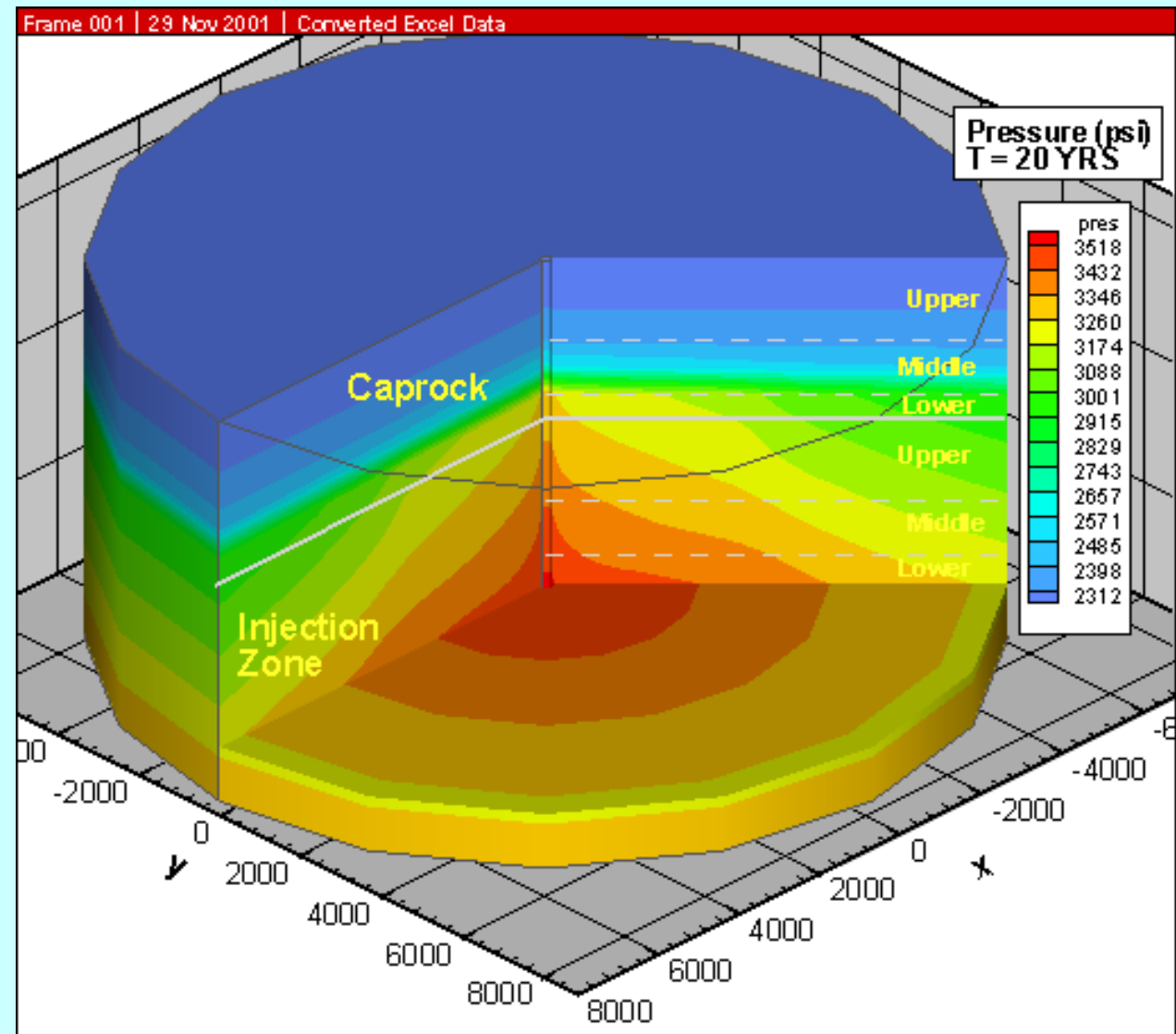
# Flow and Transport Models

- ◆ More realistic estimates require local-scale evaluation using computer simulations:
  - Simulate pressure variations, fracture pressure limitations, and zone of influence
  - Evaluate injection capacity
  - Fluid density and viscosity effects
  - Lateral and vertical movement of CO<sub>2</sub>
  - Containment time
- ◆ UTCOMP compositional code, modified by Dr. Peng Wang, was used

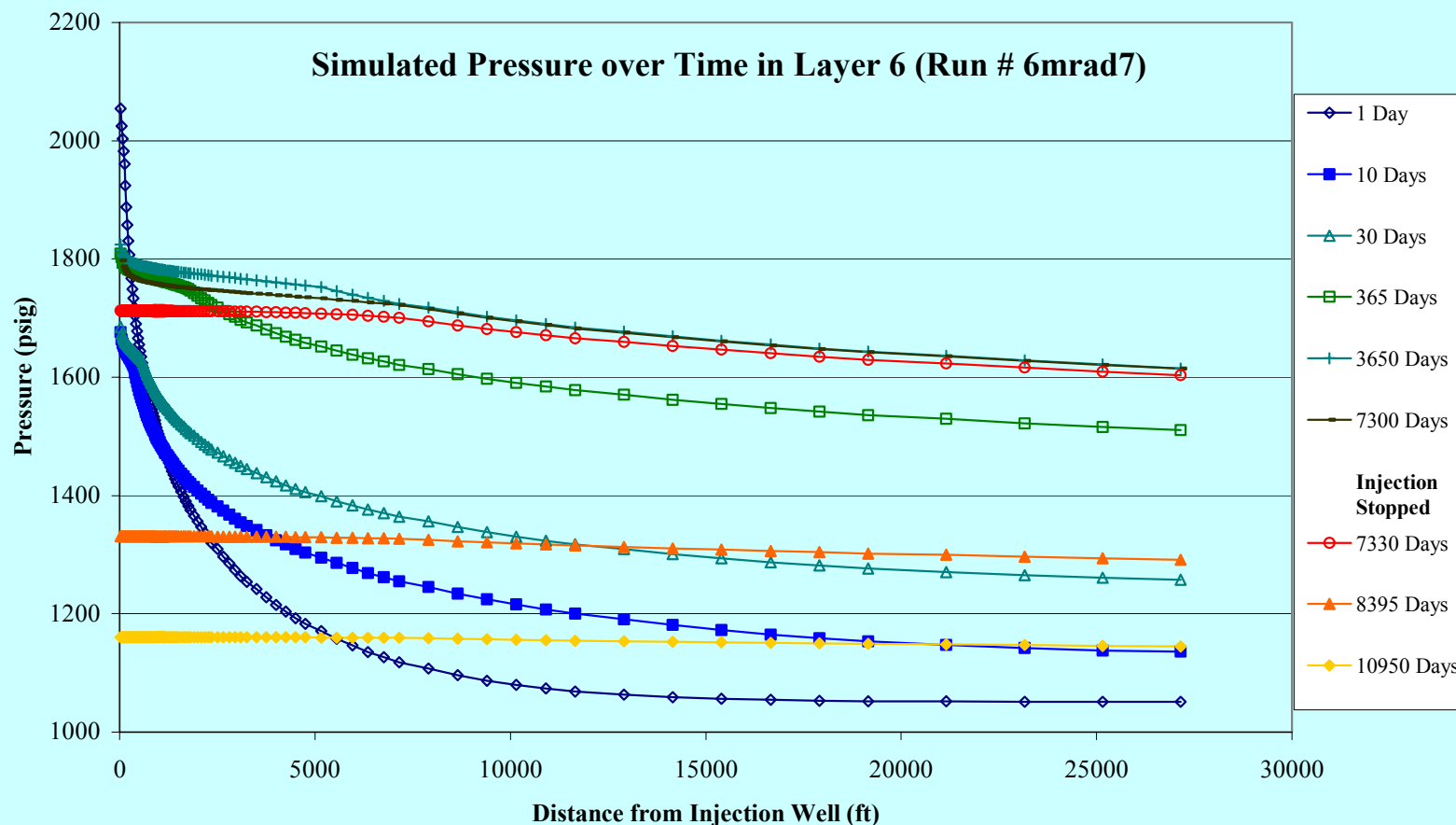
# Radial Reservoir Model



# Example of Simulated Pressure Distribution

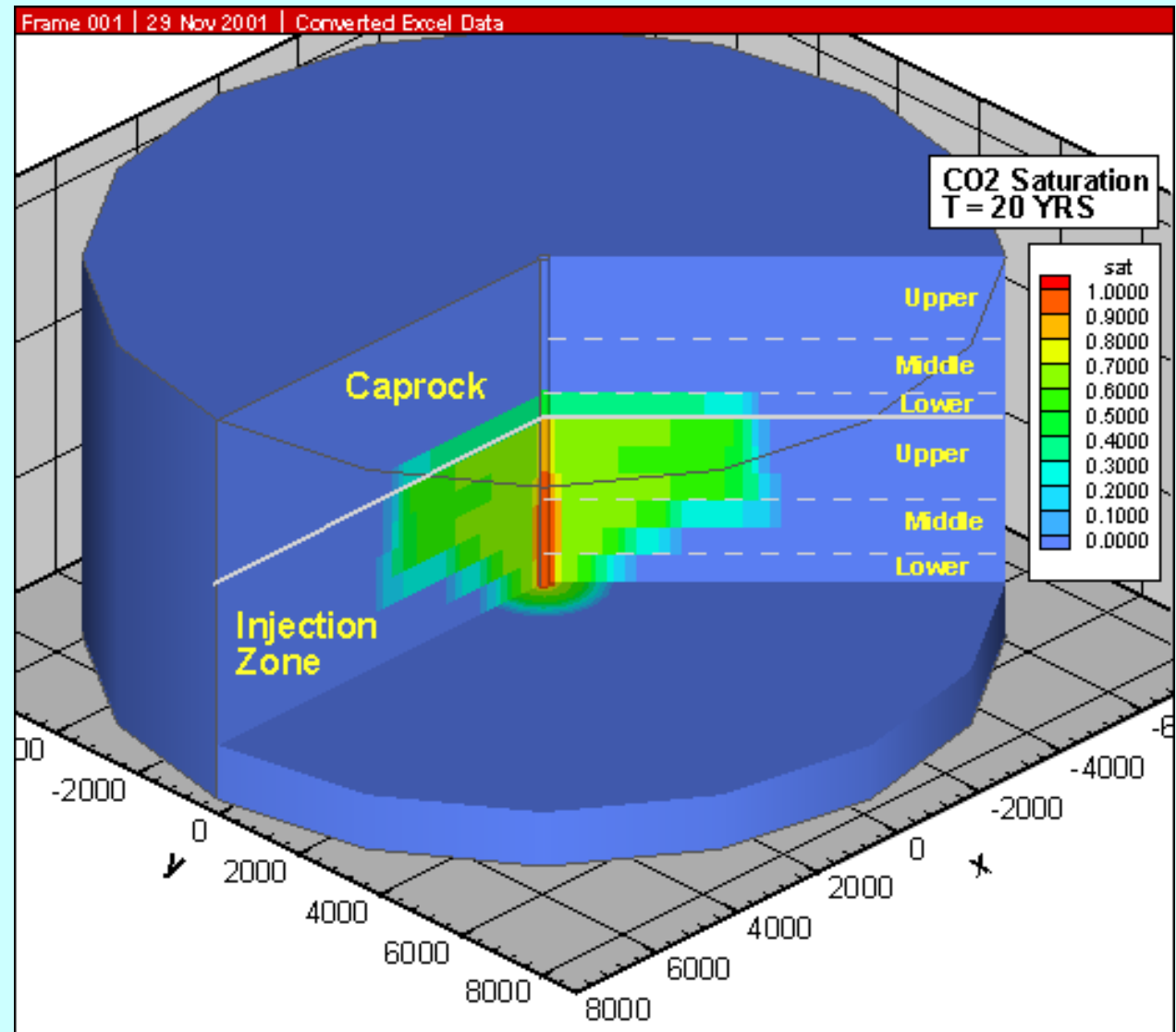


# Example of CO<sub>2</sub> Simulated Pressure Profiles



Maximum injection rates and caprock integrity are affected by pressure increase

# Example of Simulated CO<sub>2</sub> Phase Saturation





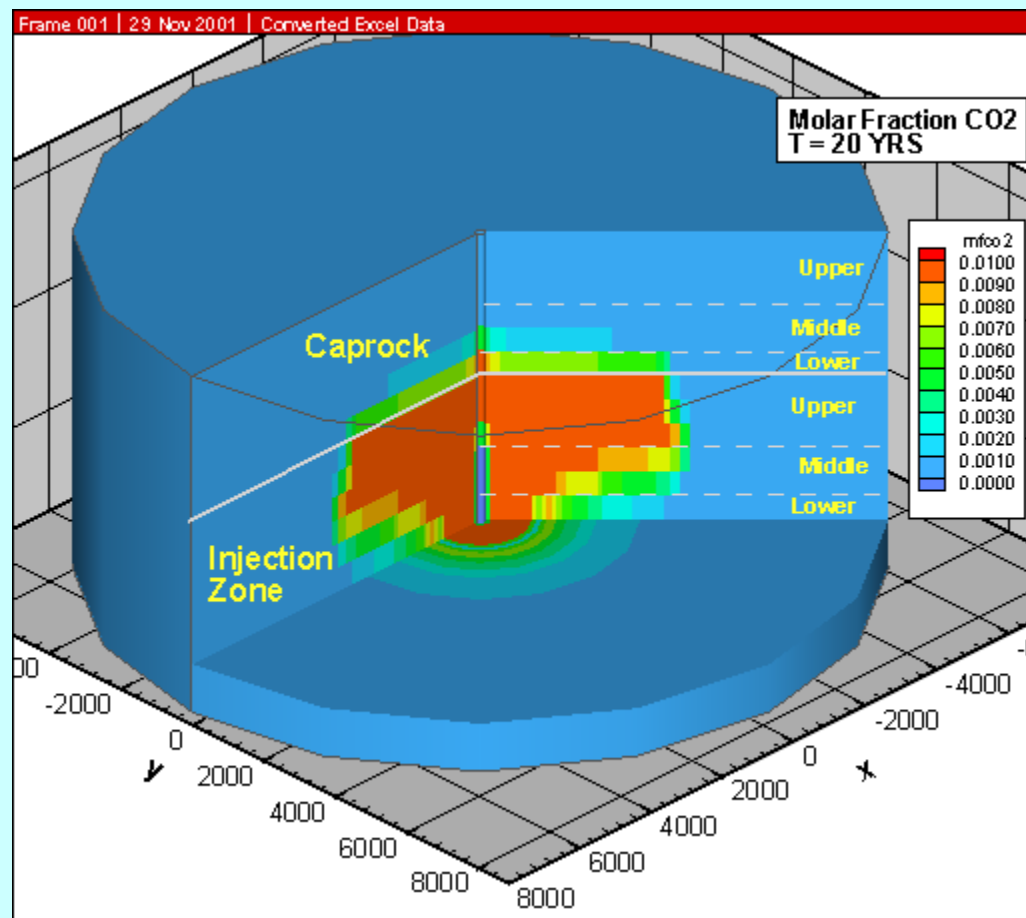
# Simulated Dissolved CO<sub>2</sub> Distribution

Function of Pressure,  
Temperature, Salinity

Simulated Dissolved %  
about 4-6%,

Increases Slowly Over  
Time

Typical CO<sub>2</sub> Mole Fraction  
~0.009 (2.3%)

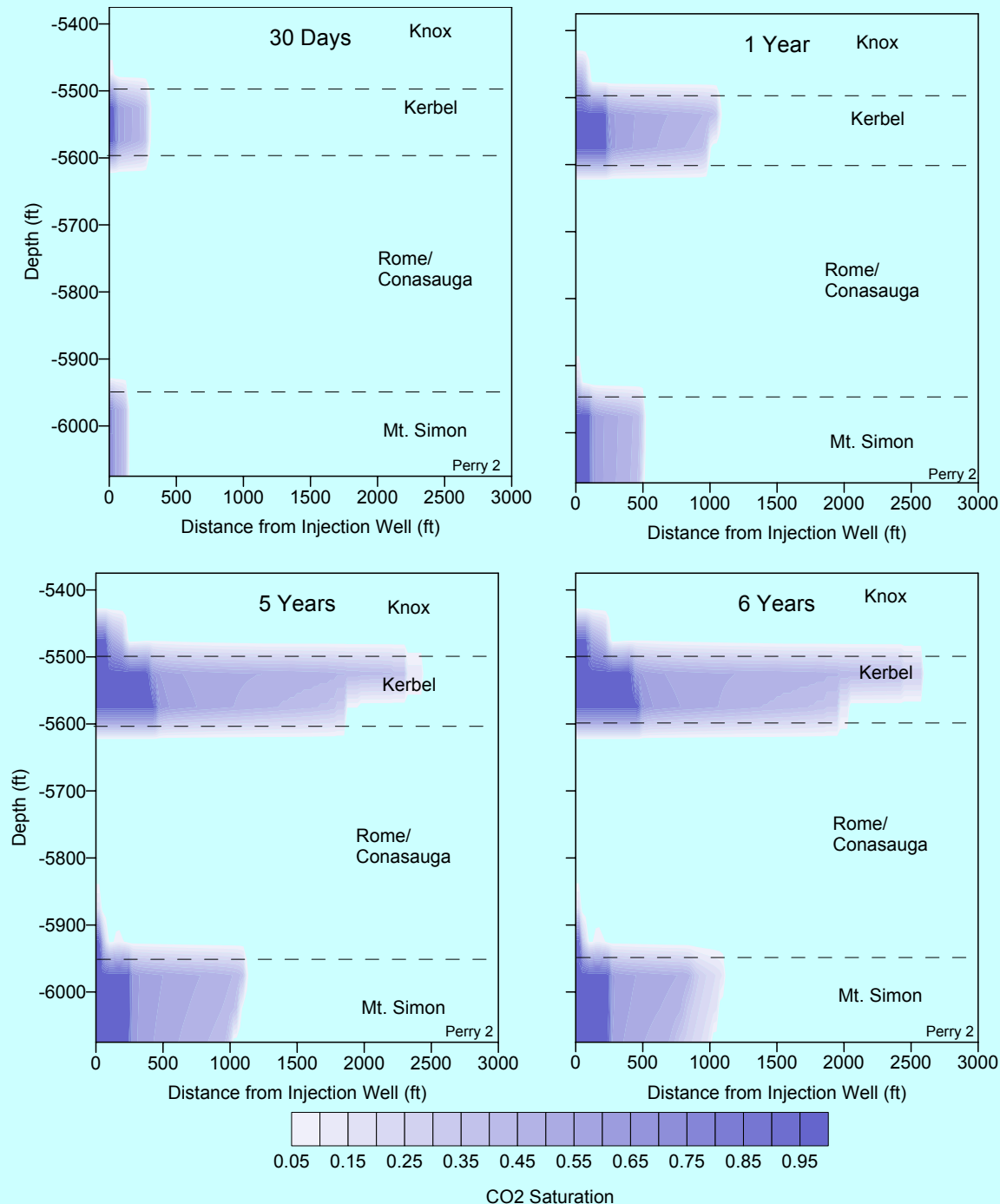


# CO<sub>2</sub> Phase Saturation for NE Ohio Simulation

Constant Pressure Injection

Injectivity ~ 206,000 ton/yr

Injectivity may be increased with Enhanced k

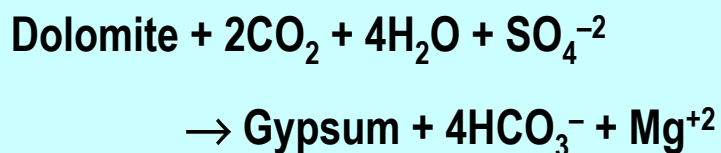


# Geochemistry Objectives

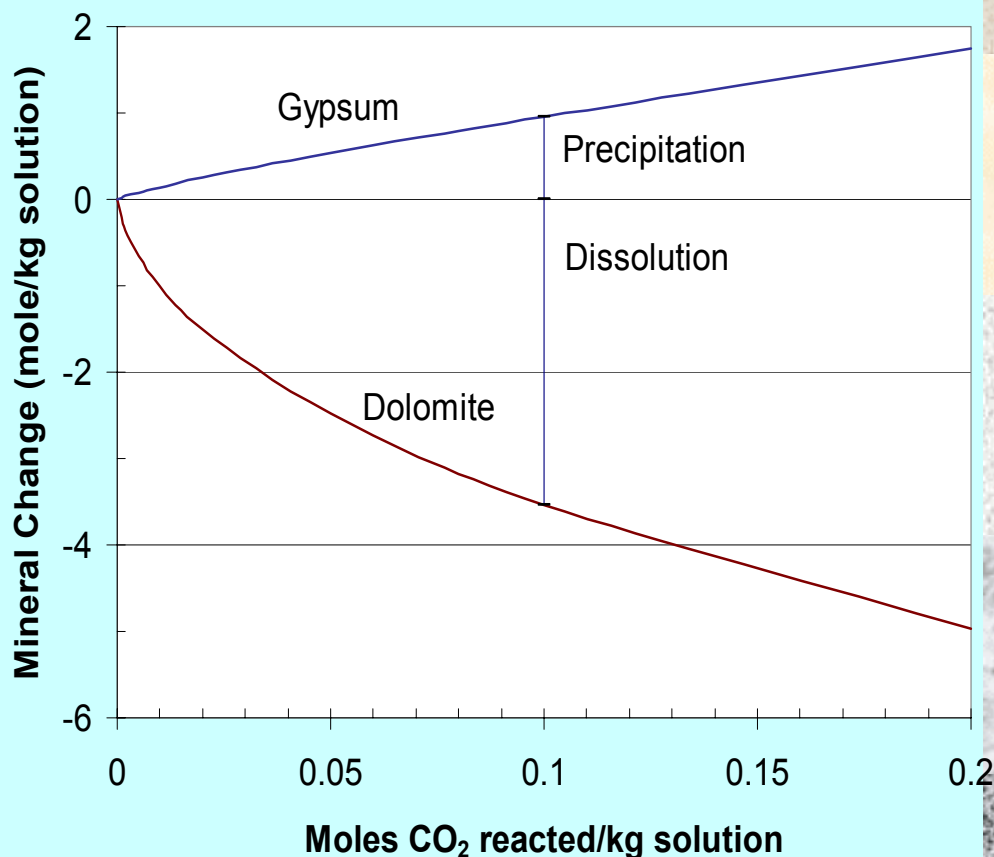
- ◆ Perform laboratory experiments to determine the potential for long-term sequestration of CO<sub>2</sub> in the Mt. Simon sandstone.
- ◆ Corroborate the experimental results by modeling the interaction of CO<sub>2</sub>, brine, and pure mineral phases at the same P-T conditions.

# Potential Reactions Between CO<sub>2</sub> and Minerals

In the absence of iron or calcium-bearing mineral phases, geochemical modeling predicts dolomite dissolution and gypsum precipitation according to the following reaction stoichiometry:



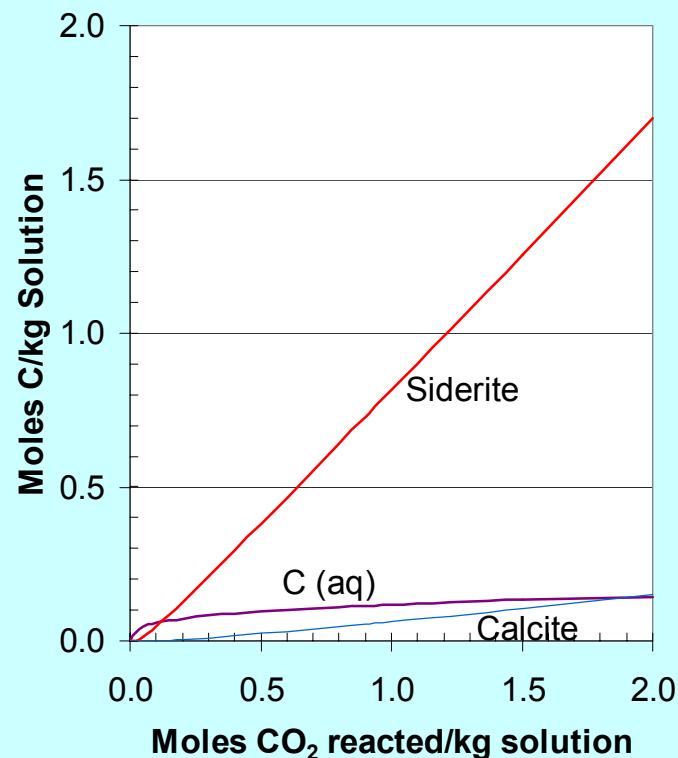
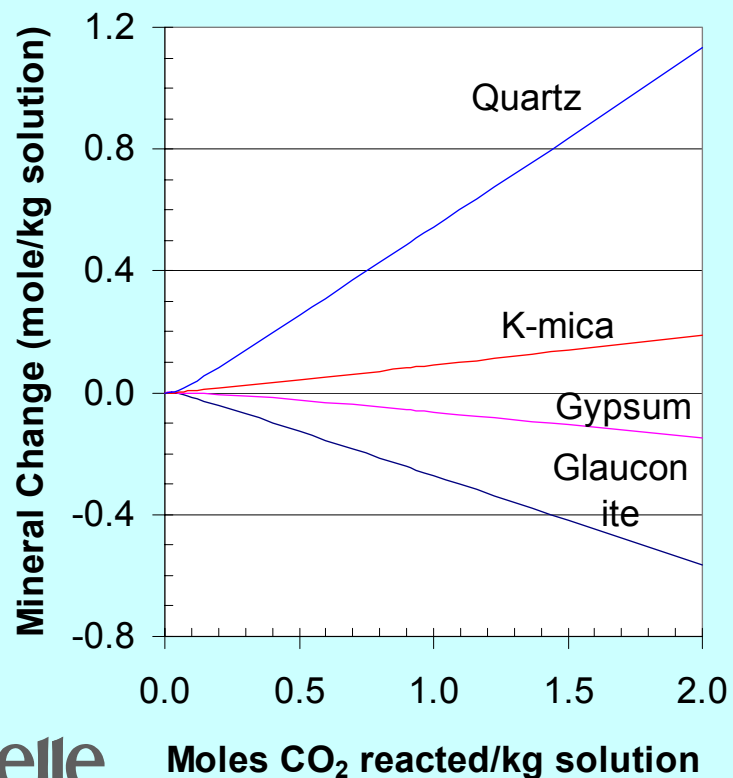
Note that 2 moles of CO<sub>2</sub> are converted to aqueous carbonate species for each mole of dolomite consumed



# Potential Reactions Between CO<sub>2</sub> and Minerals

Glaucanite, an iron-bearing phase, may react with CO<sub>2</sub> to form siderite. Geochemical modeling predicts the following changes in mineralogy:

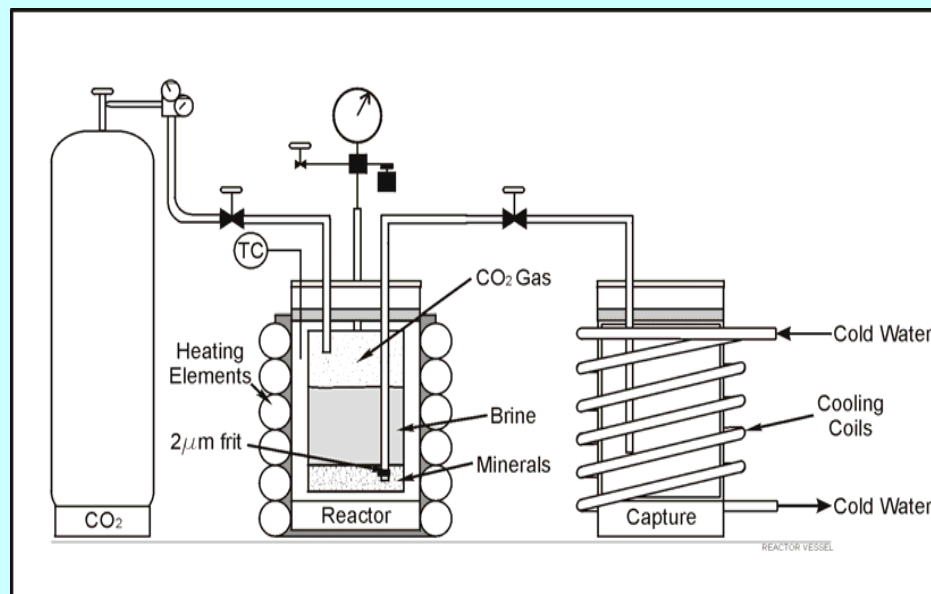
◆ Dissolution of glauconite and gypsum (if present) and Precipitation of siderite, K-mica, and silica (quartz), leading to permanent sequestration of carbon.



# Design for Mineral Equilibration Runs

## Typical Experimental Conditions:

- ◆ 50 – 150 °C
- ◆ 2000 – 2500 psi
- ◆ Variable P-CO<sub>2</sub>
- ◆ Variable P-SO<sub>2</sub>
- ◆ Natural rock cores
- ◆ Pure minerals
- ◆ Monitor gas & liquid
- ◆ Bulk and surface analysis of solid phases





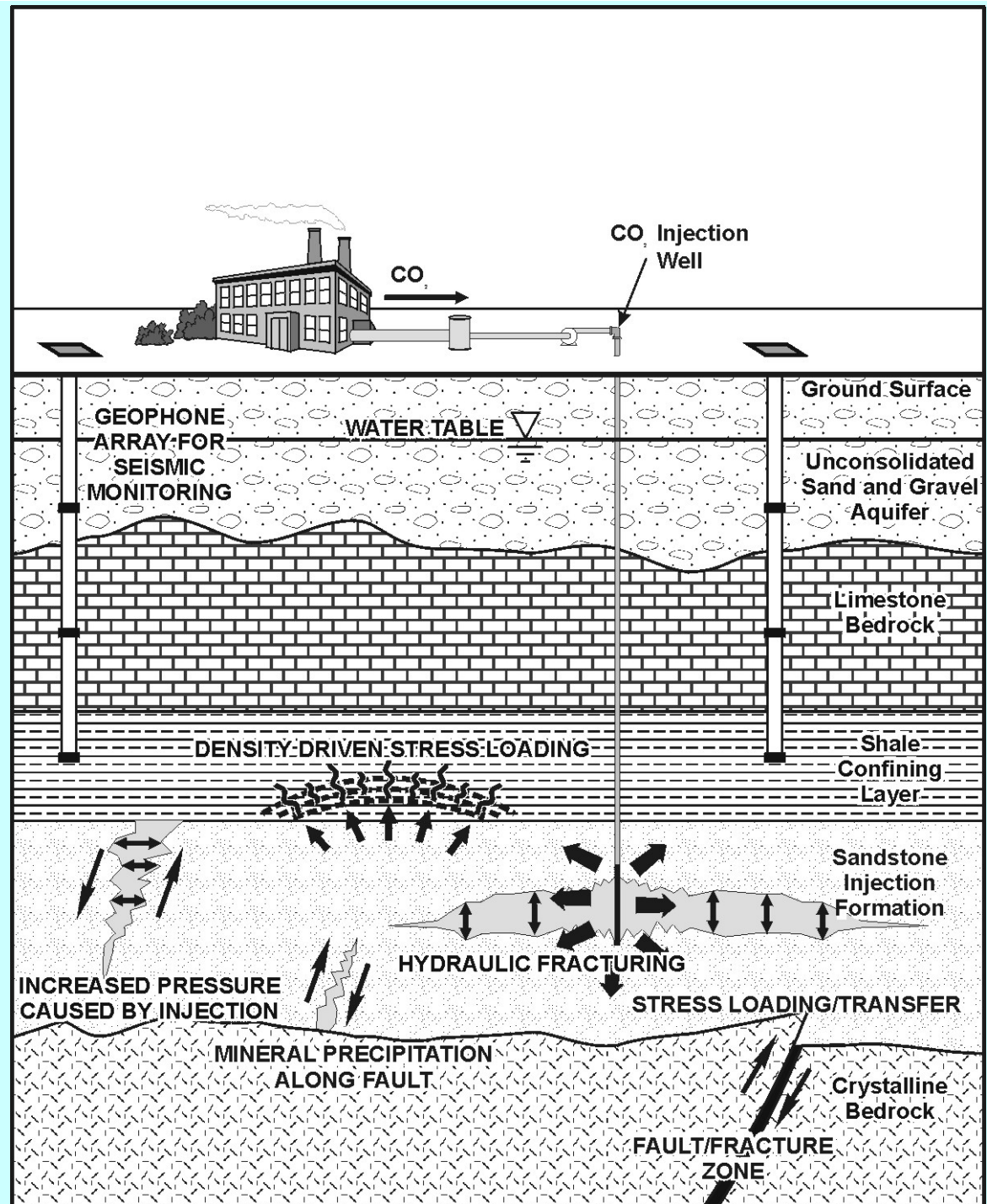
# Materials used in Experiments

- ◆ Mt. Simon Sandstone
- ◆ Rome Dolomite and Eau Claire Shale
- ◆ Frio Formation (Gulf Coast)
- ◆ Pure Anorthite
- ◆ Mixtures with pure glauconite, kaolinite and montmorillonite.
- ◆ Temperatures between 50 and 150°C
- ◆ Pressure up to 2200 psi
- ◆ Pure CO<sub>2</sub> and mixtures of CO<sub>2</sub>/SO<sub>2</sub>

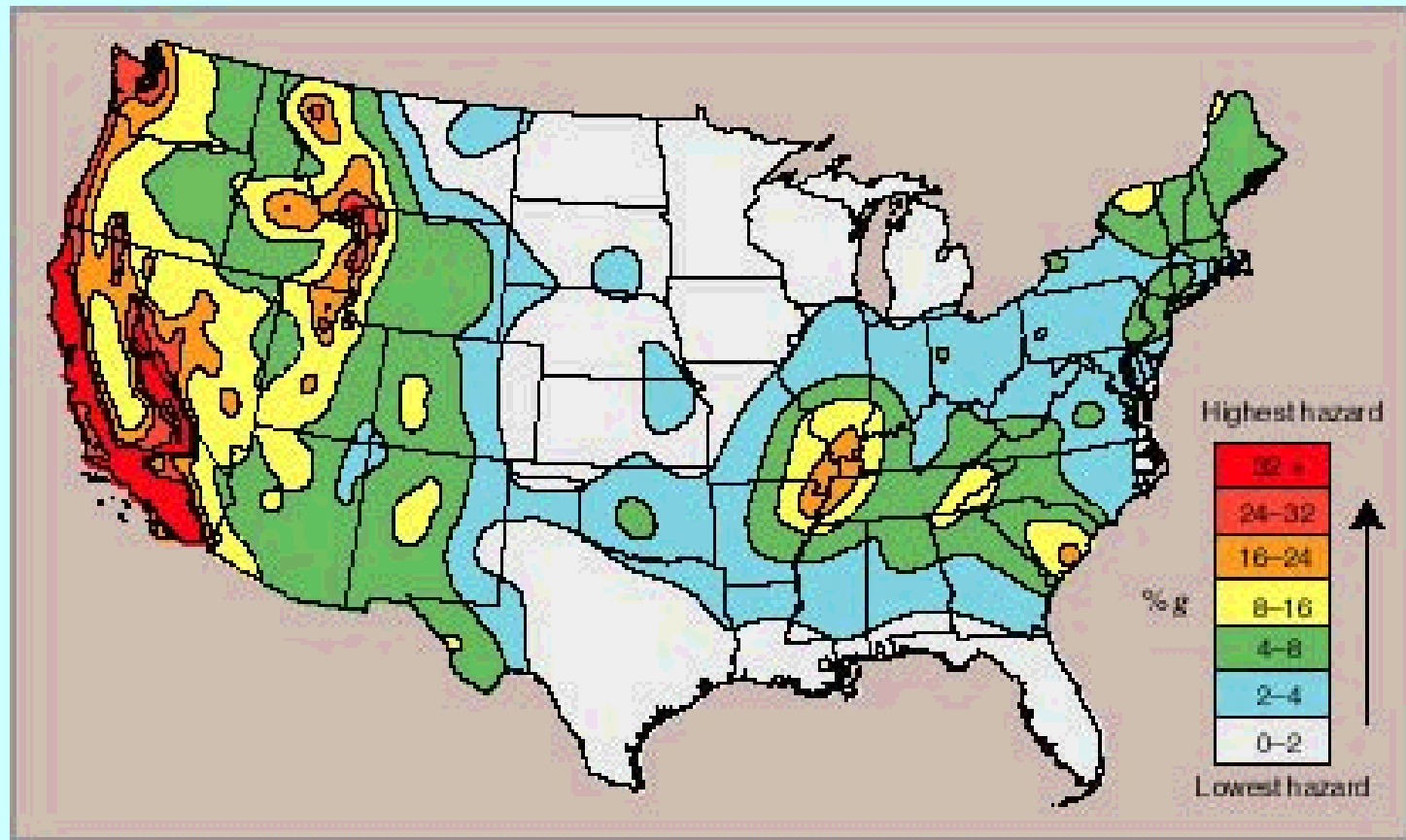
# Key Conclusions of Geochemical Investigation

- ◆ Experiments with Mt. Simon sandstone (host rock) reveal no adverse consequences of interaction with CO<sub>2</sub>.
- ◆ Experiments to verify mineral trapping show progress toward that end, but are generally too slow to be accomplished during short time periods (< 1 year).
- ◆ Geochemical modeling predicts mineral dissolution behavior and was used to assess carbonate precipitation under equilibrium conditions.
- ◆ Enhancements in experimental design are expected to speed reaction progress.

# Induced Seismicity



## Seismic Hazard Map for the United States (USGS National Seismic Hazard Mapping Project)



# Seismic Evaluation Summary

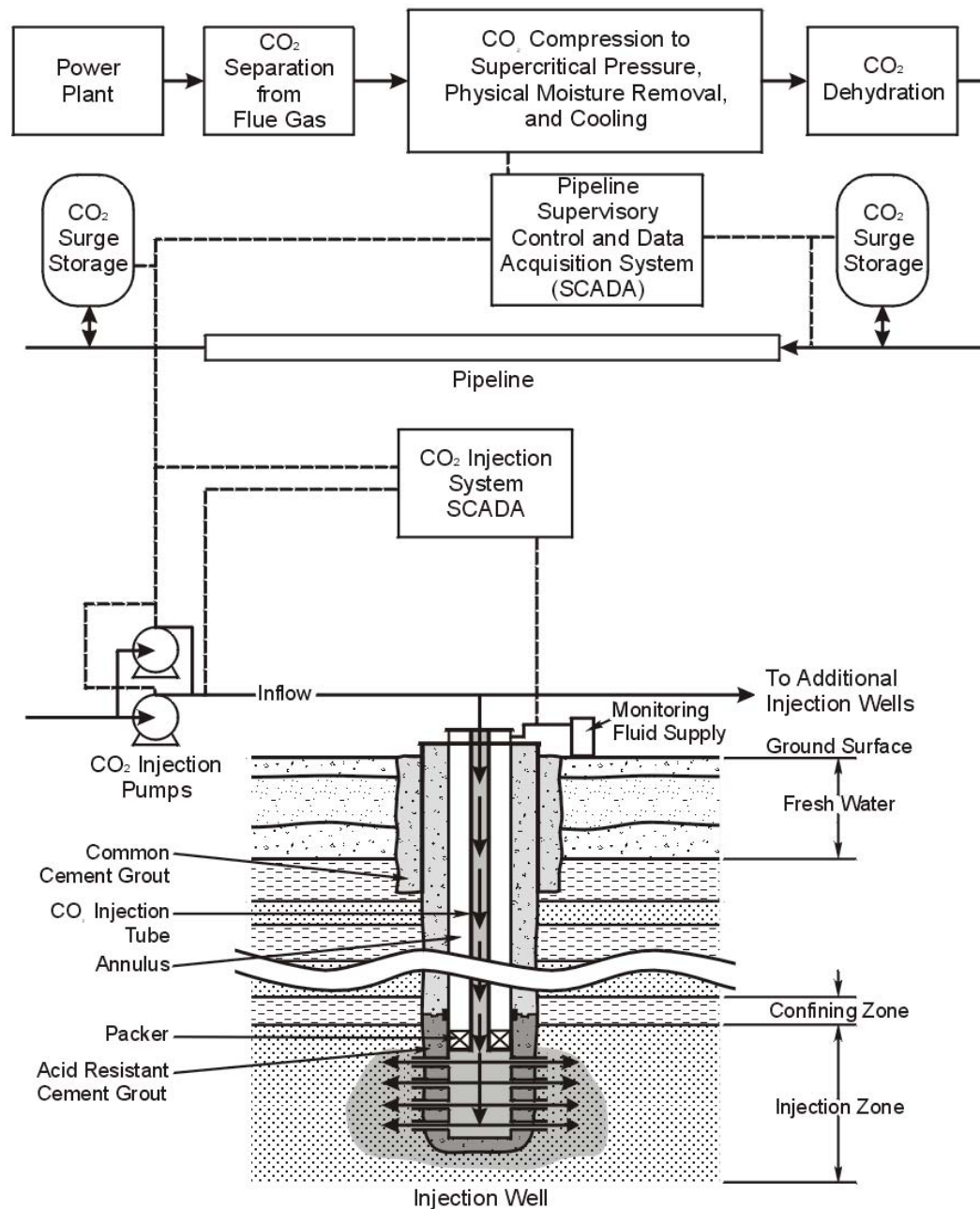
- ◆ Seismic activity induced by deep well disposal of CO<sub>2</sub> is a real possibility under certain conditions.
- ◆ Most seismic activity caused by deep well injection is the result of frictional failure along previously faulted rocks.
- ◆ Formation weakening, mineral precipitation, and density driven stress loading should also be evaluated in light of the special properties of supercritical CO<sub>2</sub>.
- ◆ Through proper siting, testing, and monitoring, induced seismicity may be prevented.
- ◆ Areas in the central, midwestern, and southeastern United States are generally seismically suitable for deep well injection of CO<sub>2</sub>. However, site-specific assessment must be performed.

# Engineering and Economic Analysis

- ◆ Capture CO<sub>2</sub> from the flue gas from 4 types of plants
- ◆ Preparation of the CO<sub>2</sub> for transmission as a supercritical liquid (compression and dehydration)
- ◆ Transmission of the CO<sub>2</sub> through a pipeline
- ◆ Injection of the CO<sub>2</sub> into a suitable aquifer
- ◆ Sensitivity Analysis
  - Power plant types PC, Coal with O<sub>2</sub>, IGCC, NGCC
  - Transportation distance 15, 100, and 400 km
  - Injection depth 1,000, 2,000, and 3,000 m
  - Normal, hilly/rocky, and urban terrain



# CO<sub>2</sub> Storage System Components



# Coal-Fired Plant Cost Breakout

## Annualized Cost for 500 MWe Plant and 25 Years of Operation

Plant Type	Depth (m)	Pipeline (km)	Terrain	Capture (\$mil/yr) A	Compression (\$mil/yr) B	Capture and Compression (\$mil/yr) C <sup>(c)</sup>	Pipeline (\$mil/yr) D	Injection (\$mil/yr) E	Total Cost (\$mil/yr) F <sup>(d)</sup>
PC/FGD <sub>(e,f)</sub>	2,000	15	Normal	20.04	33.39		1.79	3.88	
Scenario totals						53.43			59.10
PC/FGD	2,000	100	Normal	20.04	33.39		7.66	3.88	
Scenario totals						53.43			64.97
PC/FGD	2,000	400	Normal	20.04	33.39		28.89	3.88	
Scenario totals						53.43			86.20
PC/FGD	1,000	15	Normal	20.04	33.39		1.79	2.79	
Scenario totals						53.43			58.01
PC/FGD	3,000	15	Normal	20.04	33.39		1.79	6.11	
Scenario totals						53.43			61.33
PC/FGD	2,000	15	Rocky	20.04	33.39		2.06	3.88	
Scenario totals						53.43			59.37
PC/FGD	2,000	15	Urban	20.04	33.39		2.19	3.88	
Scenario totals						53.43			59.50
IGCC <sup>(g)</sup>	2,000	15	Normal	4.07	28.28		1.79	3.59	
Scenario totals						32.35			37.73

Unit Cost (\$/ton CO<sub>2</sub> Avoided) - PC ~ 60-80, IGCC ~ 40

# Summary

- ◆ On a regional basis there is enormous potential sequestration capacity due to favorable formation thickness, hydrogeology, seismicity, and proximity to sources of CO<sub>2</sub>
- ◆ The key issues are local capacity, long-term fate, engineering, cost, safety, and public acceptance
- ◆ The site-specific sequestration potential varies due to local thickness, permeability, porosity, structural features, and depth
- ◆ Detailed Engineering and Economic Assessment has been Performed

# CO<sub>2</sub> Capture and Disposal Demonstration Plan

